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COMMITTEE D02 on PETROLEUM PRODUCTS, LIQUID FUELS, AND LUBRICANTS

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Sequence VIII Surveillance Panel Meeting Minutes Thursday September 21, 2023 Teams Meeting (Virtual) 10:00 - 11:00 AM CDT

Minutes recorded by Patrick Lang Direct any comments or corrections to: <u>patrick.lang@swri.org</u>

The attendance list can be found as Attachment #1.

There were no membership changes brought to the attention of the panel.

Agenda:

The agenda can be found as Attachment #2.

Minutes Approval:

Pat Lang advised that the minutes from the June 21, 2023, virtual meeting were posted to the TMC website. A motion was made for approval of the minutes by Pat Lang and seconded by Robert Stockwell. The minutes were approved with no objections or changes.

Travis Kostan went through the recommendation of the stats group; the presentation can be found as Attachment #3.

The highlights are as follows:

According to Stats group, the new Bearing Batch can be accepted. We should re-evaluate soon once additional data becomes available because a lot of assumptions were made with little data.

Travis explained that stand B1 produced severe results after the 1009 run on that stand, so actual performance is unclear due to mechanical wear on two of the tests from that stand. One of the severe results was on 704-1. There was another data point generated on 704-1 on stand B2 during the severity investigations that was considered in this evaluation along with a 1009-1 run at both labs since all three runs were conducted in a similar manner. This gave us 14 data points in the evaluation.

Two options moving forward for the ICF:

Option 1:

- A) ICF= -4.9 /1009-1 target of 14.9 mg (4 data points used for determining the 1009-1 mean)
- B) <u>Bottom line</u>: this option gives a larger ICF because it assumes the new bearing batch is more severe and we shouldn't attribute that bias to the 1009-1 reblend. Remember, the ICF compensates for the current severity trend not the difference in 1009 performance as a result of the reblend (1009-1).
- C) <u>Possible detriment</u>: If bearings are not really different, the ICF could over correct candidates.
- D) <u>Reality</u>: This larger correction factor is minimal compared to the other option and is not going to turn a bad candidate into a pass.

Option 2:

- A) ICF= -3.6/1009-1 target of 16.2 mg (7 data points used to determine the 1009-1 mean)
- B) <u>Bottom Line</u>: This option gives a slightly smaller ICF because the target update for 1009-1 uses data from both bearing batches. Using data from both batches makes the assumption that there is no difference in bearing batches, i.e., the variation is normal. These additional datapoints skew the 1009-1 mean a bit higher. So now labs need a smaller correction to be on target when running references on 1009-1. As a result, the ICF, which is designed to compensate for the severity bias outside of the reblend, is smaller.
- C) <u>Possible detriment</u>: Candidates tests get a smaller correction when they should get more.
- D) <u>Reality</u>: this smaller correction is only minimal compared to Option #1.

There was a lot of discussion amongst the members on which option to choose. It was noted that there really isn't a "bad" option to choose from. The decision really hinges on whether or not you are of the opinion that the bearings are different. Jo Martinez of Oronite pointed out that there are three 1009-1 results on the new bearing batch (03-22) and two of the three produced higher results than on the 06-16 bearings (current batch). She further added that there is an obvious difference in performance when you look at the plot, but it is considered a marginal difference statistically. Travis advised that there was one more data point on 1009-1 from lab B that was produced after the matrix was complete and the data analyzed. This datapoint could be considered in the analysis if the group thought it would appropriate.

In general, most of the group was leaning towards Option #1. George Szappanos mentioned that if there is a difference in the bearings, it will affect candidates so we shouldn't lump all of the 1009-1 results together. As a result, we need to consider that when we make our decision. If you agree with this then Option #1 is the appropriate option because it only utilized the four tests on 1009-1 with the 06-16 bearings when determining the 1009-1 LTMS mean.

The direction question was asked to the OEM's on their preference. Mike Deegan from Ford and Brad Cosgrove from GM were leaning toward Option #2. Travis advised that this is a more conservative choice.

At this point, the time that was allocated for the meeting was already up. The group agreed that we need more time to make a decision, so another call was in order. Additionally, there was no remaining time to review the recommendation for stripped viscosity. This will be done on the next call.

Rich Grundza cautioned the group that since we are looking at an LTMS change with the addition of a new reference oil, we will likely have to exercise the two-week waiting period before it can be officially implemented.

