

Sequence IV Surveillance Panel | MINUTES

REVISION DATE: 4/10/2018 7:57:00 AM

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|-----------------------|--|
| Relevant Test: | Sequence IVB |
| Note Taker: | Chris Mileti |
| Meeting Date: | 03-28-2018 |
| Comments: | Conference call to discuss the proposed LTMS system for the Sequence IVB test. |

1. OPEN ACTION ITEMS (B. BUSCHER):

1.1. KA24E Fuel:

- 1.1.1. The IVB procedure must be updated with instructions for mixing different batches of KA24E fuel.
- 1.1.2. The Sequence VG/VH procedure can be referenced because it includes instructions for switching to a new fuel batch.

1.2. OHT Updates:

- 1.2.1. OHT is currently manufacturing clutch alignment tools.

1.2.2. **Timing Chain Wedge and Engine Rotation Locking Tool:**

- 1.2.2.1. These two action items are still open.
- 1.2.2.2. OHT is waiting on feedback regarding the design of these tools.

1.2.3. **Thermal Barrier Coating:**

- 1.2.3.1. The Surveillance Panel is interested in possibly applying a thermal coating to components of the IVB engine that have large surface areas (oil pan and front cover).
- 1.2.3.2. OHT has not yet identified a suitable product.

1.3. Oil Consumption:

- 1.3.1. The Surveillance Panel still needs to discuss a test validity limit for oil consumption.

1.4. Oil Samples:

- 1.4.1. There is an open action item for SWRI and IAR to swap oil samples and compare analytical results.
- 1.4.2. SWRI, Exxon and Lubrizol have provided Precision Matrix oil samples to IAR for analysis.
 - 1.4.2.1. Afton provided samples from their recent prove-out testing.
 - 1.4.2.2. These samples will be re-tested by IAR to eliminate laboratory bias.

1.5. Quality Index Calculations:

- 1.5.1. The Surveillance Panel has an open action item to reevaluate the QI calculations for oil gallery temperature.

1.6. TMC Updates:

- 1.6.1. Some test reports for the Prove-Out Matrix and Precision Matrix are incomplete.

1.6.2. The TMC will send an email to each laboratory that still needs to provide data for their Industry tests.

1.7. Parameter Database:

1.7.1. The Surveillance Panel has an open action item to create a database of parameters that are believed to have a significant impact on severity.

1.7.2. One example of such a parameter would be oil gallery temperature.

1.8. Oil Temperature Histogram:

1.8.1. Lubrizol has an open action item to evaluate whether a histogram is a more appropriate way to analyze the oil gallery temperature parameter.

1.8.2. IAR will follow-up with Lubrizol.

1.9. Blowby System:

1.9.1. The IVB procedure needs to be updated with instructions for cleaning the external blowby system.

1.10. 200HR Operational Data Plots:

1.10.1. The plots from SWRI and Lubrizol are available on the TMC website.

1.10.2. IAR has almost finished compiling its plots.

1.11. Engine Build Workshop:

1.11.1. Most of the labs participated in an engine build workshop earlier in the year.

1.11.2. The Surveillance Panel needs to compile all the notes from this meeting into a single document.

1.12. Unscheduled Downtime:

1.12.1. The IVB procedure needs to be updated with instructions about how to handle extended periods of unscheduled downtime.

1.12.2. These instructions need to reduce the likelihood of oxidation on camshafts and lifters.

1.13. Anomalous Operational Parameters:

1.13.1. The Surveillance Panel needs to further analyze the four anomalous operational parameters identified by Lubrizol.

1.13.2. Parameter List:

1.13.2.1. Exhaust Gas Temperature

1.13.2.2. Crankcase Pressure / Blowby Flow Rate

1.13.2.3. Intake Manifold Pressure

1.13.2.4. AFR

1.14. Appendix K:

1.14.1. Appendix K needs to be updated for the Sequence IVB test.

2. STATISTICAL ANALYSIS OF OPERATIONAL DATA (STATISTICS GROUP):

2.1. Background:

2.1.1. The Statistics Group conducted another analysis of Precision Matrix operational data (dated 03-20-2018).

2.1.2. The focus of this analysis was on exhaust gas temperature, AFR, intake manifold pressure and crankcase pressure.

2.1.3. A partial least squares analysis was used on all (28) Precision Matrix tests.

2.2.Slide #3:

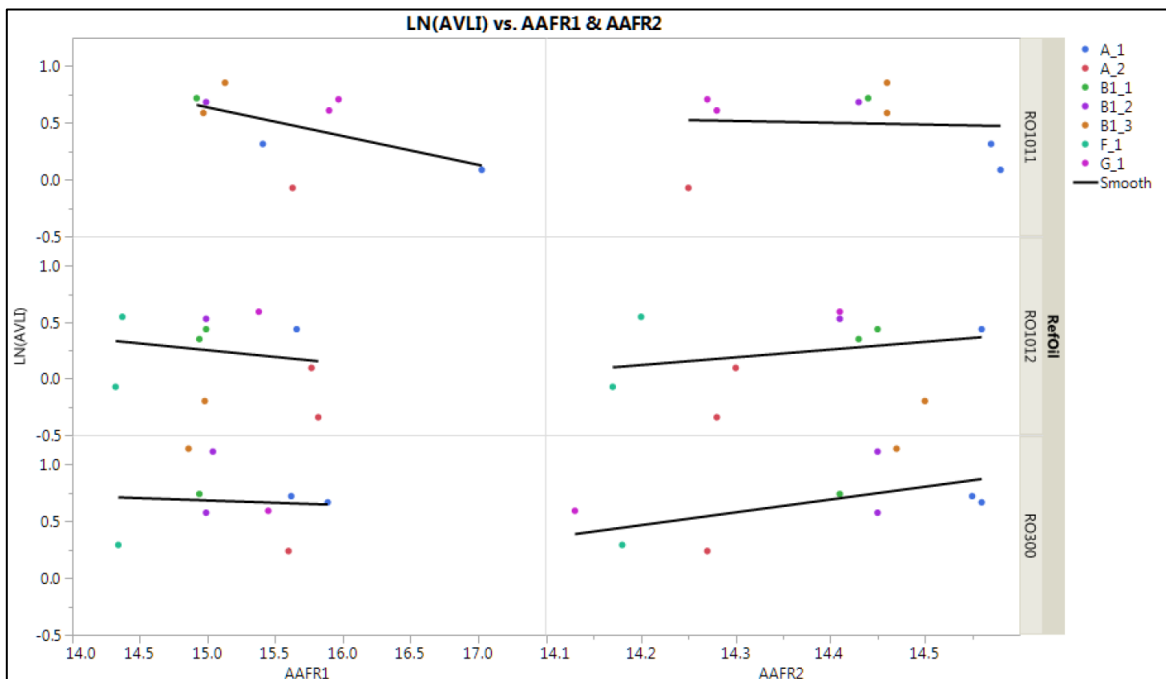
Statistical Analysis of Operational Data

- Due to multicollinearity, a Partial Least Squares (PLS) Analysis was performed on the data set
- PLS analysis results (*with 2 latent variables*) for centered and scaled data are summarized below (and sorted by their centered and scaled coefficients):

| Rank | Term | Coefficient (Centered & Scaled) |
|------|-----------|------------------------------------|
| 1 | A-2 | -0.3198 |
| 2 | I012 | -0.2625 |
| 3 | 300 | 0.2378 |
| 4 | ABLOWBY1 | 0.1554 |
| 5 | AAFR1 | -0.1487 |
| 6 | B1-2 | 0.1337 |
| 7 | G-1 | 0.1286 |
| 8 | AMAP1 | 0.1065 |
| 9 | AAFR2 | 0.0828 |
| 10 | AMAP2 | -0.0764 |
| 11 | ACCASEP2 | 0.075 |
| 12 | B1-1 | 0.0621 |
| 13 | ABLOWBY2 | 0.0612 |
| 14 | B1-3 | 0.0535 |
| 15 | F-1 | -0.0342 |
| 16 | ACCASEP1 | 0.0332 |
| 17 | I011 | 0.0315 |
| 18 | A-1 | -0.0256 |
| 19 | AEXHT1 | -0.0241 |
| 20 | AEXHT2 | 0.0132 |
| 21 | Intercept | 0 |

2.2.1. The average Stage 1 blowby and AFR parameters are interesting.

2.3.Slide #5:



2.3.1. The rows in the chart correspond to different reference oils.

2.3.2. The Surveillance Panel needs to decide whether tighter controls should be implemented on the parameters of interest (particularly AFR and blowby).

2.3.3. Buscher requested that each laboratory review this analysis and be prepared to provide feedback during the next meeting.

3. STATISTICAL ANALYSIS OF IRON PARAMETER (STATISTICS GROUP):

3.1. Background:

3.1.1. The Statistics Group conducted an analysis of the iron parameter (dated 03-26-2018).

3.1.2. Iron is measured in the oil drain samples.

3.2. Slide #3:

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- This analysis includes the results of 28 valid precision matrix tests
- Data supports the use of Ln(FEWMEOT) transformation
 - Borderline statistical significant oil difference: 1012 < 300
 - Lab differences are statistically significant (A < B1)
 - Stand within Lab differences are not statistically significant
- Oil discrimination is more significant for FEWMEOOT than FEWML25 (Fe increase over last 25 hours) and FEWML50 (Fe increase over last 50 hours).
- Oil discrimination is more significant with the Calcium Adjustment of the FEWMEOOT data
- FEWMEOOT can be affected by dilution factors such as fuel, water, volatility, etc.
 - Calcium content is lower at EOT as compared to SOT
- FEWMEOOT adjusted using calcium data may be a more preferred approach. However, this approach may contain more error as it is based on multiple (ICP) measurements of Calcium data.
 - Adopting a procedure such as the IIIGB/IIIHB may reduce the error associated with the calcium based adjustment
 - Possible concern - candidate oils may not be calcium based
- Correlation between sqrt(AVLI) and Ln(FEWMEOT) or Ln(FEWMEOT_Ca_Adj) is high (indicating parameter redundancy).

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3.2.1. Several months ago, the Statistics Group analyzed several key parameters from the Precision Matrix data set.

3.2.1.1. AVLI (average intake lifter volume loss) demonstrated the best discrimination.

3.2.2. The Statistics Group recently revisited the iron parameter.

3.2.2.1. The N=21 and N=28 data sets were both used in the analysis.

3.2.2.2. However, the Executive Summary deals exclusively with the N=28 analysis.

3.2.3. Iron demonstrates oil discrimination that is borderline statistically significant.

3.2.4. Lab differences with iron are statistically significant.

3.2.4.1. For example, Lab B1 is more severe than Lab A.

3.2.5. Rate-of-Change of Iron:

3.2.5.1. The statisticians also looked at the rate-of-change of the iron parameter during the last 50-hours of the test and the last 25-hours of the test.

3.2.5.2. The statisticians confirmed that the rate-of-change of iron provides less discrimination than the end-of-test iron.

3.2.6. Iron vs. Engine Hours:

3.2.6.1. There is not a clear correlation between iron loss and engine hours.

3.2.6.2. The 1st run on an engine generally exhibits the most iron generation.

3.2.6.3. The 2nd run on an engine generally exhibits the lowest iron generation.

3.2.6.4. The statisticians will need more data (including data from tests with higher engine hours) before they can recommend a correction factor.

3.2.7. Calcium Adjustment:

3.2.7.1. Oil discrimination with end-of-test iron did improve when a calcium adjustment was applied.

3.2.7.2. However, there are some challenges to applying a calcium adjustment.

3.2.7.3. The IVB may need to adopt an iron analysis procedure that is like the one used for the Sequence IIIG/H.

3.3. Slide #4:

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- Estimated within a stand test precision (r ; ASTM repeatability)
 - $\text{Ln}(\text{FEWMEOT}) = 0.7487$
- Estimated test precision across labs and stands (R ; ASTM reproducibility)
 - $\text{Ln}(\text{FEWMEOT}) = 0.9496$
- Oil means and standard deviations

| Oil | Number of Tests | Target Mean $\text{Ln}(\text{FEWMEOT})$ | Target Mean FEWMEOT | Target Standard Deviation $\text{Ln}(\text{FEWMEOT})$ |
|------|-----------------|--|------------------------|--|
| 300 | 9 | 5.2500 | 191 | 0.4067 |
| 1012 | 10 | 4.9249 | 138 | 0.3365 |
| 1011 | 9 | 5.0258 | 152 | 0.2722 |

- Same concerns with AVLI are seen in Fe analysis (Two high results on Oil 300 influence oil discrimination, discrimination not consistent among stands, test precision is large compared to the observed range of measurements)

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3.3.1. Concerns:

3.3.1.1. The statisticians have the same concerns with the iron parameter that they do with the AVLI parameter.

3.3.1.2. There are two severe results with REO300 that are driving oil discrimination.

3.3.1.3. Oil discrimination is not consistent among test stands.

3.3.1.4. There is a lot of overlap in the results for the three reference oils.

3.3.2. Comments from Toyota:

3.3.2.1. The increase in the rate-of-change of iron at the end of each test may be due to oil degradation.

3.3.2.2. Adding iron as a secondary parameter will provide protection against unusually performing oils.

3.3.2.3. Additional data collected during the Technology Demonstration period will aid in this analysis.

3.4. Slide #5:

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- Estimated within a stand test precision (r; ASTM repeatability)
 - $\text{Ln}(\text{FEWMEOT_Ca_Adj}) = 0.7162$
- Estimated test precision across labs and stands (R; ASTM reproducibility)
 - $\text{Ln}(\text{FEWMEOT_Ca_Adj}) = 0.9410$
- Oil means and standard deviations

| Ref. Oil | Number of Tests | Target Mean Ln(FEWMEOT_Ca_Adj) | Target Mean FEWMEOT | Target Standard Deviation Ln(FEWMEOT_Ca_Adj) |
|----------|-----------------|-----------------------------------|------------------------|--|
| 300 | 9 | 5.3987 | 221 | 0.3967 |
| 1012 | 10 | 5.0581 | 157 | 0.3277 |
| 1011 | 9 | 5.1648 | 175 | 0.2863 |

- Same concerns with AVLI are seen in Fe analysis (Two high results on Oil 300 influence oil discrimination, discrimination not consistent among stands, test precision is large compared to the observed range of measurements)

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3.4.1. The final calcium level is lower than the initial calcium level for all the Precision Matrix tests.

3.4.1.1. This supports the theory that the oil becomes diluted during the test.

3.5. Slide #7:

Reference Oil Discrimination Comparison

The table below compares the numbers of standard deviations of separation between the highest and lowest reference oil across GF-6 test types. The median of other tests is approx. 3.55 and the mean (without PHOS) is 3.99.

| Test | Parameter | Oil 1 | Oil 2 | Range | Test s _r | SDs of Separation |
|-----------|--------------------|----------|----------|--------|---------------------|-------------------|
| IIH | Ln(PVIS) | 4.7191 | 3.3289 | 1.3902 | 0.4641 | 3 |
| IIH | WPD | 4.63 | 3.66 | 0.97 | 0.47 | 2.1 |
| IIHA | Ln(MRV) | 11.1107 | 9.7854 | 1.3253 | 0.4214 | 3.1 |
| IIHB | PHOS | 94.15 | 78.92 | 15.23 | 1.53 | 10 |
| VIE | FEI 1 | 2.56 | 1.3 | 1.26 | 0.29 | 4.3 |
| VIE | FEI 2 | 1.82 | 1.41 | 0.41 | 0.12 | 3.4 |
| VIF | FEI 1 | 2.23 | 1.45 | 0.78 | 0.21 | 3.7 |
| VIF | FEI 2 | 2.25 | 1.41 | 0.84 | 0.19 | 4.4 |
| IX (LSPI) | Sqrt(AvPIE + 0.5) | 4.2644 | 3.3819 | 0.8825 | 0.2856 | 3.1 ^{*1} |
| VH | AES | 8.43 | 6.47 | 1.96 | 0.5 | 3.9 |
| VH | Ln(10-RCS) | 0.9155 | -0.5294 | 1.4449 | 0.2194 | 6.6 |
| VH | AEV50 | 9.26 | 8.77 | 0.49 | 0.25 | 2 |
| VH | APV50 | 8.67 | 7.35 | 1.32 | 0.53 | 2.5 |
| X (CW) | Ln(CHST) | -2.10574 | -2.63174 | 0.526 | 0.14148 | 3.7 ^{*2} |
| IVB | Sqrt(AVLI) | 1.3931 | 1.1543 | 0.2388 | 0.168 | 1.4 |
| IVB | Ln(FEWMEOT) | 5.25 | 4.9249 | 0.3251 | 0.2701 | 1.2 |
| IVB | Ln(FEWMEOT_Ca_Adj) | 5.3987 | 5.0581 | 0.3406 | 0.2584 | 1.3 |

*1: Oil 220 not used as a reference oil. Including this oil would yield approx. 12 SDs of separation between 220 and 222.

*2: 271 vs. 1011

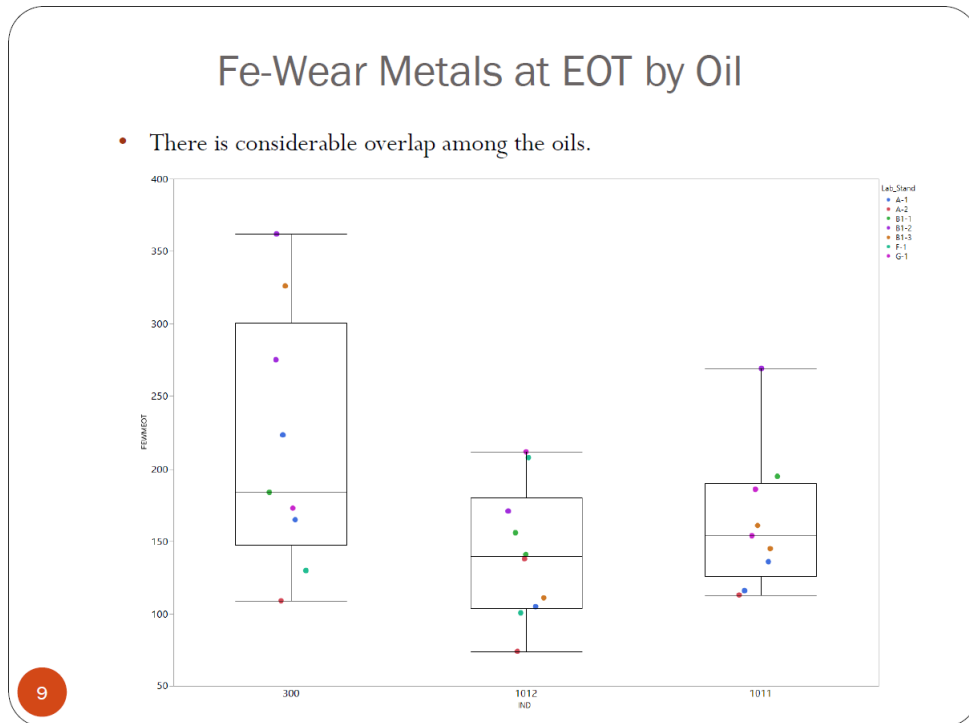
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3.5.1. The Sequence IVB parameters are shown in yellow.

3.5.2. These parameters are separated by standard deviations that range between 1.2 and 1.4.

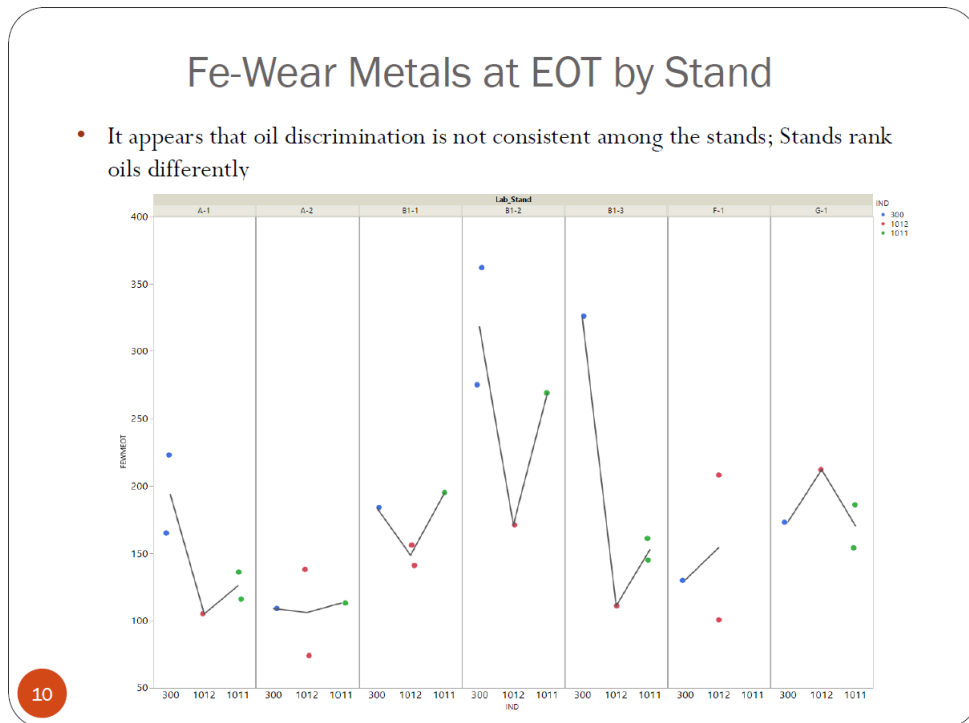
3.5.2.1. These are the lowest standard deviations of any GF-6 test.

3.6. Slide #9:



- 3.6.1. The best discrimination is exhibited between REO300 and REO1012.
- 3.6.2. There is still significant overlap between all three oils.

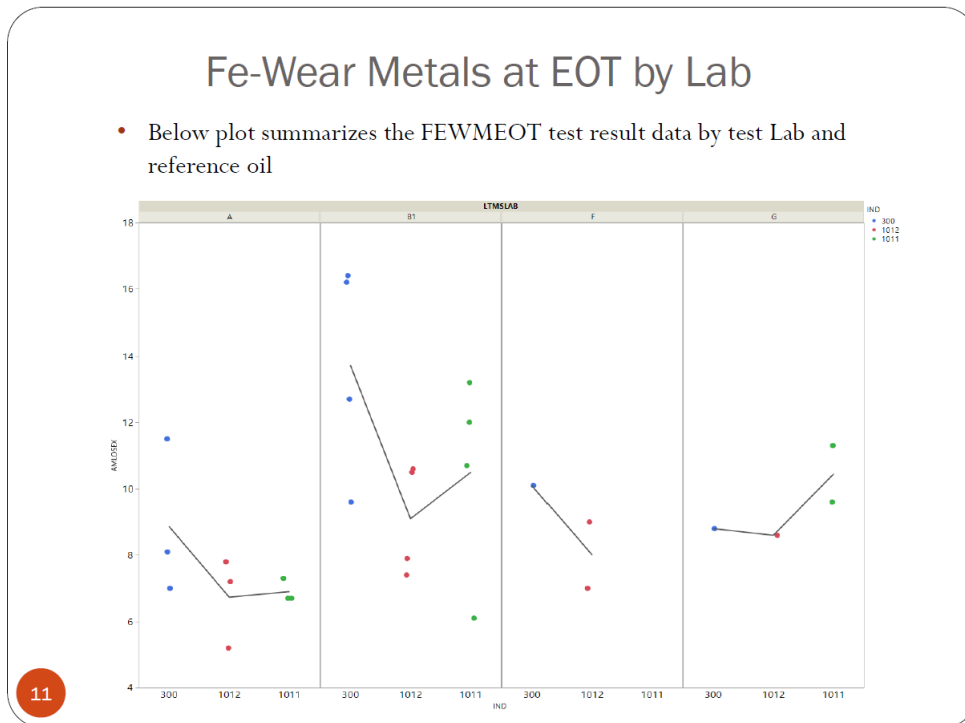
3.7. Slide #10:



- 3.7.1. The oil vs. wear pattern is different between test stands.
- 3.7.2. Some stands have a "V" pattern and some have an inverted "V" pattern.
- 3.7.3. The line for stand F-1 is flat.
- 3.7.4. The legs on some "V" patterns are longer than on others.

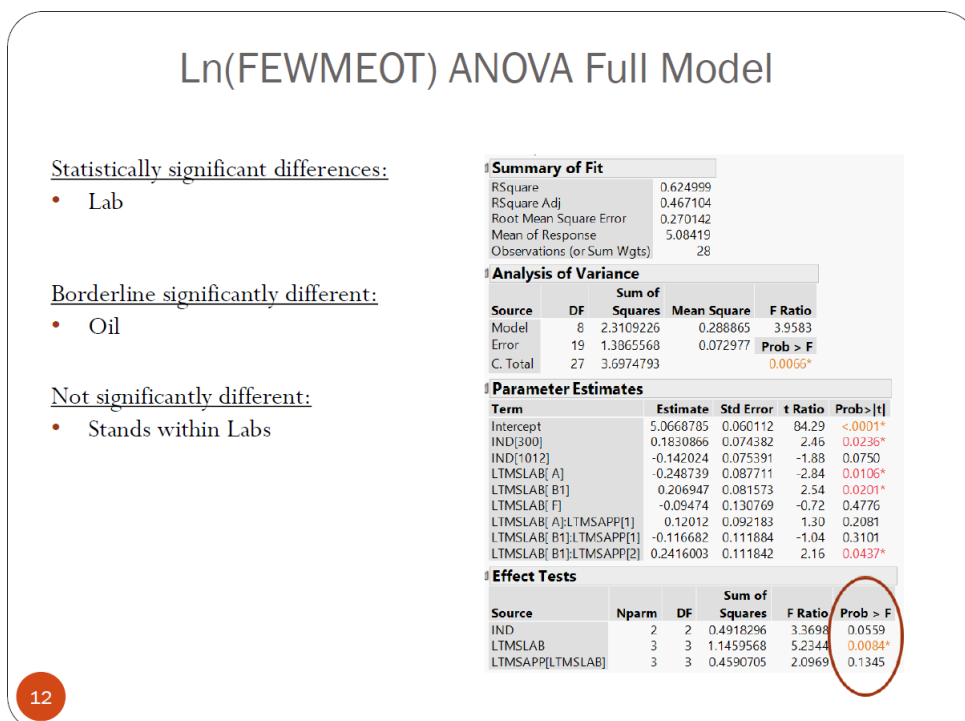
3.7.5. A-2 is the mildest stand while B1-2 is the most severe.

3.8.Slide #11:



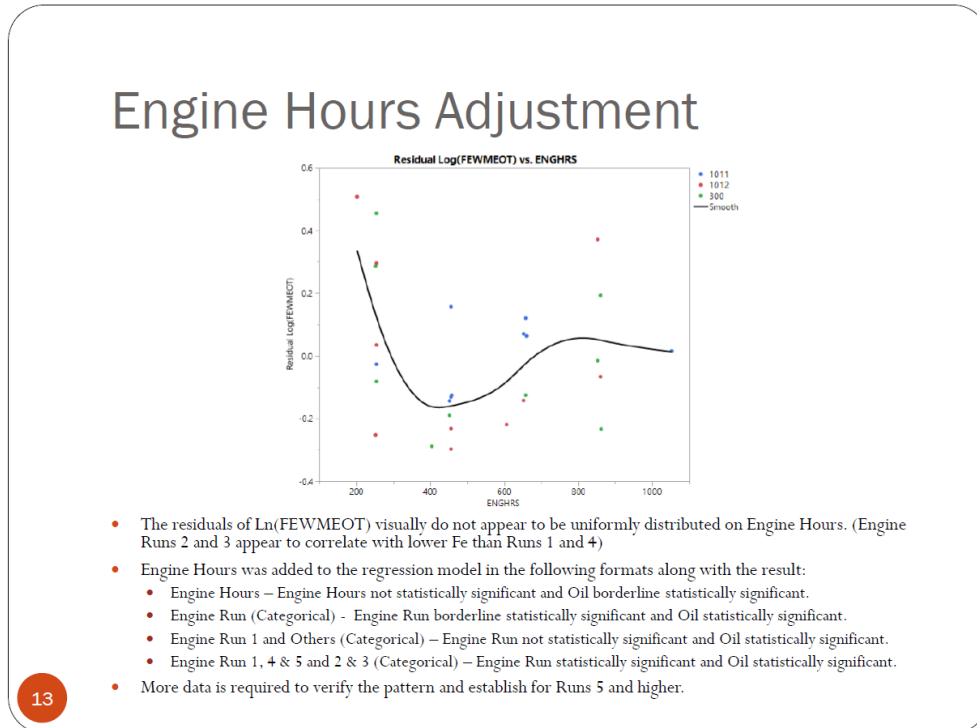
- 3.8.1. Lab A has a relatively flat profile.
- 3.8.2. Lab B1 has a “check mark” shaped profile.
- 3.8.3. Lab F has a decreasing profile (only two oils were run during the Precision Matrix).
- 3.8.4. REO300 and REO1012 yielded almost identical results at Lab G.

3.9.Slide #12:



- 3.9.1. The laboratories are statistically different.
- 3.9.2. The stands within a single lab do not appear to be statistically different.
- 3.9.3. **IMPORTANT NOTE:** None of this iron data has been adjusted for calcium.

3.10. Slide #13:



- 3.10.1. The 1st run on an engine generates the highest end-of-test iron.
- 3.10.2. The 2nd run on an engine generates the lowest end-of-test iron.
- 3.10.3. The 3rd and 4th runs on an engine generate more wear than the 2nd run.
- 3.10.4. The statisticians were hoping to see a linear relationship between the residual and engine hours.

3.10.5. Intertek's Comments about Engine Longevity:

- 3.10.5.1. Most of the labs are running a given engine and cylinder head combination for up to six runs.
- 3.10.5.2. IAR has performed cylinder head swaps.
 - 3.10.5.2.1. They found that this will extend engine longevity to approximately 8-9 runs.
 - 3.10.5.2.2. At (9) runs, the engines must be decommissioned for excessive oil consumption.

3.10.6. Comments from Statisticians:

- 3.10.6.1. They need more data before they can recommend an engine hour adjustment.
 - 3.10.6.1.1. This would include data generated on an engine after a cylinder head change.
 - 3.10.6.1.2. Ideally, it would also include 8th or 9th run data.
- 3.10.6.2. There is a consensus within the Statistics Group that an engine hour adjustment is needed for the iron parameter.
- 3.10.6.3. They may need to revisit the AVLI parameter (to determine if there is an engine hour effect) once additional data is available.

3.10.7. Comments from Toyota:

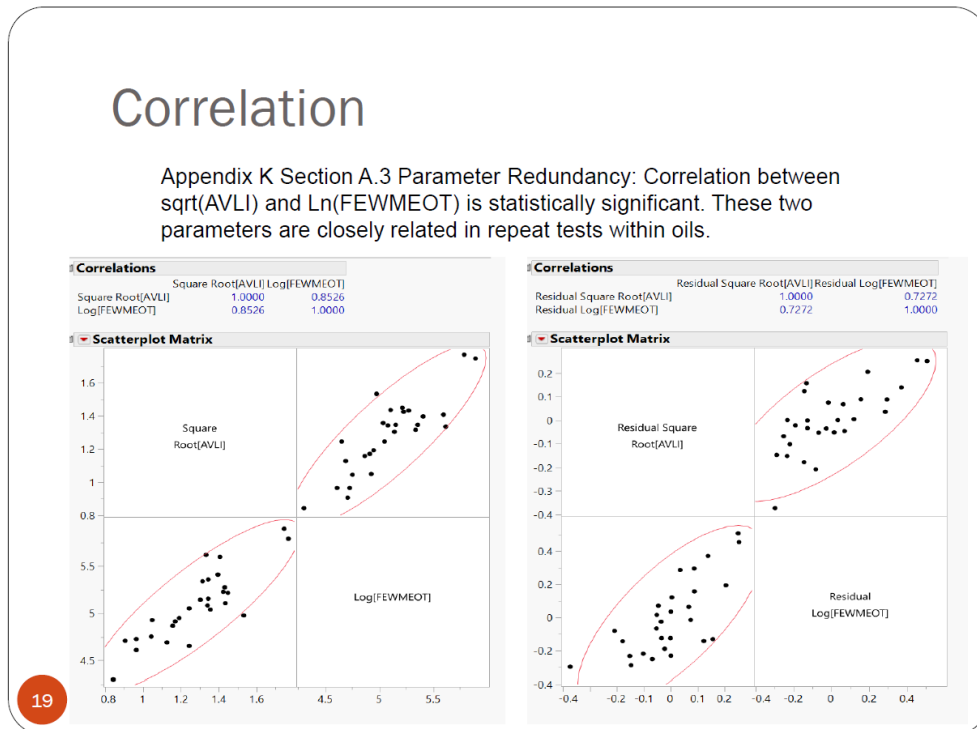
- 3.10.7.1. Toyota is not surprised to see that the 1st run on an engine delivers the highest end-of-test wear.
 - 3.10.7.1.1. The first run occurs right after the break-in.

- 3.10.7.1.2. IAR noted that the break-in does not generate much iron.
- 3.10.7.2. The proposed iron pass/fail limit is intended to screen out high wear oils only.
- 3.10.7.2.1. All the reference oils would pass if the limit were set at 400ppm.

3.10.8. Carry-Over Effect:

- 3.10.8.1. Both Lubrizol and Exxon are concerned about a “carry-over” effect.
- 3.10.8.2. Exxon noted that there is no “carry-over” effect with procedures like the Sequence III because the engine is rebuilt after each test.
- 3.10.8.3. Lubrizol noted that wear in areas of the engine other than the rings and bore can lead to a “carry-over” effect.
 - 3.10.8.3.1. For example, deformed valve stems may be causing excessive lifter button wear.
 - 3.10.8.3.2. Toyota responded that AVLI correlates well to weight loss.
 - 3.10.8.3.2.1. This indicates that most of the weight loss is coming from the wear surface of the lifter in most cases.
- 3.10.8.4. IAR noted that timing chains may have a “carry-over” effect as well.
- 3.10.8.5. There was a consensus within the group that an end-of-test checklist is needed to confirm that the engine was not damaged.
 - 3.10.8.5.1. IAR uses a similar checklist whenever they run a high wear oil.

3.11. Slide #19:



- 3.11.1. There is a very strong correlation between AVLI and iron.
 - 3.11.1.1. This a concern if both are considered primary parameters.

3.11.2. Comments from TMC:

- 3.11.2.1. They are not sure how to handle iron in LTMS if it is a secondary parameter.
- 3.11.2.2. This parameter may require Y_i charts without severity adjustments.
- 3.11.2.3. Ultimately, this is a decision that should be made by the Surveillance Panel.