Next Meeting:

The next meeting will be Thursday September 28 at 9:00 CDT.

Attachment #1

Attendance List

V= present

ASTM SEQUENCE VIII SURVEILLANCE PANEL VOTING MEMBERSHIP ATTENDANCE RECORD

Teams MTG 9-21-23

Name	Address	Attendance
Alfanso, Adrian	Intertek 5404 Bandera Road San Antonio, TX 78238 Phone:210-647-9429 adrian.alfonso@intertek.com	
Bowden, Jason	OH Technologies, Inc. P.O. Box 5039 Mentor, OH 44061-5039 Phone: 440-354-7007 dhbowden@ohtech.com	
Savant, Amol	Valvoline 21st and Front Streets Ashland, KY 41101 Phone: 606-585-8982 acsavant@valvolineglobal.com	
Maddock, Ben	Afton Chemical 500 Spring Street P.O. Box 2158 Richmond, VA 23218 Ben.Maddock@aftonchemical.com	
Grundza, Rich	ASTM/TMC Phone: 412-365-1031 reg@astmtmc.org	
Hsu, Jeff	Shell Projects and Technology-USA 3333 Hwy 6 Houston, TX 77082 Phone:281-544-8619 J.Hsu@shell.com	1.
Hairston, William	Haltermann Solutions 15600 W. Hardy Road Houston, TX 77060 Phone No: 832-647-9264 whhairston@haltermann.com	
Riou, Joseph	Southwest Research Institute 6220 Culebra Road P.O. Box 28510 San Antonio, TX 78228-0510 Phone: 210-522-6266 jriou@swri.org	

ASTM SEQUENCE VIII SURVEILLANCE PANEL VOTING MEMBERSHIP ATTENDANCE RECORD

Name	Address	Attendance

Lanctot, Dan	Test Engineering Inc. 12718 Cimarron Path San Antonio, TX 78249-3423 Phone: 210-690-1958 dlanctot@tei-net.com	
Kowalski, Teri	Toyota Motor North America, Inc. 1555 Woodridge Ann Arbor, Mi 48105 Phone: 734-995-4032 Cell: 734-355-8082 teri.kowalski@tema.toyota.com	
Cosgrove, Bradley	GM Global Propulsion Systems Phone: 313-590-2186 Bradley.Cosgrove@gm.com	V
Rubas, Paul	ExxonMobil Research and Engineering Company 600 Billingsport Rd. Paulsboro, NJ 08066 Email: paul.j.rubas@exxonmobil.com	
Tang, Haiying	Stellantis Phone: 248-512-0593 haiying.tang@stellantis.com	
Stockwell, Robert	Chevron Oronite Company LLC 4502 Centerview Drive Suite 210 San Antonio, TX 78228 Phone: 210-232-3188 Robert.stockwell@chevron.com	1
Agudelo, Jorge	BP Lubricants USA 1500 Valley Rd Wayne, NJ 07470 Jorge.Agudelo@BP.com	

ASTM SEQUENCE VIII SURVEILLANCE PANEL VOTING MEMBERSHIP ATTENDANCE RECORD

Name	Address	Attendance

Deegan, Mike	Ford Motor Company 17228 Federal Drive Allen Park, MI 48101 Phone: 313-805-8942 mdeegan@ford.com	
Ritchie, Andy	Infineum P.O. Box 735 1900 East Linden Ave. Linden, NJ 07036-0735 Phone: 908-474-2097 andrew.ritchie@infineum.com	
Szappanos, George	Lubrizol Corporation 29400 Lakeland Blvd. Wickliffe, OH 44092 Phone: 440-347-2631 George.szappanos@lubrizol.com	

15 Prost (voting) 18 voting mentions

ASTM SEQUENCE VIII SURVEILLANCE PANEL NON- VOTING MEMBERSHIP and GUESTS ATTENDANCE RECORD

Name	Address	Phone/Fax/Email	Attendance
Travis Kostan	Swri		~
Amanda Stone	After		1/
Ricardo Affinito	Ormife		V
Todd Dronak	Infineum		
Jo Martin Z	dronite		\checkmark
Ed Hennessy	Halfer many		\checkmark

Attachment #2

Agenda

- 1. Welcome
- 2. Attendance
- 3. Approval of the minutes from the June 21, 2023, virtual meeting. Minutes posted to TMC website.
- 4. Review of the matrix data.
 - a. Review of stats group recommendation for the industry correction factor (ICF) -Travis Kostan
- 5. Next Meeting will be at call of the chair
- 6. Adjournment