3.12. Slide #21:

Fe-Wear Metals - Correction Approach

- Method Summary:
 - Calcium concentration is believed to remain constant from SOT to EOT
 - Reference ASTM 7320 - Sequence IIIIGB for more information
 - Changes in Ca levels can be due to volatility or dilution (i.e. fuel, water, etc.)
 - Ratio of (Ca_SOT/Ca_EOT) is used to correct the FEWMEOT data to equivalent SOT levels
 - Example of correction calculations are provided below

| TESTKEY | LTMESLAB | Stand | RefOil | ENGRHS | FEWMEOT | Ca_SOT | Ca_EOT | Ca_SOT/Ca_EOT | FEWMEOT_Ca_Adj | AVLI |
|------------|----------|-------|--------|--------|---------|--------|--------|---------------|----------------|------|
| 127173-IVB | B1 | S1 | RO1012 | 254 | 156 | 2400 | 2168 | 1.1070 | 172.7 | 1.55 |
| 129759-IVB | B1 | S2 | RO300 | 254 | 275 | 2029 | 1781 | 1.1392 | 313.3 | 1.78 |
| 125079-IVB | B1 | S3 | RO1011 | 254 | 161 | 2111 | 1861 | 1.1343 | 182.6 | 1.8 |
| 125882-IVB | A | S2 | RO1012 | 252 | 74 | 2449 | 2163 | 1.1322 | 83.8 | 0.71 |
| 129752-IVB | A | S1 | RO300 | 252 | 223 | 2076 | 1773 | 1.1709 | 261.1 | 1.95 |
| 129762-IVB | B1 | S1 | RO1011 | 456 | 195 | 2107 | 1805 | 1.1673 | 227.6 | 2.05 |
| 129766-IVB | B1 | S2 | RO1012 | 456 | 171 | 2439 | 2058 | 1.1851 | 202.7 | 1.7 |
| 129767-IVB | B1 | S3 | RO1012 | 456 | 111 | 2419 | 2035 | 1.1887 | 131.9 | 0.82 |
| 130948-IVB | A | S2 | RO300 | 452 | 109 | 2069 | 1783 | 1.1604 | 126.5 | 1.27 |
| 129760-IVB | B1 | S1 | RO300 | 658 | 184 | 2056 | 1700 | 1.2094 | 222.5 | 2.1 |
| 129763-IVB | B1 | S2 | RO1011 | 658 | 269 | 2137 | 1811 | 1.1800 | 317.4 | 1.98 |
| 109201-IVB | A | S1 | RO1011 | 452 | 116 | 2115 | 1878 | 1.1262 | 130.6 | 1.09 |
| 130944-IVB | G | S1 | RO1012 | 254 | 212 | 2521 | 2264 | 1.1135 | 236.1 | 1.81 |
| 125183-IVB | F | S1 | RO1012 | 202 | 208 | 2396 | 2192 | 1.0931 | 227.4 | 1.73 |
| 129768-IVB | B1 | S1 | RO1012 | 860 | 141 | 2401 | 2052 | 1.1701 | 165 | 1.42 |
| 130938-IVB | B1 | S2 | RO300 | 860 | 302 | 2009 | 1726 | 1.1640 | 421.4 | 3.05 |
| 129755-IVB | A | S1 | RO1012 | 652 | 105 | 2496 | 2148 | 1.1620 | 122 | 1.55 |
| 125184-IVB | G | S1 | RO1011 | 458 | 154 | 2129 | 1840 | 1.1571 | 178.2 | 1.84 |
| 125880-IVB | A | S2 | RO1011 | 652 | 113 | 2159 | 1866 | 1.1570 | 130.7 | 0.93 |
| 130939-IVB | B1 | S3 | RO300 | 254 | 326 | 1993 | 1798 | 1.1085 | 361.4 | 3.13 |
| 120739-IVB | F | S1 | RO300 | 404 | 130 | 1988 | 1711.7 | 1.1614 | 151 | 1.34 |
| 131277-IVB | A | S1 | RO300 | 852 | 165 | 2100 | 1796 | 1.1680 | 192.7 | 2.06 |
| 129756-IVB | A | S2 | RO1012 | 852 | 138 | 2478 | 2145 | 1.1552 | 159.4 | 1.1 |
| 130943-IVB | G | S1 | RO1011 | 660 | 186 | 2186 | 1842 | 1.1868 | 220.7 | 2.03 |
| 129764-IVB | B1 | S3 | RO1011 | 456 | 145 | 2094 | 1816 | 1.1531 | 167.2 | 2.35 |
| 130940-IVB | G | S1 | RO300 | 862 | 173 | 2102 | 1767 | 1.1896 | 205.8 | 1.81 |
| 130945-IVB | F | S1 | RO1012 | 606 | 101 | 2442.3 | 2158.1 | 1.1317 | 114.3 | 0.93 |
| 125881-IVB | A | S1 | RO1011 | 1052 | 136 | 2121 | 1894 | 1.1199 | 152.3 | 1.37 |

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3.12.1. The calcium adjustment used in this analysis was taken from the Sequence IIIIGB.
 3.12.2. Calcium reduction is assumed to be the result of volatility and dilution.

3.12.3. Comments from Intertek:

- 3.12.3.1. The Sequence IVB generates a lot of water and fuel dilution.
- 3.12.3.2. If a calcium adjustment is used, the Surveillance Panel may want to adopt the ICP measurement restrictions listed in the Sequence IIIIGB procedure.
 - 3.12.3.2.1. The IIIIGB procedure specifies that start-of-test and end-of-test ICP samples be measured at the same time and on the same machine.

3.13. Slide #25:

Ln(FEWMEOT_Ca_Adj) - ANOVA Full Model

Statistically significant differences:

- Lab, Oil

Not significantly different:

- Stands within Labs

| Summary of Fit | | | | |
|----------------------------|--|--|--|----------|
| RSquare | | | | 0.657934 |
| RSquare Adj | | | | 0.513907 |
| Root Mean Square Error | | | | 0.258386 |
| Mean of Response | | | | 5.226639 |
| Observations (or Sum Wgts) | | | | 28 |

| Analysis of Variance | | | | |
|----------------------|----|-----------|-------------|----------|
| Source | DF | Squares | Mean Square | F Ratio |
| Model | 8 | 2.4398569 | 0.304982 | 4.5681 |
| Error | 19 | 1.2685020 | 0.066763 | Prob > F |
| C. Total | 27 | 3.7083589 | | 0.0031* |

| Parameter Estimates | | | | |
|-------------------------|-----------|-----------|---------|-----------|
| Term | Estimate | Std Error | t Ratio | Prob > t |
| Intercept | 5.2072249 | 0.057496 | 90.57 | <.0001* |
| RefOil[RO1011] | -0.042438 | 0.073795 | -0.58 | 0.5720 |
| RefOil[RO1012] | -0.149076 | 0.07211 | -2.07 | 0.0526 |
| LTMESLAB[A] | -0.249068 | 0.083894 | -2.97 | 0.0079* |
| LTMESLAB[B1] | 0.2137059 | 0.078023 | 2.74 | 0.0130* |
| LTMESLAB[F] | -0.11074 | 0.125078 | -0.89 | 0.3870 |
| LTMESLAB[A]:Stand[S1] | 0.1176384 | 0.088171 | 1.33 | 0.1979 |
| LTMESLAB[B1]:Stand[S1] | -0.111157 | 0.107015 | -1.04 | 0.3120 |
| LTMESLAB[B1]:Stand[S2] | 0.246849 | 0.106975 | 2.31 | 0.0324* |

| Effect Tests | | | | | |
|-----------------|-------|----|----------------|---------|----------|
| Source | Nparm | DF | Sum of Squares | F Ratio | Prob > F |
| RefOil | 2 | 2 | 0.5391278 | 4.0376 | 0.0346* |
| LTMESLAB | 3 | 3 | 1.1972860 | 5.9778 | 0.0048* |
| Stand[LTMESLAB] | 3 | 3 | 0.4703869 | 2.3485 | 0.1049 |

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- 3.13.1. The calcium adjustment does improve the significance of the oil discrimination.
- 3.13.2. It improves the oil discrimination from a borderline level to a statistically significant level.

3.14. Slide #28:

Ln(FEWMEOT_Ca_Adj) Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand(Lab)}$
- Plot below of $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ LSMeans by Lab, with 95% confidence intervals
- Lab A is statistically significantly different than Lab B1.

| Lab | Ln(FEWMEOT_Ca_Adj) LS Mean | FEWMEOT_Ca_Adj LS Mean |
|-----|----------------------------|------------------------|
| A | 4.9581 | 142 |
| B1 | 5.4209 | 226 |
| F | 5.0965 | 163 |
| G | 5.3533 | 211 |

| Lab1 | Lab2 | Ln(FEWMEOT_Ca_Adj) LS Mean Difference | p-Value |
|------|------|---------------------------------------|---------|
| B1 | A | 0.4628 | 0.0035 |
| G | A | 0.3952 | 0.0886 |
| B1 | F | 0.3244 | 0.2672 |
| G | F | 0.2568 | 0.6063 |
| F | A | 0.1383 | 0.8625 |
| B1 | G | 0.0676 | 0.9689 |

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- 3.14.1. The p-values are more significant with the calcium adjustment.

3.15. Slide #30:

Ln(FEWMEOT_Ca_Adj) Precision

Repeatability Model: $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand(Lab)}$
 Reproducibility Model: $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil}$

| Model RMSE | Repeatability | Reproducibility |
|---|--|--|
| <ul style="list-style-type: none"> $s_r = 0.2584$ | <ul style="list-style-type: none"> $s_r = 0.2584$ $r = 0.7162$ | <ul style="list-style-type: none"> $s_R = 0.3395$ $R = 0.9410$ |

Based upon the $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ pooled standard deviation (s_r) and ASTM's repeatability (r), there is no significant difference between an FEWMEOT_Ca_Adj result¹ of 200 and 409.

Note 1: An FEWMEOT_Ca_Adj result of 200 was arbitrarily selected for comparison

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- 3.15.1. There is an improvement in overall repeatability with the calcium adjustment.
 - 3.15.1.1. This is a small improvement and not necessarily a "slam dunk".

3.15.2. The final decision about using a calcium adjustment will be up to the Surveillance Panel.

3.15.3. Comments from Intertek:

3.15.3.1. They are in favor of the calcium adjustment.

3.15.3.2. A transform is needed.

3.15.3.3. They are concerned about the potential redundancy between AVLI and end-of-test iron.

3.15.3.4. This issue can be resolved by making iron a secondary parameter.

3.15.4. Comments from General Motors:

3.15.4.1. *What should be done about oils that do not use calcium?*

3.15.4.1.1. They have concerns about using calcium to assess volatility and dilution.

3.15.4.1.2. Calcium is a detergent, so it is surface active.

3.15.4.1.3. Some calcium will be lost due to this surface activation.

3.15.4.1.4. IAR noted that the Industry may need to look at magnesium or sulfur when testing formulations that do not use calcium.

3.15.4.2. *Would it be more appropriate to use fuel dilution or water content to assess volatility/dilution?*

3.15.4.3. The three Precision Matrix oils probably use similar chemistry.

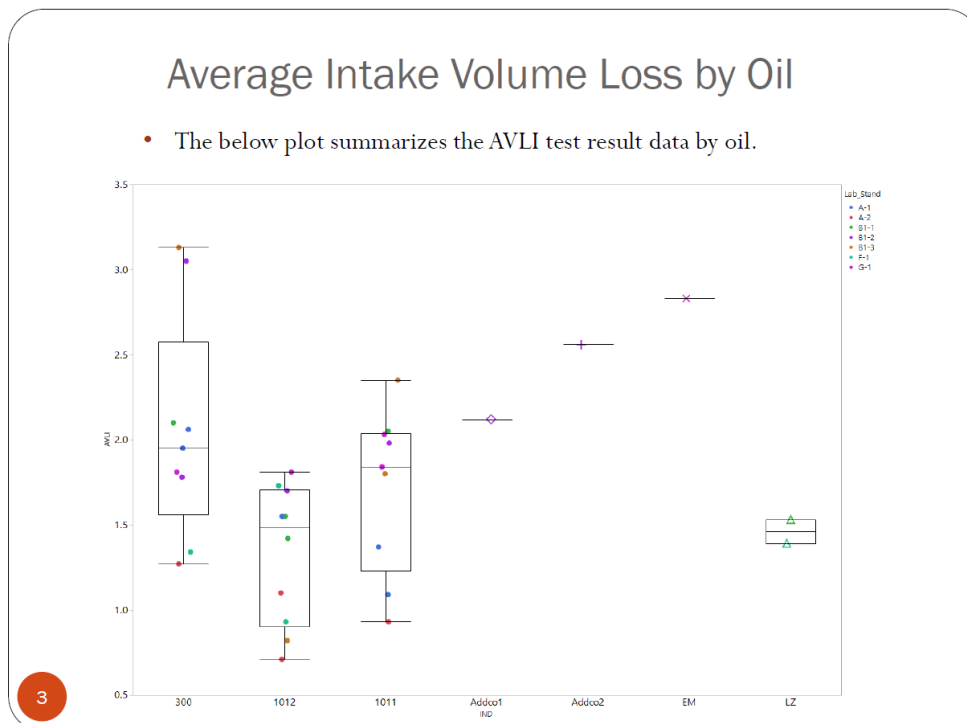
3.15.4.3.1. The Surveillance Panel will need to look at outlier oils to determine if they display a different relationship between iron and AVLI.

4. STATISTICAL ANALYSIS OF HIGH WEAR OILS (STATISTICS GROUP):

4.1. Background:

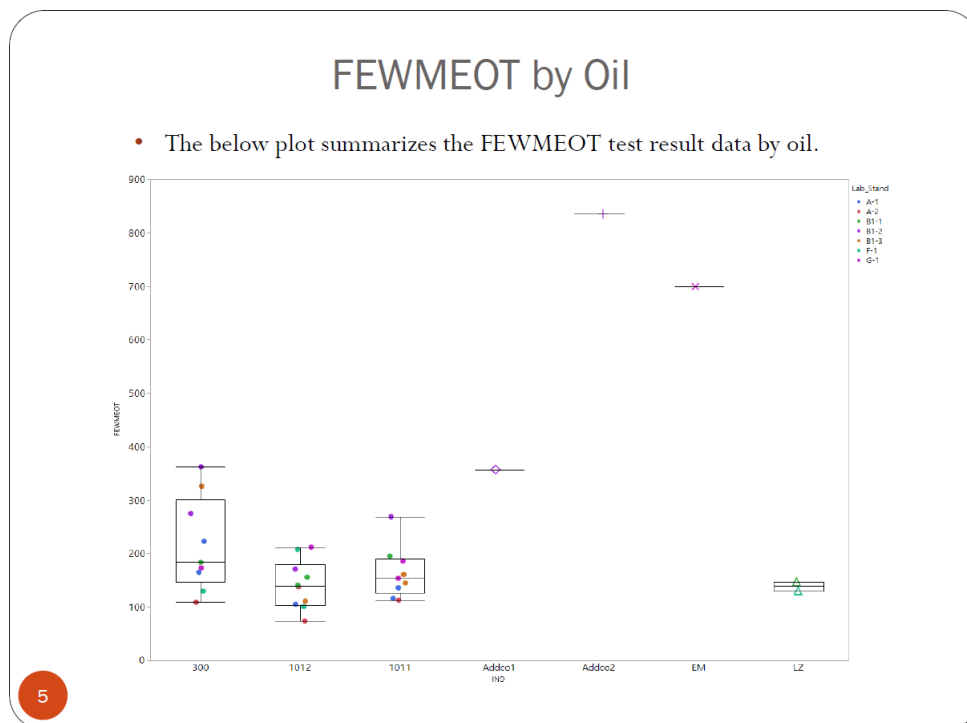
4.1.1. The Statistics Group conducted an analysis of results from oils that were intended to generate high wear on the Sequence IVB test (dated 03-27-2018).

4.2. Slide #3:



4.2.1. This slide shows the Precision Matrix oils and the high wear oils on the same plot.

4.3. Slide #5:



4.3.1. IAR cannot explain the two consecutive mild results with the Lubrizol high wear oil.

4.3.2. Comments from Toyota:

4.3.2.1. The Lubrizol oil had a late TAN-TBN cross-over.

4.3.2.2. This suggests that the oil offers good degradation control.

4.3.3. General Motors asked if Lubrizol had any Sequence IIIG data for this oil.

4.3.4. Comments from Lubrizol:

4.3.4.1. This oil was not run on the Sequence III.

4.3.4.2. However, Lubrizol's statistical models predict that this oil would fail the Sequence IIIG for both WPD and PVIS.

4.3.4.3. The oil uses a typical AO package for a GF-4 formulation.

4.3.5. Comments from Intertek:

4.3.5.1. They have reports and/or presentations from the Surveillance Panel members that have run high wear oils.

4.3.5.2. This data will be compiled and shared with the Industry.

4.3.6. Statement from Unnamed Additive Company (Conveyed by Buscher):

4.3.6.1. This company is identified as "Addco2".

4.3.6.2. The data in the plot is for an oil with no ash and minimal anti-wear additives.

4.3.6.2.1. Average Intake Lifter Volume Loss = 2.56mm³

4.3.6.2.2. E.O.T. Iron = 836ppm

4.3.6.3. They rescinded the results from their second oil (which was an SN+ formulation).

4.3.7. Comments from Lubrizol:

4.3.7.1. The 200HR iron from the "Addco2" test is extremely high, especially considering that it had an average intake lifter volume loss around 2.5mm³.

4.3.7.2. Was there excessive wear or damage to the engine?

4.3.8. Intertek Response to Lubrizol's Question:

4.3.8.1. IAR confirmed that the engine did exhibit excessive wear after the test.

4.3.8.2. This was the 9th run on the engine.

4.3.8.3. The engine was "healthy" during the 8th run.

- 4.3.8.4. The crankshaft was worn to a point at which it would no longer meet factory tolerances.
- 4.3.8.5. PDI bore traces indicate a wear scar of approximately 40-microns on the thrust-side.
 - 4.3.8.5.1. The block would need to be honed if it were to be used again.
- 4.3.8.6. There is excessive piston ring wear.
- 4.3.8.7. There is some timing chain wear.
- 4.3.8.8. Oil consumption was around 1000g.
- 4.3.8.9. IAR believes that this oil would have even rendered a 1st run engine unserviceable.

4.3.9. Comments from Exxon:

- 4.3.9.1. The results from "Addco2" are like what they experienced with their high wear oil.
- 4.3.9.2. Their oil rendered a 6th run block unserviceable.
- 4.3.9.3. These two situations exemplify why they are concerned with iron as a pass/fail parameter.

4.3.10. Comments from Lubrizol:

- 4.3.10.1. Lubrizol shares Exxon's concerns about iron as a pass/fail parameter.
- 4.3.10.2. Lubrizol is also confused by the lack of consistency in engine wear with the "poor" oils.
 - 4.3.10.2.1. Lubrizol completely disassembled the Precision Matrix engine that was used to test its "poor" proof-of-performance oil.
 - 4.3.10.2.2. Wear was minimal.
- 4.3.10.3. IAR confirmed that the engine used for the repeat test with Lubrizol's "poor" proof-of-performance oil is still in service.
 - 4.3.10.3.1. So, wear with this engine was also minimal.

5. IVB LTMS SUGGESTIONS SUMMARY (STATISTICS GROUP):

5.1. Background:

- 5.1.1. The Word document outlines the proposed LTMS system for the Sequence IVB test (dated 03-08-2018).
- 5.1.2. The Excel spreadsheet has tabs that display the output of the proposed LTMS system.

5.2. Overview of Proposed LTMS System (Word Document):

- 5.2.1. This would be a stand-based system with charts for AVLI (average intake lifter volume loss) and 200HR (end-of-test) iron.
 - 5.2.1.1. The statisticians have proposals for unadjusted iron and iron that is adjusted for calcium.
 - 5.2.1.2. The Excel file with the calcium adjustment was completed today.
- 5.2.2. Test stands will be charted separately with their own severity adjustments.

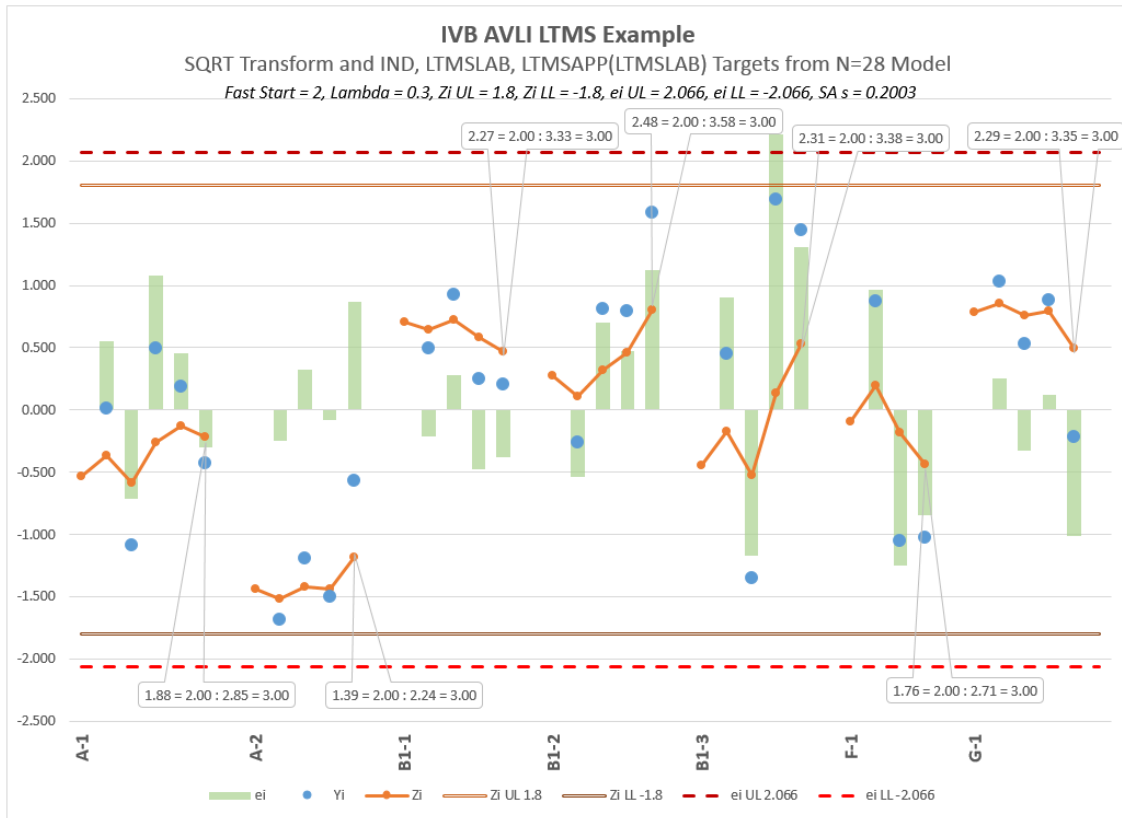
5.2.3. Z_i Limit:

- 5.2.3.1. A default recommended limit is used.
- 5.2.3.2. This default limit is used in all GF-6 test types except the Sequence IX.

5.2.4. Z_o Limit:

- 5.2.4.1. A "fast start" Z_o limit is proposed.
- 5.2.4.2. Two tests are the default setting.
- 5.2.4.3. It will be up to the discretion of the Surveillance Panel to increase this to three tests.

5.3. LTMS Chart AVLI (Spreadsheet):



5.3.1. Stands A-1 and A-2 (which are in the same lab) are statistically very similar (even though they display some small visual differences).

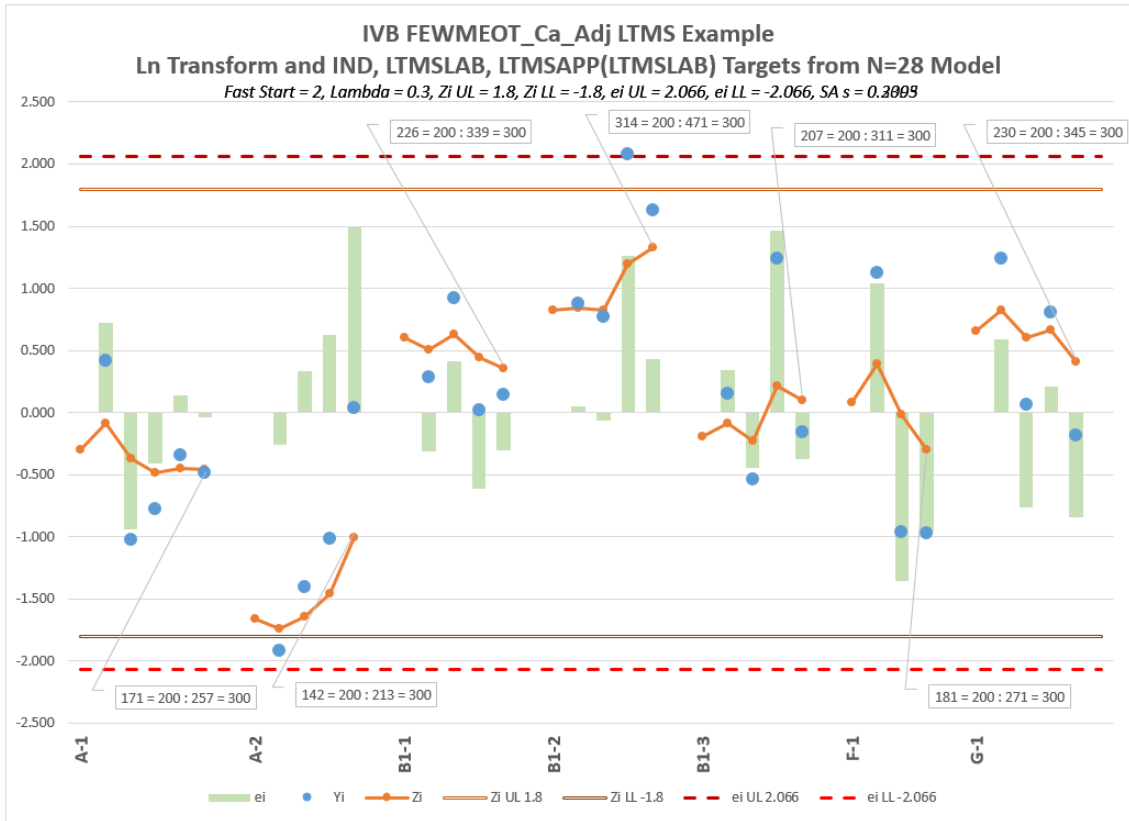
5.3.1.1. This supports the stand-based system.

5.3.2. Stand B1-3 did have one result that failed due to an e_i alarm.

5.3.2.1. However, the subsequent Precision Matrix result would have allowed the stand to reference.

5.3.2.2. This is the only example of a failing result with the proposed LTMS system.

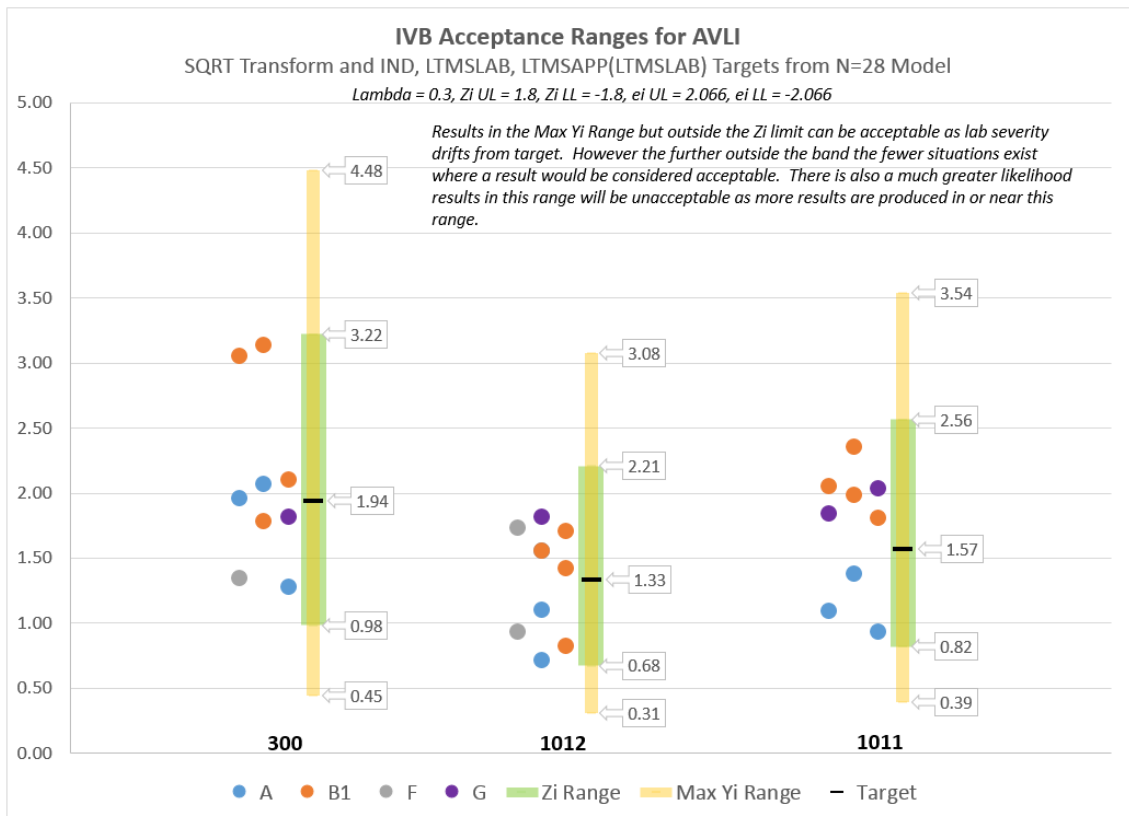
5.4. LTMS Chart FE_Ca_Adj (Spreadsheet):



5.4.1. The pattern is like that of the AVLI parameter.

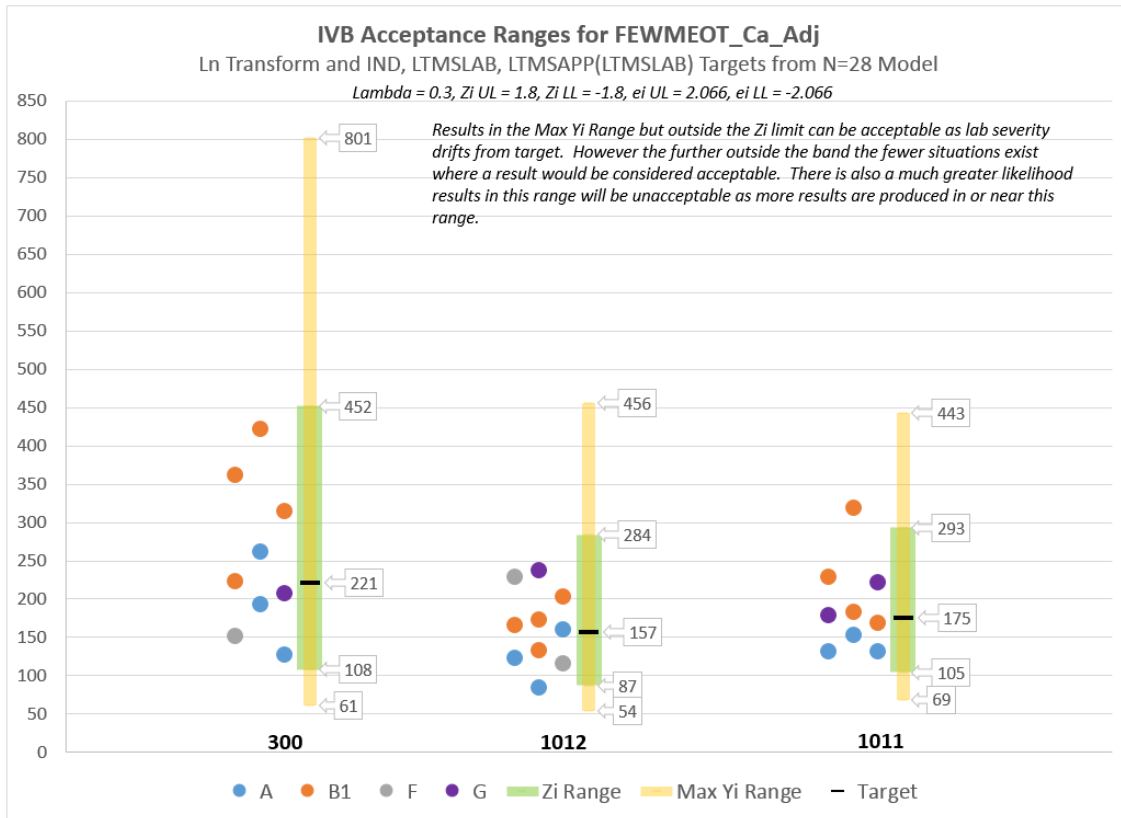
5.4.2. Stand B1-3 does not trip an e_i alarm with the iron parameter.

5.5. Range Chart AVLI (Spreadsheet):



5.5.1. A lab that repeatedly operated in the yellow bands would trigger an alarm.

5.6. Range Chart FEWMEOT_Ca_Adj (Spreadsheet):



5.6.1. In certain situations, an 801ppm result with REO300 or a 456ppm result with REO1012 would be acceptable.

5.6.1.1. However, a lab cannot operate close to these limits for long.

5.6.2. Comments from Lubrizol:

5.6.2.1. Stand B1-2 is operating with a Zi of 1.3.

5.6.2.2. So, a high iron result on B1-2 would be acceptable.

5.6.2.3. However, the next test would need to have a lower iron for that stand to maintain calibration.

5.7. General Discussion:

5.7.1. Comments from Exxon:

5.7.1.1. They would like the Surveillance Panel to formally discontinue any further discussion or analysis with the N=21 dataset.

5.7.1.2. There was unanimous approval within the Surveillance Panel to discontinue the N=21 dataset.

5.7.2. How Should the Three Existing Reference Oils be Used?

5.7.2.1. The statisticians stated that this is an engineering decision and not a statistical decision.

5.7.2.2. Afton believes that REO1011 should be checked [during reference tests] more often than the other two oils because of its 0W-16 viscosity.

5.7.2.3. IAR reminded the Surveillance Panel that it can decide on a reference oil frequency now and change it later.

5.7.2.4. There was a broad consensus within the Surveillance Panel to initially test all three reference oils at an equal frequency.

5.7.3. Transformations:

5.7.3.1. There was a general agreement within the Panel that a square-root would be used for AVLI and a natural log would be used for the calcium-adjusted iron.

5.7.4. Iron:

5.7.4.1. Afton and the TMC are concerned about implementing iron as a pass/fail parameter before there is a clear understanding about how engine life will impact it.

5.7.4.1.1. They suggested making iron a "report only" parameter until more data is available.

5.7.4.2. Comments from Intertek:

5.7.4.2.1. The IVB Data Dictionary will need to be updated to reflect the proposed LTMS system.

5.7.4.2.2. The Sequence IIIIGB procedure uses magnesium or sodium to adjust the iron for formulations that lack calcium.

5.7.4.2.3. The IVB will need to adopt the following IIIIGB oil sample methodology:

5.7.4.2.3.1. S.O.T. and E.O.T. ICP samples will need to be run consecutively and in duplicate.

5.7.4.2.3.2. The average of the duplicate runs will be reported.

5.7.4.3. Lubrizol, Infineum and Exxon would all like to see more clarity with the iron parameter before the Surveillance Panel votes on the LTMS system.