Attachment # 3

Stats Group ICF Matrix Recommendation

Sequence VIII Correction Factor Matrix, RO 1009-1 Intro, and Bearing Batch Intro

STATS GROUP SEPTEMBER 2023

Stats Group

- Amanda Stone, Afton
- Amy Ross, Valvoline
- Ricardo Affinito, Chevron Oronite
- Jo Martinez, Chevron Oronite
- Todd Dvorak, Infineum
- Martin Chadwick, Intertek
- Phil Scinto, Lubrizol
- Seth Demel, Shell
- Travis Kostan, SwRI
- Richard Grundza, TMC

Executive Summary

General Comments:

- The new bearing batch can be accepted.
- A lot of assumptions have been made with little data. We should re-evaluate soon once additional data becomes available. <u>Bearing Weight Loss:</u>
- Option #1:
 - Apply an industry correction factor of -4.9 mg for tests moving forward.
 - 1009-1 will have an LTMS mean of 14.9 mg and a standard deviation of 3.01 mg.
 - This is the option to choose if you think the bearings might be more severe and we should only consider a re-blend difference on the same hardware.
- Option #2:
 - Apply an industry correction factor of -3.6 mg for tests moving forward.
 - 1009-1 will have an LTMS mean of 16.2 mg and a standard deviation of 3.01 mg.
 - This is the option to choose if you believe the new bearings are the same and we can use all data to estimate the difference due to the oil re-blend.
- Based on the methodology used, with both options there is some evidence that this may slightly over correct candidates < 10 mg and may under correct candidates > 20 mg (no candidate data offered > 20 mg to study).
- Severity adjustment standard deviation should be updated from 4.8 to 3.0.

Stripped Viscosity:

- It is recommended to apply and industry correction factor of -0.14 cSt for tests moving forward.
- 1009-1 is recommended to have an LTMS mean of 9.73 cSt and a standard deviation of 0.07 cSt.

Bearing Weight Loss (BWL)

BWL Since 2018

The dashed lines are the oil targets, and all data is shown for operationally valid tests only.



A3-5

Timeline

- <u>December 2022 January 2023:</u>
 - Both labs starting producing 1006-2 results > 25.
- January 2023 April 2023:
 - More than 20 experimental runs in total were conducted between the two labs varying parts, fuel, and oil retains on 1006-2 to try to return severity to a normal level with no success (both labs averaged slightly over 30 mg.
 - Two tests on 1009-1 resulted in 17.4 mg and 18.7 mg and one test on 704-1 of 12.5 suggested that the test was indeed severe but not as bad for oils with a lower target performance.
- <u>May 2023:</u>
 - With 704-1 nearly depleted, SP agreed to run two 1009 tests to determined the feasibility of introducing 1009-1 as a reference oil moving forward. (results were 18.3 and 16.4).
- June 2023:
 - SP agrees to run the rest of the stats group matrix (an additional 8 runs), which is shown on the following slide.

TOTAL BEARING WEIGHT LOSS Unit of Measure: mg CRITICAL PARAMETER

Reference Oil	Mean Standard Deviation	
704-1	8.3	2.32
1006	15.9	4.85
1006-2	17.5	4.23

Sequence VIII Reference Oil Targets					
		Effective Dates		TBWL	
Oil	n	From ¹	To ²	$\overline{\mathbf{X}}$	s
1009	5	1-7-03	1-23-05	12.8	2.00
	11	1-24-05	5-21-21	13.8	2.14

Test Matrix

The matrix below was the recommended matrix. The data generated from these tests, and possibly including some of the previously generated data, could be used to:

- 1. Estimate an industry correction factor.
- 2. Introduce 1009-1 as the sole reference oil moving forward (704-1 supply depleted).
- 3. Prove-out the 03-22 bearing batch.

A1	A2	B1	B2
<mark>1009</mark>	<mark>704-1</mark>	<mark>1009</mark>	<mark>1009-1</mark>
<mark>704-1</mark>	<mark>1009-1</mark>	<mark>704-1</mark>	<mark>704-1</mark>
<mark>1009-1</mark>	<mark>1009-1</mark>	<mark>1009-1</mark>	<mark>1009-1</mark>

- Yellow highlighted = 06-16 (current) bearing batch
- Green highlighted = 03-22 (new) bearing batch

Test Matrix

During the test matrix, there was a higher than normal result on the second run in stand B1 producing 16.5 mg BWL. Following this test, clear mechanical wear was seen on the third run in the stand. A couple of additional runs were made on the stand which also exhibited mechanical wear, and the lab has requested to have the analysis completed without the final data point from this stand.