5.7.4.4. General Motors and Ford agree that this test needs an iron parameter because AVLI is not sufficient.

5.7.4.4.1. They want to make iron a pass/fail parameter now to eliminate the timing uncertainty with making it a pass/fail parameter in the future.

5.7.4.4.2. They do not want any more delays with GF-6.

5.7.5. Communication:

5.7.5.1. The TMC will issue an information letter that summarizes all the procedural and process changes that accompany the new LTMS system.

5.7.6. Proposed Pass/Fail Limits:

5.7.6.1. Toyota is considering a 400ppm pass/fail limit for iron.

5.7.6.1.1. This limit may be increased to 450ppm if a calcium adjustment is used.

5.7.6.2. Exxon noted that all three reference oils have Y_i 's that would allow them to get into the 450ppm range for iron.

5.7.6.2.1. Two of these three oils are considered good performers.

5.7.6.2.2. One of these oils is considered a borderline performer.

5.7.6.3. Consensus within Surveillance Panel:

5.7.6.3.1. Chart iron using the unadjusted targets for now.

5.7.6.3.2. Implement the calcium adjustment after more data becomes available.

5.7.6.3.3. Limit the application of iron severity adjustments to candidate oils.

5.7.6.3.4. Do not implement calibration requirements for iron.

5.7.6.4. Lobe Failures:

5.7.6.4.1. Lobe failures should be captured in LTMS.

5.7.6.4.2. They will be reported as valid but not charted.

5.7.7. Vote:

5.7.7.1. The Surveillance Panel ran out of time during this conference call to hold a vote on the proposed LTMS system.

5.7.7.2. Buscher will issue an electronic ballot.

5.7.7.3. Intertek made the motion and Toyota seconded the motion.

| Action Items | Person responsible | Completion Date |
|--------------|--------------------|-----------------|
| | | |
| | | |
| | | |

| Follow-up Notes/Updates | Initials | Date Added |
|-------------------------|----------|------------|
| | | |
| | | |
| | | |

| Attendees | Organization | Contact Information |
|-----------|--------------|---------------------|
| | | |
| | | |
| | | |

Sequence IV Surveillance Panel

Conference Call

March 28, 2018







9:00 a.m. - 12:00 p.m.

A G E N D A

1. Chairman comments
2. Previous action item review
3. Sequence IVB Precision Matrix 2 AFR, exhaust gas temperature, crankcase pressure and intake manifold pressure operational data analysis
4. Sequence IVB Precision Matrix 2 statistical analysis review:
Analysis and conclusions on iron content
5. Sequence IVB Precision Matrix 2 + high wear candidate oils statistical analysis review:
Analysis and conclusions on AVLI and FEWMEOT
6. Sequence IVB LTMS review
7. Possible vote to accept a Sequence IVB LTMS
8. Motion and action item review
9. Next meeting
10. Adjourn






**MEMBERSHIP
SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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March 28, 2018

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SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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**NON-MEMBER MAILING LIST
SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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| Knight, Clayton | Test Engineering, Inc. 12718 Cimarron Path San Antonio, TX 78249 Phone No.: 210-862-5987 cell Fax No.: 210-690-1959 Email: cknight@tei-net.com | |
| Kostan, Travis | Southwest Research Institute 6220 Culebra Road P.O. Drawer 28510 San Antonio, TX 78228-0510 Phone No.: 210-522-2407 Fax No.: 210-684-7523 Email: travis.kostan@swri.org | ✓ |
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**NON-MEMBER MAILING LIST
SEQUENCE IV SURVEILLANCE PANEL**

March 28, 2018

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| Matasic, James | Lubrizol Corporation 29400 Lakeland Blvd. Wickliffe, OH 44092 Phone No.: 440-347-2487 Fax No.: Email: James.Matasic@Lubrizol.com |  |
| McMillan, Mike | 5019 Deer Creek Cir N Washington, MI 48094 Phone No.: 586-677-9198 Fax No.: Email: mmcmillan123@comcast.net | |
| Meier, Adam | ExxonMobil Phone No.: Fax No.: Email: adam.r.meier@exxonmobil.com |  |
| O'Malley, Kevin | Lubrizol Corporation 29400 Lakeland Blvd. Wickliffe, OH 44092 Phone No.: 440-347-4141 Fax No.: Email: Kevin.OMalley@lubrizol.com |  |
| Pastor, Jofran | Infineum Phone No.: Fax No.: Email: jofran.pastor@infineum.com | |
| Porter, Christian | Afton Chemical Corporation 500 Spring Street P.O. Box 2158 Richmond, VA 23217-2158 Phone No.: 804-788-5837 Fax No.: 804-788-6358 Email: christian.porter@aftonchemical.com | |
| Ritchie, Andrew | Infineum USA L.P. 1900 E. Linden Avenue Linden, NJ 07036-0536 Phone No.: 908-474-2097 Fax No.: 908-474-3637 Email: andrew.ritchie@infineum.com |  |

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March 28, 2018

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March 28, 2018

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| | <p>Phone No.: Fax No.: Email:</p> | |
| | <p>Phone No.: Fax No.: Email:</p> | |
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| | <p>Phone No.: Fax No.: Email:</p> | |
| | <p>Phone No.: Fax No.: Email:</p> | |

TOYOTA

Sequence IVB LTMS

**Sequence IV Surveillance Panel
eBallot**

March 30, 2018

- AVLI = Intake lifter average volume loss, mm³
- FEWM EOT = Iron content at end of test, ppm

- Stand based LTMS
 - All stands will be charted separately
 - Severity adjustments will be calculated on a stand basis
- Use ASTM reference oils 300, 1012 and 1011
- Use an equal reference oil assignment frequency
- Adopt the transform $\text{Sqrt}(\text{AVLI})$ for LTMS and severity adjustment calculations
- Adopt the transform $\text{Ln}(\text{FEWMEOT})$ for severity adjustment calculations

Sequence IVB LTMS eBallot

TOYOTA

- Set reference oil targets from the complete, N = 28, precision matrix 2 data set
 - IND, LTMSLAB, LTMSLAP (LTMSAPP) w/ Sqrt from N = 28 Model
- AVLI Targets

| Oil | Number of Tests | Target Mean AVLI | Target Mean Sqrt(AVLI) | Target Standard Deviation Sqrt(AVLI) |
|------|-----------------|------------------|------------------------|--------------------------------------|
| 300 | 9 | 1.94 | 1.3931 | 0.2230 |
| 1012 | 10 | 1.33 | 1.1543 | 0.1847 |
| 1011 | 9 | 1.57 | 1.2538 | 0.1932 |

- Severity adjustment standard deviation (SA s) is RMSE from Oil only model Sqrt(AVLI) = 0.2003

Sequence IVB LTMS eBallot

TOYOTA

- Set reference oil targets from the complete, N = 28, precision matrix 2 data set
 - IND, LTMSLAB, LTMSLAP (LTMSAPP) w/ Ln from N = 28 Model
- FEWMEOT Targets

| Oil | Number of Tests | Target Mean FEWMEOT | Target Mean Ln(FEWMEOT) | Target Standard Deviation Ln(FEWMEOT) |
|------|-----------------|---------------------|-------------------------|---------------------------------------|
| 300 | 9 | 191 | 5.2500 | 0.4067 |
| 1012 | 10 | 138 | 4.9249 | 0.3365 |
| 1011 | 9 | 152 | 5.0258 | 0.2722 |

- Severity adjustment standard deviation (SA s) is RMSE from Oil only model Ln(FEWMEOT) = 0.3426

- AVLI will be a primary, critical LTMS parameter, with calibration acceptance criteria and severity adjustments
 - Will be charted
- FEWMEOT will be a secondary, non-critical LTMS parameter, with severity adjustments, but without calibration acceptance criteria
 - Will be charted
- Tests with lobe failures would be un-chartable

- Utilize limits on Z_i (EWMA of severity), e_i (prediction error), and the excessive influence calculation to determine acceptance and calculate severity adjustments
 - Z_i Lambda = 0.3
 - Z_0 = Average of first two tests in a stand
 - Note this is how many references a new stand will require to enter the system
 - Z_i Limit = +1.800/-1.800; a stand that exceeds these limits requires additional references until it is within the limits
 - Do not update severity adjustments until after an acceptable reference is conducted

Sequence IVB LTMS eBallot

TOYOTA

- e_i Limit 1 = +/-1.351; this limit applies to previously calibrated stands that have not been calibrated for two reference periods and are attempting to calibrate again
 - The stand can calibrate with one test if the Level 1 limits are not exceeded
 - References after the first attempt will be judged against the level 3 ei limits
- e_i Limit 2 = +/-1.734; this limit applies in situations pre-determined by the SP to have potential impact to severity
 - Some situations that warrant consideration include hardware changes or engine build changes in a currently calibrated stand

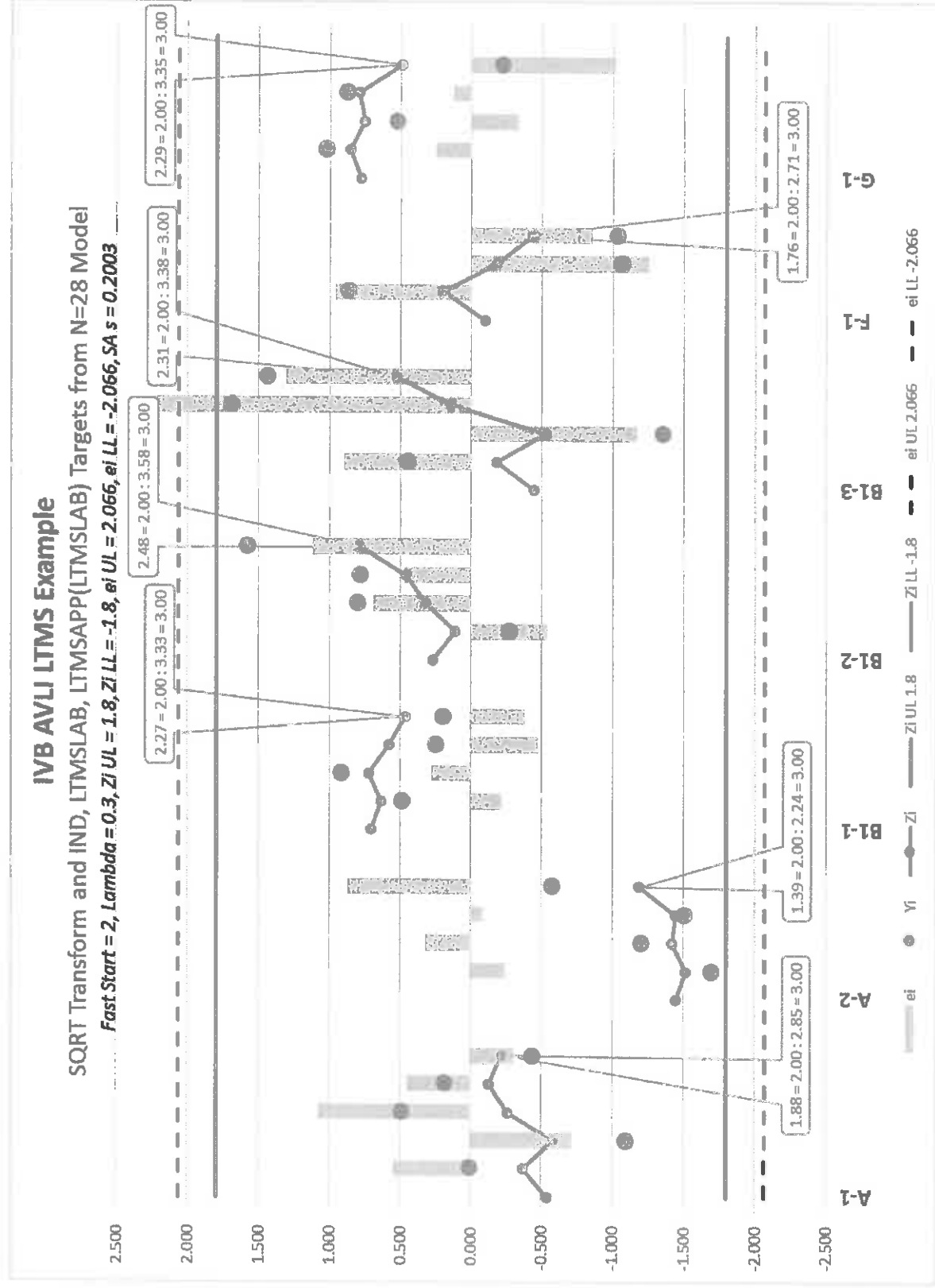
- The stand can calibrate with one test if the Level 2 limits are not exceeded
- References after the first attempt will be judged against the level 3 ei limits
- e_i Limit 3 = +/-2.066; this limit applies to all other situations when determining an acceptable reference.
 - If the limit is exceeded do not update control charts until after an additional reference is conducted and apply excessive influence calculations
- The excessive influence calculation minimizes the impact of a failing reference test if the following reference test does not agree with the initial failing results and returns to historical severity performance (LTMS 1.A.5)

- A minimum of two references will be required for each new stand
- The reference calibration period will expire after 15 full length non-reference tests or 6 months, whichever comes first

- The TMC will plot industry Zi charts to identify potential shifts in industry wide performance
 - Lambda = 0.2
 - $Z_0 = 0.000$
 - Z_i Limit 1 = +/-0.775
 - When industry level one limits are exceeded the TMC investigates whether severity adjustments are adequately addressing the trend, investigates the possible causes, and communicates as appropriate with industry
 - Z_i Limit 2 = +/-0.859
 - When industry level two limits are exceeded the TMC informs the surveillance panel that the limit has been exceeded. The surveillance panel then investigates and pursues resolution of the alarm