A1	A2	B1	B2
1009 🗸	<mark>704-1</mark> 🗸	<mark>1009</mark> 🗸	<mark>1009-1</mark> 🗸
<mark>704-1</mark> 🗸	<mark>1009-1</mark> 🗸	704-1 ?	<mark>704-1</mark> 🗸
1009-1 🗸	1009-1 🗸	1009-1 X	<u>1009-1</u> ✓
Other recent data			
A1	A2	B1	B2
<mark>1009-1</mark>		<mark>1009-1</mark>	<mark>704-1</mark>

Requested Matrix

- Yellow highlighted = 06-16 (current) bearing batch
- Green highlighted = 03-22(new) bearing batch

Bearing Batch

It is unclear if the new bearing batch is different at this time, but the current estimated difference is 3.1 mg. It is not recommended to add in this difference at this time as an additional contribution to the ICF.



1009-1 vs. 1009

Using data generated only on identical hardware for the estimated re-blend difference results in a target update to 14.9 mg. Using all data on 1009-1 results in a target update of 16.2.



Correction Factor Using 16.2 Target for 1009-1

To estimate an ICF we consider all data and 1009-1 only. It is recommended to use the 1009-1 only difference of 3.6 mg as the ICF. Though 1009-1 is further from target than 704-1, it is less than the difference seen in 1006-2. This suggests we might slightly over correct candidates < 10 mg (solid passes anyway), but may potentially under correct candidates > 20 mg.



1009-1 Data After Correction Factor of -3.6 mg

The graph below shows the data after the -3.6 mg correction factor, along with the Shewhart severity upper and lower limits.



Correction Factor Using 14.9 Target for 1009-1

To estimate an ICF we again consider all data and 1009-1 only. It is recommended to use the 1009-1 only difference of 4.9 mg as the ICF.



1009-1 Data After Correction Factor of -4.9 mg

The graph below shows the data after the -4.9 mg correction factor, along with the Shewhart severity upper and lower limits.



Model Predictions

VIF 2.5 2.7

1.2 1.1 1.6 1.1

summa	агу от г	π					
		0.000010					
RSquare Adj 0		0.796039					
Root Me	an Squar	e Error	2.282551				
Mean of	Respons	e	16.43846				
Observat	tions (or !	Sum Wgts)	13				
Analys	is <mark>of</mark> Va	riance					
		Sum of					
Source	DF	Squares	Mean Squa	are	F Rat	io	
Model	6	275.27055	45.87	84	8.80	58	
Error	6	31.26022	. 5.21	00	Prob >	F	
C. Total	12	306.53077			0.009	0*	
Parame	eter Est	imates					
Term			Estimate	Sto	d Error	t Ratio	Prob> t
Intercept			15.821271	0.7	737952	21.44	<.0001*
IND[704	I-1]		-6.428374	1.1	124845	-5.71	0.0012*
IND[100	9]		2.3765474	1	.41269	1.68	0.1435
LTMSLAB[A]		-0.677796	0.0	684935	-0.99	0.3606	
LTMSLABIAI:LTMSAPP[4]		-0.231432	0.9	909695	-0.25	0.8077	
LTMSLA	BIBI:LTMS	APP[3A]	1.4642058	1.1	192468	1.23	0.2655
IND[100	9-1]:BEA	RBAT[06-16	-1.398098	0.9	909695	-1.54	0.1752
Effect 1	Tests						

			Sum of		
Source	Nparm	DF	Squares	F Ratio	Prob > F
IND	2	2	260.05529	24.9571	0.0012*
LTMSLAB	1	1	5.10200	0.9793	0.3606
LTMSAPP[LTMSLAB]	2	2	7.89162	0.7573	0.5090
BEARBAT[IND]	1	1	12.30622	2.3620	0.1752