Sequence IVB LTMS eBallot

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Sequence IVB LTMS eBallot

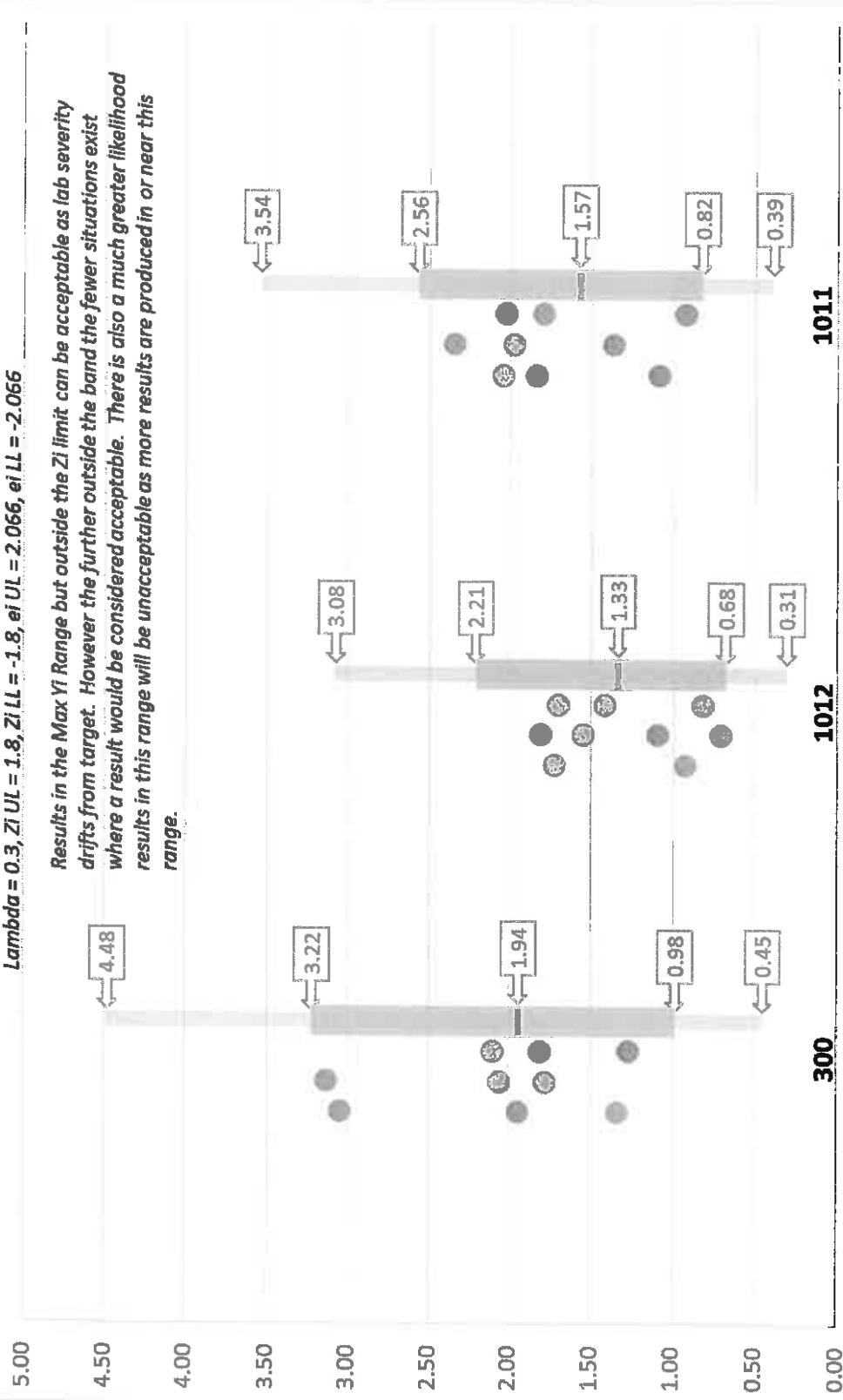
TOYOTA

IVB Acceptance Ranges for AVLI

SQRT Transform and IND, LTMSLAB, LTMSAPP(LTMSLAB) Targets from N=28 Model

$\Lambda = 0.3, Zi UL = 1.8, Zi LL = -1.8, ei UL = 2.066, ei LL = -2.066$

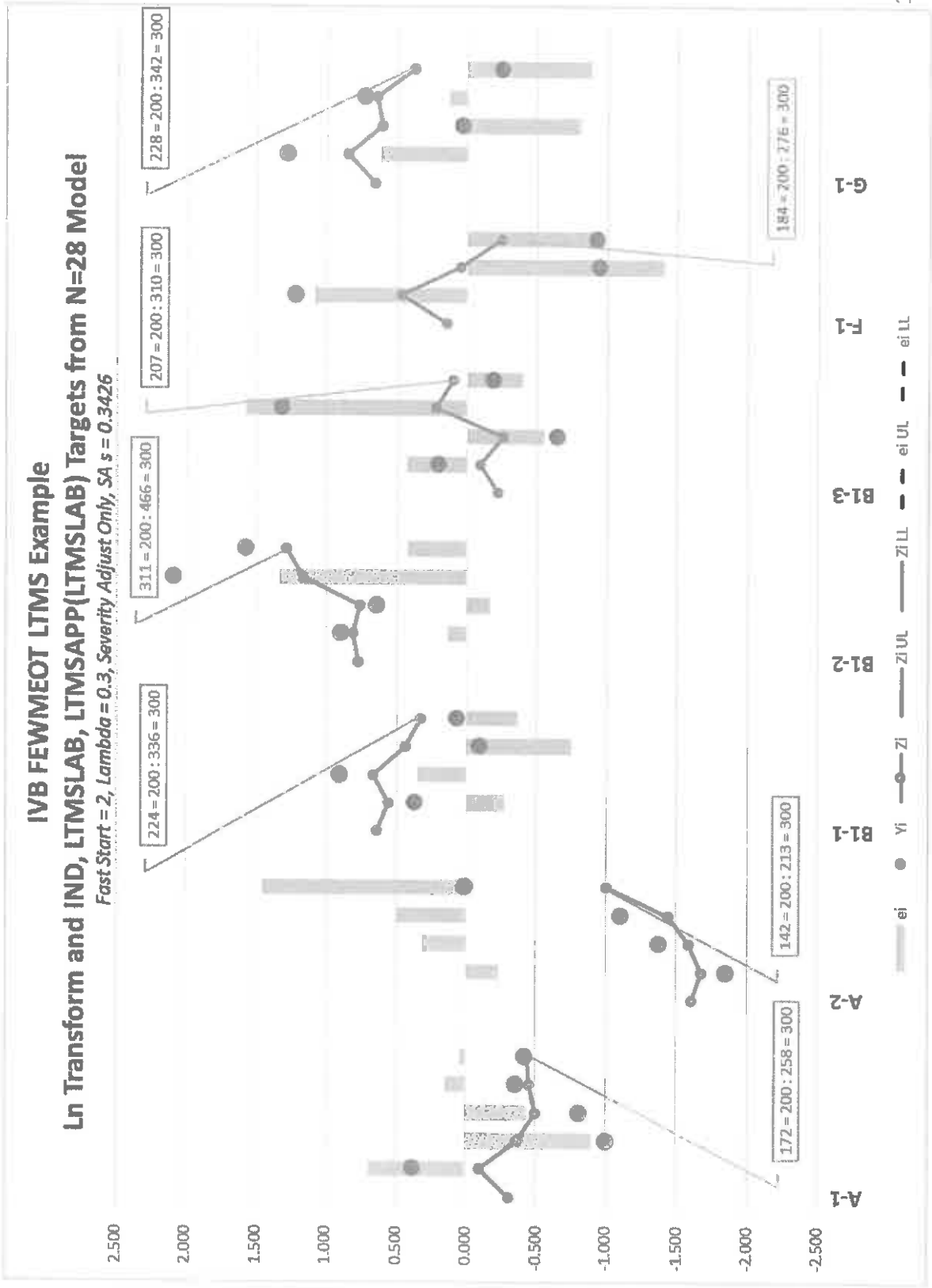
Results in the Max Yi Range but outside the Zi limit can be acceptable as lab severity drifts from target. However the further outside the band the fewer situations exist where a result would be considered acceptable. There is also a much greater likelihood results in this range will be unacceptable as more results are produced in or near this range.



● A ● B1 ● F ● G ● Zi Range ● Max Yi Range — Target

Sequence IVB LTMS eBallot

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Sequence IVB LTMS eBallot

TOYOTA

- **Motion:**
 - Sequence IV surveillance panel accepts the Sequence IVB LTMS, as documented in the previous slides of this presentation (IVB LTMS eBallot 20180329.pptx). Effective 4/18/18 (two weeks after the close of this eBallot) to be applied to all Precision Matrix 2 and later reference tests. The ASTM TMC will grant calibration status where applicable, based on the agreed on LTMS, with calibration intervals effective based on reference test EOT dates.
- **Motion by:**
 - Bill Buscher
- **Seconded by:**
 - Teri Kowalski
- **This eBallot will close on Wednesday, 4/4/18**

IVB LTMS Suggestion Summary – Items in **BOLD** need particular attention from the SP

1. Adopt the transform $\sqrt{\text{AVLI}}$ for LTMS and severity adjustment calculations.
2. **References will be conducted on RO's 300 (40%), 1012 (40%) and 1011 (20%).**
3. **Select Reference Oil targets from presented n=21, n=28, or other model.**

- a. IND, LTMSLAB, LTMSLAP(LTMSAPP) w SQRT from N=21 Model

- i. AVLI Targets

| IND | Mean $\sqrt{\text{AVLI}}$ | Std dev $\sqrt{\text{AVLI}}$ |
|------|---------------------------|------------------------------|
| 300 | 1.4306 | 0.2269 |
| 1011 | 1.2373 | 0.2136 |
| 1012 | 1.1104 | 0.1815 |

- ii. Severity adjustment standard deviation (SA s) is RMSE from Oil only model
 $\sqrt{\text{AVLI}} = 0.2082$

- b. IND, LTMSLAB, LTMSLAP(LTMSAPP) w SQRT from N=28 Model

- i. AVLI Targets

| IND | Mean $\sqrt{\text{AVLI}}$ | Std dev $\sqrt{\text{AVLI}}$ |
|------|---------------------------|------------------------------|
| 300 | 1.3931 | 0.2230 |
| 1011 | 1.2538 | 0.1932 |
| 1012 | 1.1543 | 0.1847 |

- ii. Severity adjustment standard deviation (SA s) is RMSE from Oil only model
 $\sqrt{\text{AVLI}} = 0.2003$

4. **All stands will be charted separately.**

- a. **Severity adjustments will be calculated on a stand basis**

5. Utilize limits on Z_i (EWMA of severity), e_i (prediction error), and the excessive influence calculation to determine acceptance and calculate severity adjustments.

- a. Z_i Lambda = 0.3

- b. Z_0 = Average of **first two tests** in a stand. Note this is how many references a new stand will require to enter the system.

- c. Z_i Limit = **+1.800/-1.800**; a stand that exceeds these limits requires additional references until it is within the limits. Do not update severity adjustments until after an acceptable reference is conducted.

- d. e_i Limit 1 = +/-1.351; this limit applies to previously calibrated stands that have not been calibrated for two reference periods and are attempting to calibrate again. The stand can calibrate with one test if the Level 1 limits are not exceeded. References after the first attempt will be judged against the level 3 e_i limits.

- e. e_i Limit 2 = +/-1.734; this limit applies in situations pre-determined by the SP to have potential impact to severity. Some situations that warrant consideration include hardware changes or engine build changes in a currently calibrated stand. The stand can calibrate with one test if the Level 2 limits are not exceeded. References after the first attempt will be judged against the level 3 e_i limits.

- f. e_i Limit 3 = +/-2.066; this limit applies to all other situations when determining an acceptable reference. If the limit is exceeded do not update control charts until after an additional reference is conducted and apply excessive influence calculations.

- g. The excessive influence calculation minimizes the impact of a failing reference test if the following reference test does not agree with the initial failing results and returns to historical severity performance (LTMS 1.A.5).
- 6. A minimum of two references will be required for each new stand.
- 7. The reference calibration period will expire after **fifteen full length non-reference tests or 6 months**, whichever comes first.
- 8. The TMC will plot industry Z_i charts to identify potential shifts in industry wide performance.
 - a. $\Lambda = 0.2$
 - b. $Z_0 = 0.000$
 - c. Z_i Limit 1 = ± 0.775
 - i. When industry level one limits are exceeded the TMC investigates whether severity adjustments are adequately addressing the trend, investigates the possible causes, and communicates as appropriate with industry.
 - d. Z_i Limit 2 = ± 0.859
 - i. When industry level two limits are exceeded the TMC informs the surveillance panel that the limit has been exceeded. The surveillance panel then investigates and pursues resolution of the alarm.

Sequence IVB High Wear Oil

Statistics Group

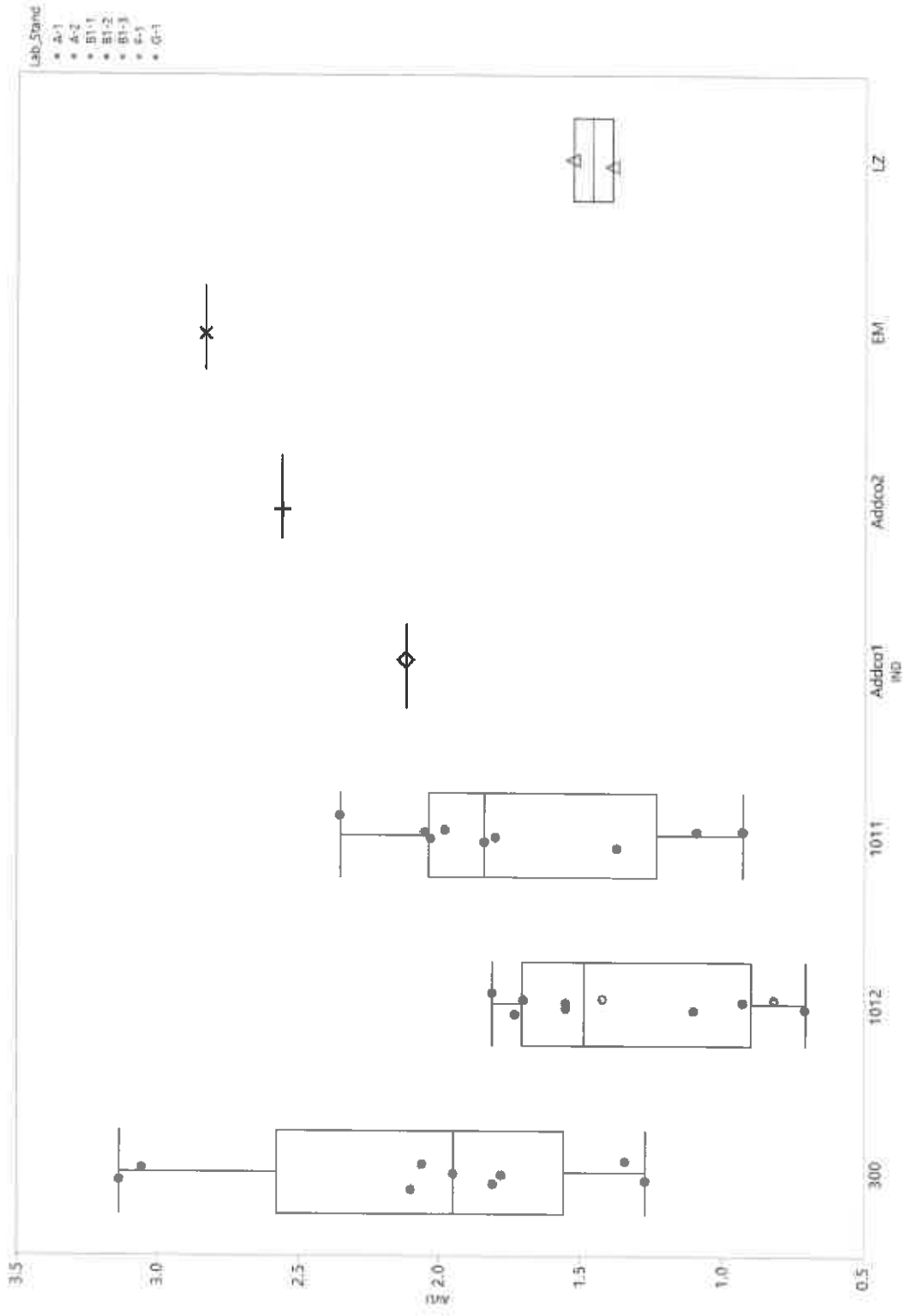
March 27, 2018

Statistics Group

- Arthur Andrews, ExxonMobil
- Doyle Boese, Infineum
- Jo Martinez, Chevron Oronite
- Kevin O'Malley, Lubrizol
- Martin Chadwick, Intertek
- Richard Grundza, TMC
- Lisa Dingwell, Afton
- Todd Dvorak, Afton
- Travis Kostan, SwRI

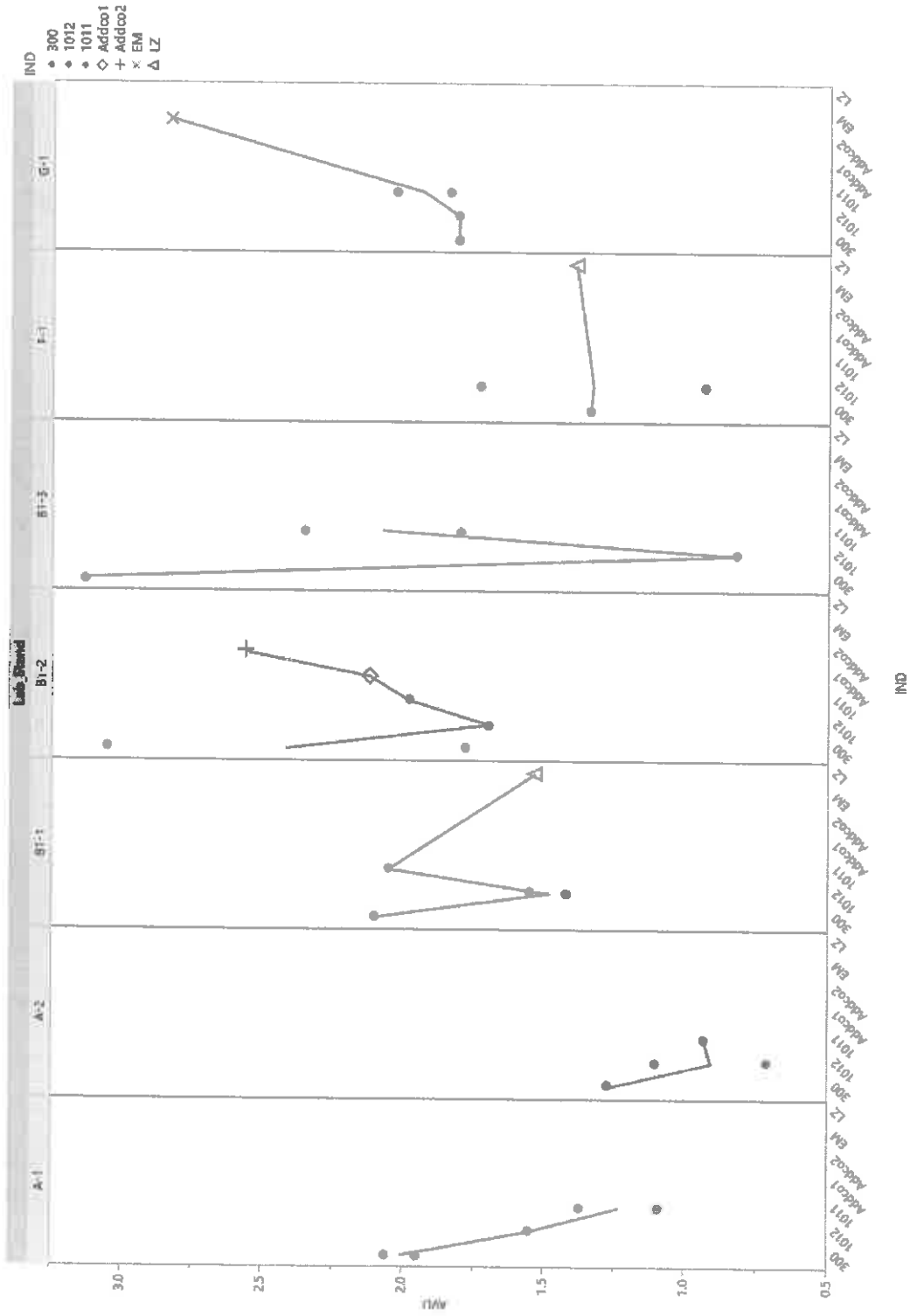
Average Intake Volume Loss by Oil

- The below plot summarizes the AVLI test result data by oil.