Least Squa	are	s Means									
Level		Lea Sq Mea	st an Lower	9 5%	Upp	er 95%					
[704-1]06-1	6	9	.4	6.2		12.5					
[1009] 06-16		18	.2	13.8		22.6					
[1009-1] 06-	16	18	.5	15.7		21.3					
[1009-1]03-	22	21	.3	17.8		24.7					
			5								
Level	- Le	vel	Difference	Std Er	r Dif	Lower CL	Upper CL	p-Value	-5	0	
[1009-1] 03-22	[70	4-1] 06-16	11.87830	1.76	0790	5.78296	17.97364	0.0021*			
[1009-1] 06-16	[70	4-1] 06-16	9.08210	1.72	0614	3.12584	15.03836	0.0075*			
[1009] 06-16	[70	4-1] 06-16	8.80492	2.38	4935	0.54898	17.06087	0.0384*			
[1009-1] 03-22	[100)9] 06-16	3.07338	2.42	8521	-5.33345	11.48020	0.6134		_	-
[1009-1] 03-22	[10	09-1] 06-16	2.79620	1.81	9390	-3.50200	9.09439	0.4739			-
[1009-1] 06-16	[100	09] 06-16	0.27718	2.13	2058	-7.10338	7.65774	0.9991		_ _	

🛛 💌 Contrast							
⊿ Test Detail	⊿ Test Detail						
[704-1] 06-16	0						
[1009] 06-16	0.5						
[1009-1] 06-16	0.5						
[1009-1] 03-22	-1						
Estimate	-2.935						
Std Error	1.8621						
t Ratio	-1.576						
Prob> t	0.1661						
SS	12.941						
Lower 95%	-7.491						
Upper 95%	1.6217						
SS NumDF	DenDF	F Ratio	Prob > F				
12.94 1	6	2.4839	0.1661				

Current 1009 target: 13.8

Difference between 1009 and 1009-1 for 06-16 bearing batch = 0.3 1009-1 new target: 14.1

Difference between 1009 06-16 and current target: -4.4

Difference between 06-16 and 03-22 batch: -2.9

ICF = -7.3

10 15

Model Predictions

BWL (VIII) Correction/Targets Evaluation



Prediction Profiler

 Data Used: All 1009 & 1009-1 Data (Matrix) + 2 Tests 1009-1
resulted in 17.4 mg and 18.7 mg (01/23 – 04/23)
 Model Used: BWL ~ IND + BEARBAT[IND]
• 1009 LSMeans = Mean = 17.4 mg, SD (assume 1009 = 1009-1) = 2.6 mg
 ICF (based on 1009) = 13.8 mg - 17.4 mg = -3.6 mg
• 1009-1 LSMeans = 20.0 mg = 17.4 mg + 2.6 mg (unadjusted)
• 1009-1 After ICF = 20.0 mg – 3.6 mg = 16.4 mg (unadjusted)

ICF = -3.6 mg, 1009-1 LTMS mean = 16.4 mg, SD = 2.6

10 Hour Stripped Viscosity

SVIS Since 2018

10-HOUR STRIPPED VISCOSITY Unit of Measure: centistokes NONCRITICAL PARAMETER

Reference Oil	Mean	Standard Deviation
704-1	10.27	0.11
1006	9.00	0.17
1006-2	9.37	0.07
1009	9.51	0.10

10.6 IND • 704-1 10.4 • 1006-2 10.2 10.0 SVIS 9.8 9.6 9.4 9.2 **LTMSDATE**

SVIS also increased at the same time as bearing weight loss with 1006-2.

1009-1 vs. 1009

Consider the difference of the re-blend first. The re-blend data on both bearing batches is similar and shows an average difference from the original blend of 0.22 cSt, resulting in a target of 9.73 cSt.



Correction Factor

Modeling lab and stand differences seems inappropriate on the current data set. To estimate an ICF for the 06-16 bearings, we can take the average difference from target of all 6 results (recommended), or we can take an average of the two average differences.



1009-1 Data After Correction Factor of -0.14 cSt

The graph below shows the data after the -0.14 cSt correction factor, along with the Shewhart severity upper and lower limits.