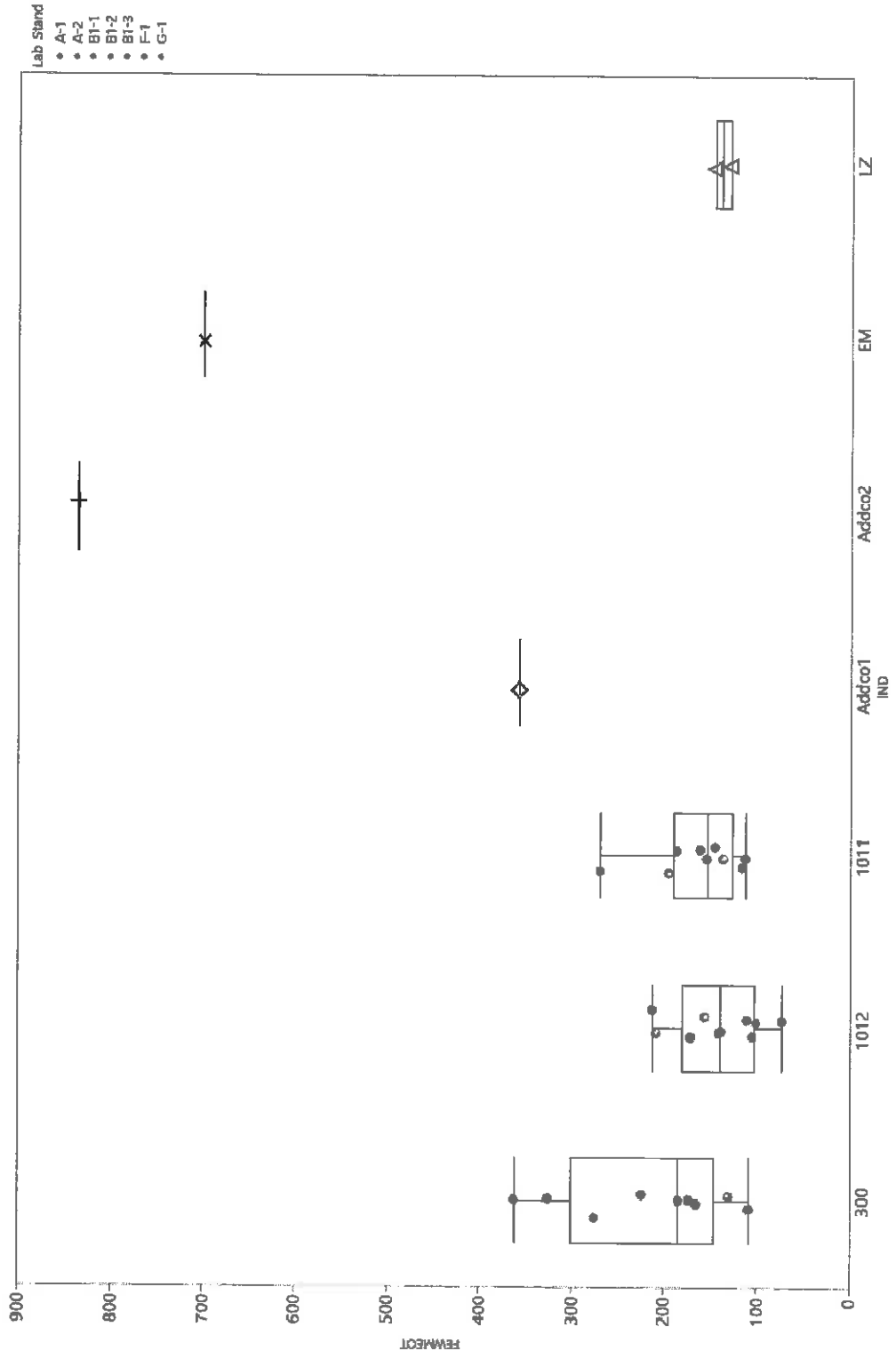
Average Intake Volume Loss by Stand

- The below plot summarizes the AVL test result data by oil within the stand.



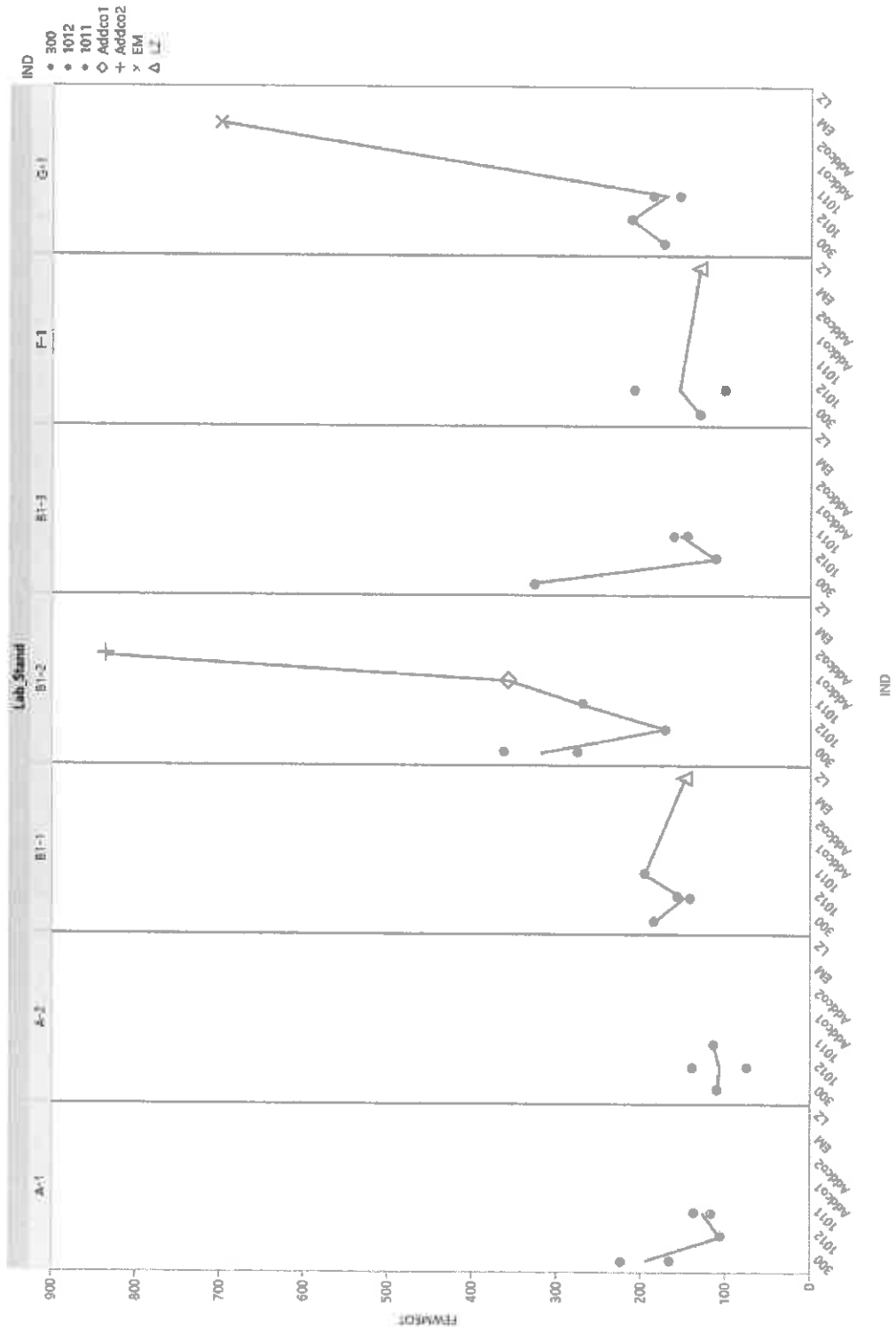
FEWMEOOT by Oil

- The below plot summarizes the FEWMEOOT test result data by oil.



FEWMEOT by Stand

- The below plot summarizes the FEWMEOT test result data by oil within the stand.



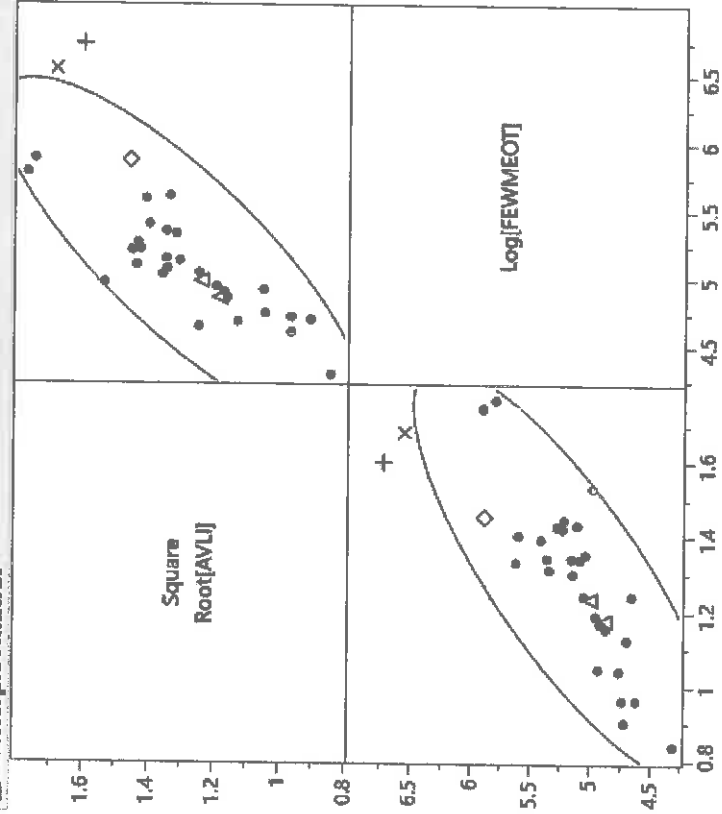
Correlation

- There is significant correlation between AVLI and FEWMEOOT.

Correlations

| | Square Root[AVLI] | Log[FEWMEOOT] |
|-------------------|-------------------|---------------|
| Square Root[AVLI] | 1.0000 | 0.8136 |
| Log[FEWMEOOT] | 0.8136 | 1.0000 |

Scatterplot Matrix



Legend for shape

- 300
- 1012
- 1011
- ◇ Addco1
- + Addco2
- × EM
- △ LZ

Statistical Analysis of Sequence IVB Operational Data

(Includes EGT, AFR, IntManPres, Crankcase Pressure Operational Data, Exclusive)

By: Industry Stats Team

03-20-18

tatistical Analysis of Operational Data

Analysis was performed to investigate the relationship of Sqrt(AVLI) parameter with respect to the below list of variables:

- Reference Oil (indicator coding of variable)
- Stand[Lab] (indicator coding of variable)
- AFR (stage 1 & 2)
- Blowby Flow Rate (stage 1 & 2)
- Crankcase Pressure (stage 1 & 2)
- Exhaust Temps (stage 1 & 2)
- Manifold Pressure (stage 1 & 2)

Analyzed data included all 28 PM test results

Statistical Analysis of Operational Data

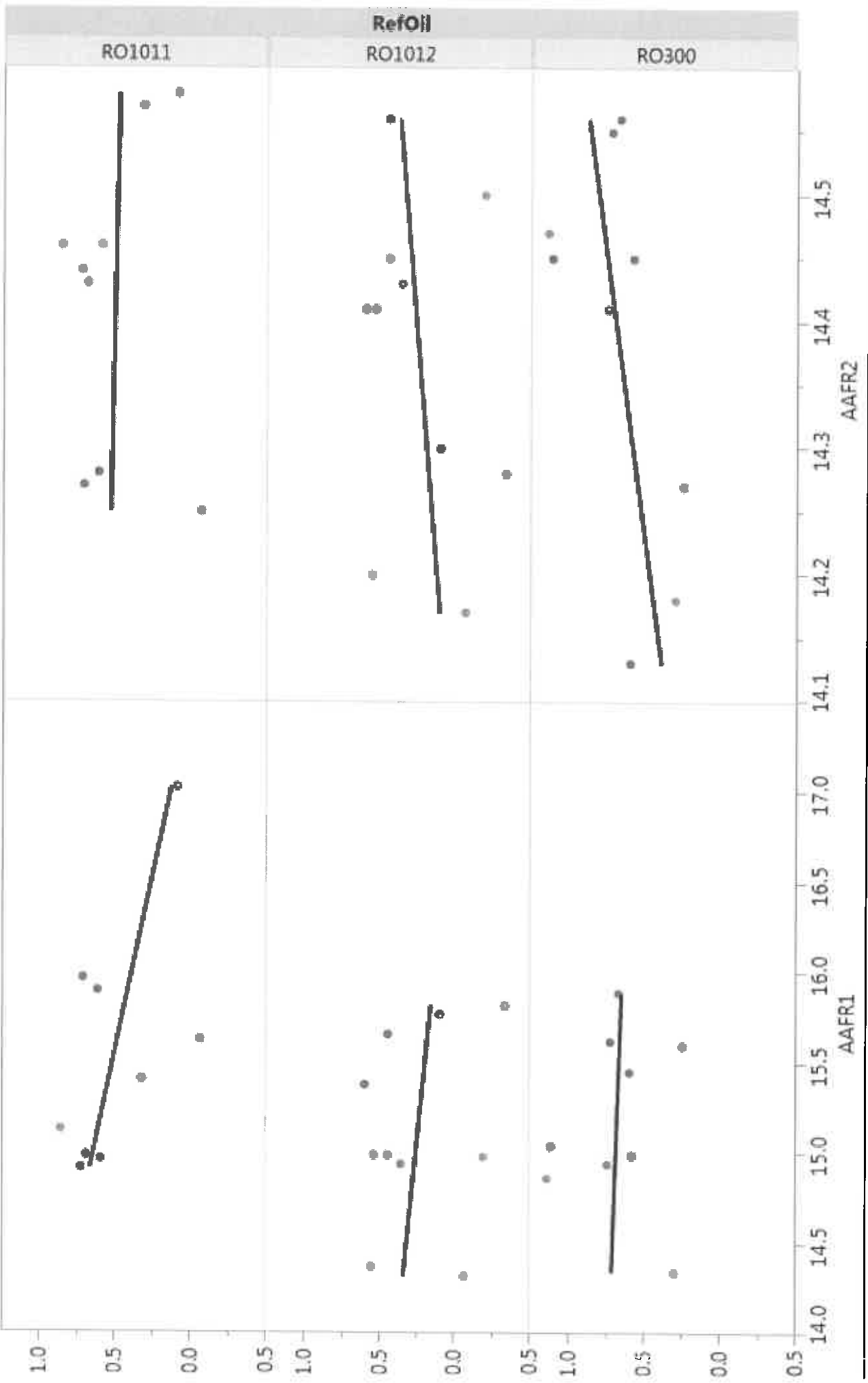
Due to multicollinearity, a Partial Least Squares (PLS) Analysis was performed on the data set

PLS analysis results (*with 2 latent variables*) for centered and scaled are summarized below (and sorted by their centered and scaled coefficients):

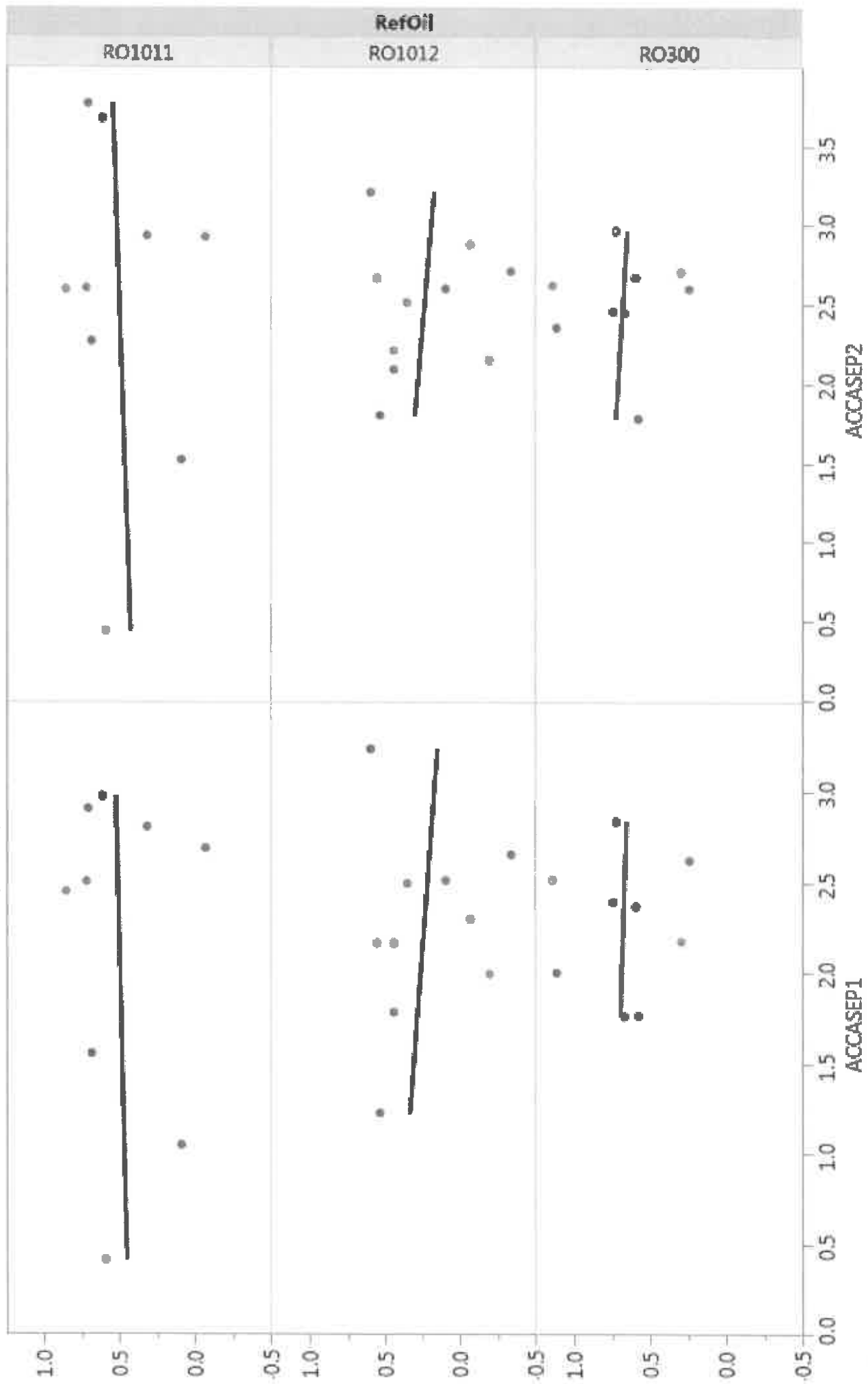
| Rank | Term | Coefficient (Centered & Scaled) |
|------|-----------|------------------------------------|
| 1 | A-2 | -0.3198 |
| 2 | 1012 | -0.2625 |
| 3 | 300 | 0.2378 |
| 4 | ABLOWBY1 | 0.1554 |
| 5 | AAFR1 | -0.1487 |
| 6 | B1-2 | 0.1337 |
| 7 | G-1 | 0.1286 |
| 8 | AMAP1 | 0.1065 |
| 9 | AAFR2 | 0.0828 |
| 10 | AMAP2 | -0.0764 |
| 11 | ACCASEP2 | 0.075 |
| 12 | B1-1 | 0.0621 |
| 13 | ABLOWBY2 | 0.0612 |
| 14 | B1-3 | 0.0535 |
| 15 | F-1 | -0.0342 |
| 16 | ACCASEP1 | 0.0332 |
| 17 | 1011 | 0.0315 |
| 18 | A-1 | -0.0256 |
| 19 | AEXHT1 | -0.0241 |
| 20 | AEXHT2 | 0.0132 |
| 21 | Intercept | 0 |