Model Predictions

1.1 1.1 1.4

⊿ Sumn	nary of	Fit								
RSquar RSquar	e e Adj	_	0.976 0.948	565 444						
Root M Mean o Observ	lean Squar of Respons ations (or	re Error se Sum Wats)	0.066 9.973	237 333 12						
⊿ Analy	sis of V	ariance								
Source	DF	Sum o Square	of s Mea	an Soua	are	F Rat	io			
Model	6	0.9141302	1	0.1523	355	34.72	64			
Error	5	0.0219364	6	0.0043	887	Prob >	F			
C. Tota	11	0.9360666	7			0.000	6*			
⊿ Paran	neter Es	timates								
Term			Es	timate	Ste	d Error	t Rat	io	Prob> t	VIF
Interce	pt		9.9	717535	0.0	022449	444.	19	<.0001*	
IND[70	04-1]		0.4	268924	4 0.034267		12.	46	<.0001*	2.3
IND[10	09]		-0.3	318628	0.0	041136	-7.	75	0.0006*	2.7
LTMSL	AB[A]		0.0	279688	0	.02056	1.	36	0.2318	1.1
LTMSL	AB[A]:LTM	ISAPP[4]	0.0	298438		0.0264	1.	13	0.3096	1.1
LTMSL	AB[B]:LTM	ISAPP[3A]	0.04	460937	0	.03529	1.	31	0.2484	1.4
IND[10)09-1]:BE4	ARBAT[03-2	2] -0	.00151		0.0264	-0.	06	0.9566	1.1
⊿ Effect	t Tests									
				S	um o	of				
Source	•	Nparm	n DF	Sq	uare	es Fl	Ratio	Pr	ob > F	
IND		1	2 2	0.706	55393 80.52		5228	0	.0002*	
LTMSL	LTMSLAB 1				1185	50 1.	8505	C	.2318	

LTMSAPP[LTMSLAB]



2 2 0.01511452 1.7225 0.2697

Least So	quare	es M	leans T	able			
			Least	:			
Level		S	q Mean	Lowe	r 95%	Upper	95%
[704-1] 0	6-16		10.40)	10.29	1	0.50
[1009] 06	-16		9.65		9.52		9.79
[1009-1]	06-16		9.87	,	9.78		9.95
[1009-1]	03-22		9.86		9.76		9.97
evel	- Level		Difference	Std Frr Dif	Lower (linner (l	n-Value
704-1106-16	- Level	5-16	0 7455208	0.0705791	0.48508	3 1.005959	0.0005
704-1106-16	[1009-1]	03-22	0.5366667	0.0540820	0.33710	3 0.736230	0.0007
704-1106-16	[1009-1]	06-16	0.5336458	0.0527992	0.33881	6 0.728476	0.0006
1009-1] 06-16	[1009] 06	5-16	0.2118750	0.0619587	-0.016754	4 0.440504	0.0656
1009-1] 03-22	[1009] 06	5-16	0.2088542	0.0705791	-0.051584	4 0.469292	0.1061
1009-1] 06-16	[1009-1]	03-22	0.0030208	0.0527992	-0.191809	9 0.197851	0.9999
 Contra 	st						
Test De	tail						
[704-1] (06-16		0				
[1009] 06	5-16	0.	.5				
[1009-1]	06-16	0.	.5				
[1009-1]	03-22	_	1				
Estimate		-0.10	3				
Std Error		0.054	1				
t Ratio		-1 00	3				
Drobalt		0 1 1 5	1				
sc		0.115					
33 Lawar 05	0/	0.015	2				
Lower 95	%	-0.24	2				
Upper 95	%	0.036	1				
SS Nu	ImDF	DenD	F F Rat	tio Prob	> F		
0.016	1		5 3.62	13 0.1	154		

Current 1009 target: 9.51

Difference between 1009 and 1009-1 for 06-16 bearing batch = 0.211009-1 new target: 9.72

Difference between 1009 06-16 and current target: -0.14

Difference between 06-16 and 03-22 batch: -0.10

ICF = -0.24

0.2 0.4 0.6 0.8 1.0

Model Predictions

SVIS (VIII) Correction/Targets Evaluation



 Data Used: All 1009 & 1009-1 Data (Matrix) + 2 Tests 1009-1
resulted in 9.81 cSt and 9.88 cSt (01/23 – 04/23)
 Model Used: SVIS ~ IND + BEARBAT[IND]
• 1009 LSMeans = Mean = 9.65 cSt, SD (assume 1009 = 1009-1) = 0.07 cSt
 ICF (based on 1009) = 9.51 cSt – 9.65 cSt = -0.14 cSt
• 1009-1 LSMeans = 9.88 cSt = 9.65 cSt + 0.23 cSt (unadjusted)
• 1009-1 After ICF = 9.88 cSt – 0.14 cSt = 9.74 cSt (unadjusted)
 ICF = -0.14 cSt, 1009-1 LTMS mean = 9.74 cSt, SD = 0.07 cSt