-Appendix-
Plots of PLS Variables

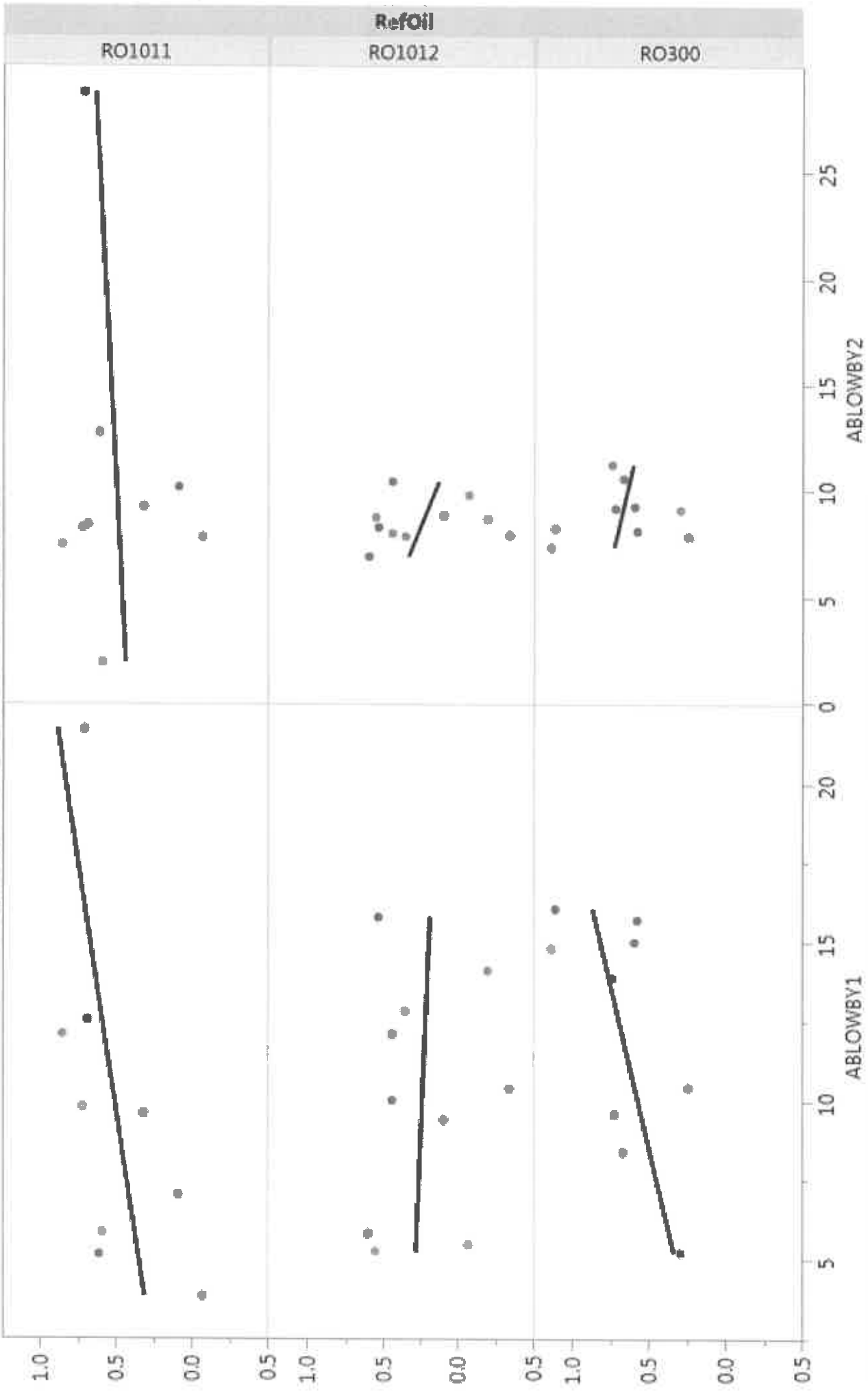
LN(AVLI) vs. AAFR1 & AAFR2



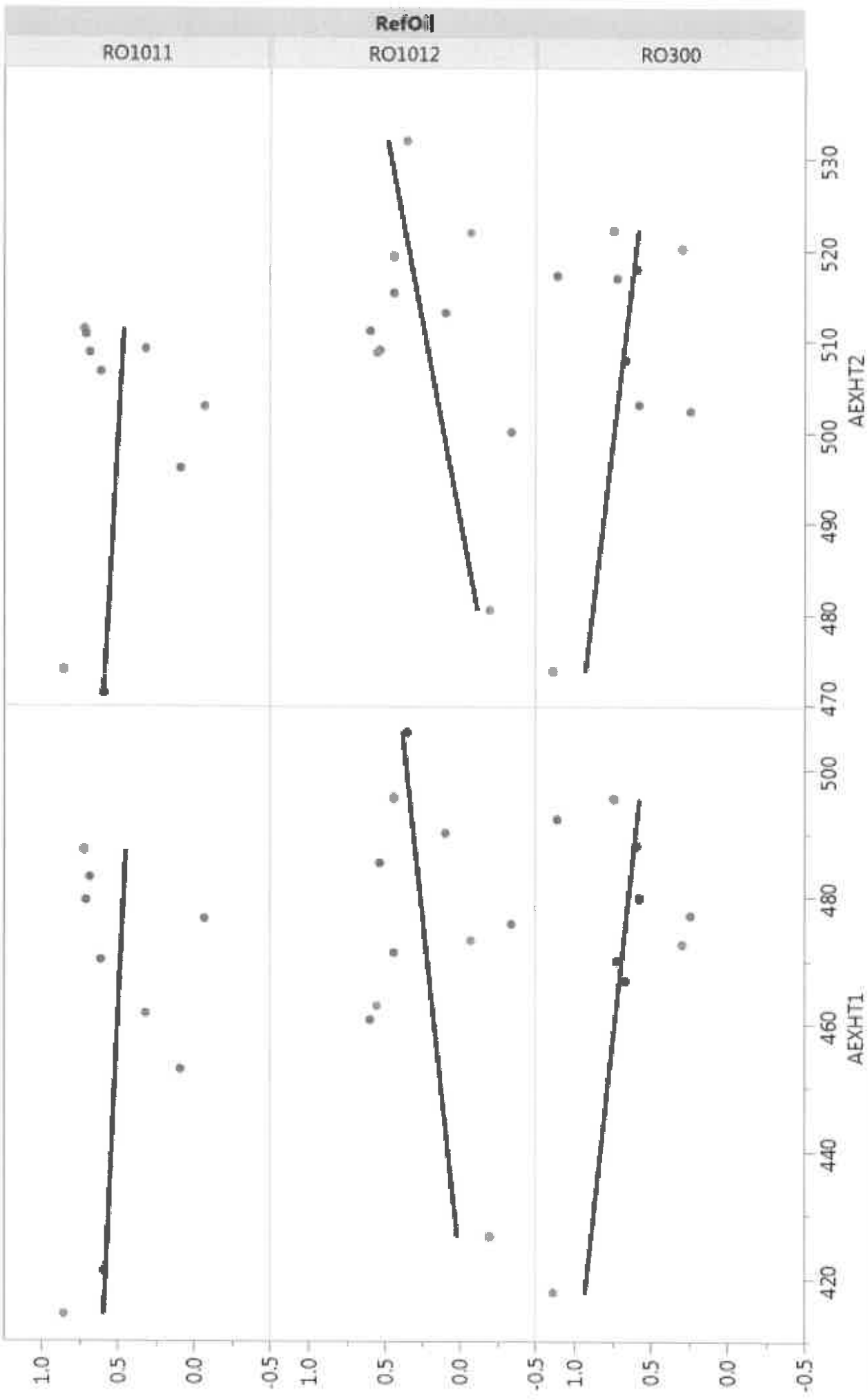
LN(AVLJ) vs. ACCASEP1 & ACCASEP2



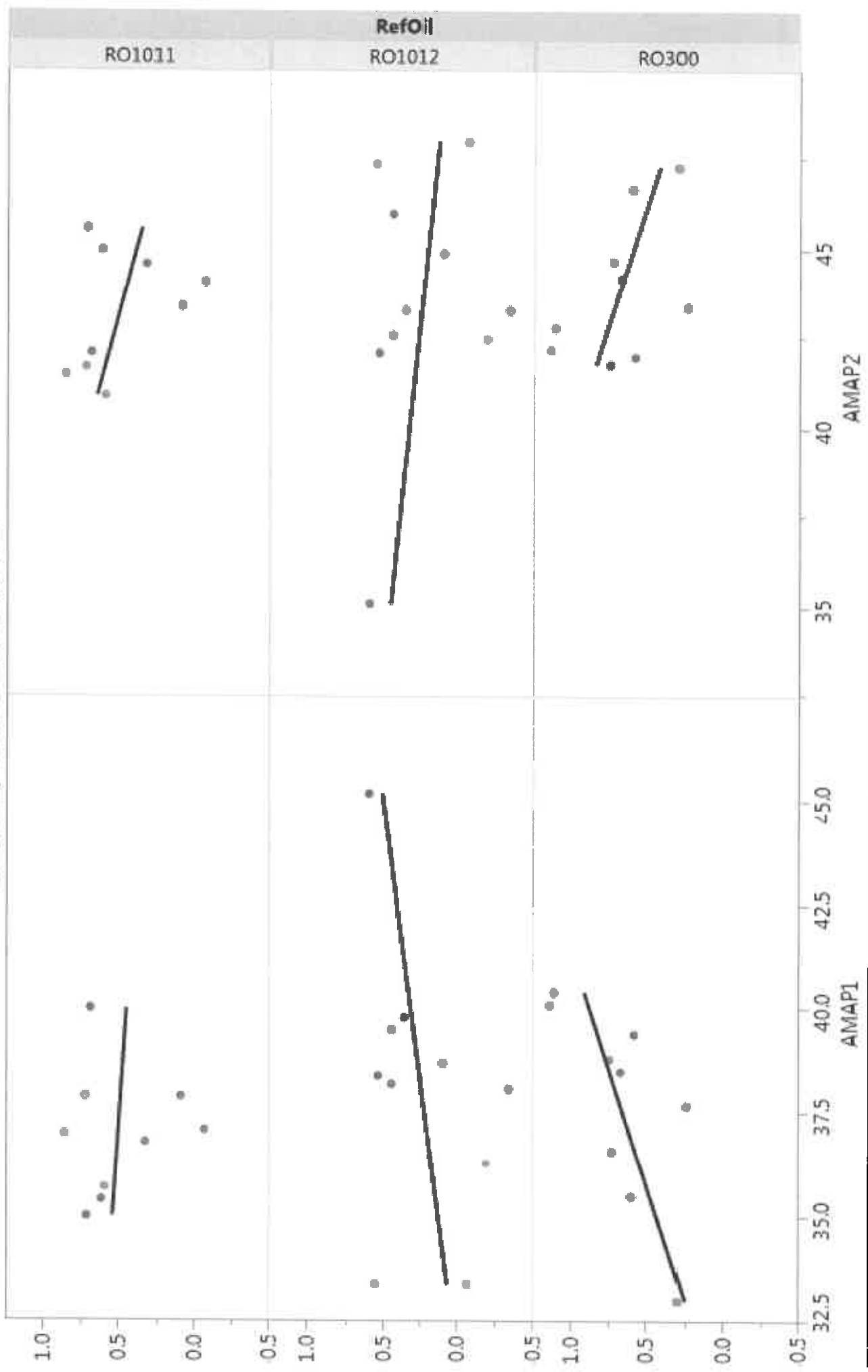
LN(AVLI) vs. ABLOWBY1 & ABLOWBY2



LN(AVLI) vs. AEXHT1 & AEXHT2



LN(AVLI) vs. AMAP1 & AMAP2



Sequence IVB Precision Matrix Iron Analysis

Statistics Group

March 26, 2018

Statistics Group

- Arthur Andrews, ExxonMobil
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- Jo Martinez, Chevron Oronite
- Kevin O'Malley, Lubrizol
- Martin Chadwick, Intertek
- Richard Grundza, TMC
- Lisa Dingwell, Afton
- Todd Dvorak, Afton
- Travis Kostan, SwRI

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- This analysis includes the results of 28 valid precision matrix tests
- Data supports the use of Ln(FEWMEOT) transformation
 - Borderline statistical significant oil difference: $1012 < 300$
 - Lab differences are statistically significant ($A < B1$)
 - Stand within Lab differences are not statistically significant
- Oil discrimination is more significant for FEWMEOOT than FEWML25 (Fe increase over last 25 hours) and FEWML50 (Fe increase over last 50 hours).
- Oil discrimination is more significant with the Calcium Adjustment of the FEWMEOOT data
- FEWMEOOT can be affected by dilution factors such as fuel, water, volatility, etc.
 - Calcium content is lower at EOT as compared to SOT
- FEWMEOOT adjusted using calcium data may be a more preferred approach. However, this approach may contain more error as it is based on multiple (ICP) measurements of Calcium data.
 - Adopting a procedure such as the IIGB/IIHB may reduce the error associated with the calcium based adjustment
 - Possible concern - candidate oils may not be calcium based
- Correlation between $\text{sqrt}(\text{AVLI})$ and $\text{Ln}(\text{FEWMEOOT})$ or $\text{Ln}(\text{FEWMEOOT_Ca_Adj})$ is high (indicating parameter redundancy).

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- Estimated within a stand test precision (r; ASTM repeatability)
 - $\ln(\text{FEWMEOT}) = 0.7487$
- Estimated test precision across labs and stands (R; ASTM reproducibility)
 - $\ln(\text{FEWMEOT}) = 0.9496$
- Oil means and standard deviations

| Oil | Number of Tests | Target Mean $\ln(\text{FEWMEOT})$ | Target Mean FEWMEOT | Target Standard Deviation $\ln(\text{FEWMEOT})$ |
|------|-----------------|-----------------------------------|---------------------|---|
| 300 | 9 | 5.2500 | 191 | 0.4067 |
| 1012 | 10 | 4.9249 | 138 | 0.3365 |
| 1011 | 9 | 5.0258 | 152 | 0.2722 |

- Same concerns with AVLJ are seen in Fe analysis (Two high results on Oil 300 influence oil discrimination, discrimination not consistent among stands, test precision is large compared to the observed range of measurements)

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- Estimated within a stand test precision (r; ASTM repeatability)
 - $\text{Ln}(\text{FEWMEO}_T\text{Ca_Adj}) = 0.7162$
- Estimated test precision across labs and stands (R; ASTM reproducibility)
 - $\text{Ln}(\text{FEWMEO}_T\text{Ca_Adj}) = 0.9410$
- Oil means and standard deviations

| Ref. Oil | Number of Tests | Target Mean $\text{Ln}(\text{FEWMEO}_T\text{Ca_Adj})$ | Target Mean FEWMEO _T | Target Standard Deviation $\text{Ln}(\text{FEWMEO}_T\text{Ca_Adj})$ |
|----------|-----------------|---|------------------------------------|--|
| 300 | 9 | 5.3987 | 221 | 0.3967 |
| 1012 | 10 | 5.0581 | 157 | 0.3277 |
| 1011 | 9 | 5.1648 | 175 | 0.2863 |

- Same concerns with AVLJ are seen in Fe analysis (Two high results on Oil 300 influence oil discrimination, discrimination not consistent among stands, test precision is large compared to the observed range of measurements)

Data Utilized

- Precision Matrix Data:
 - 4 Labs {A, B1, F and G}
 - 3 Reference Oils {300, 1012, and 1011}
 - 7 Stands {A-1, A-2, B1-1, B1-2, B1-3, F-1 and G-1}
 - Total number of tests = 28
- Precision Matrix Data Table from Rich Grundza's 20180115 IVB Matrix update.

| Run order | B1-1 | B1-2 | B1-3 | A-1 | A-2 | F-1 | G-1 | E-1 |
|-----------|--------------------|--------------------|--|---|--------------------|--------------------|--------------------|------|
| 1 | 1012 129773-IVB | 300 129759-IVB | 1011 125879-IVB | 300 129752-IVB | 1012 125882-IVB | 1012 125183-IVB | 1012 130944-IVB | 300 |
| 2 | 1011 129762-IVB | 1012 129766-IVB | 1012 129767-IVB | 1011 109201-IVB 1011* 125881-IVB | 300 130948-IVB | 300 120759-IVB | 1011 125184-IVB | 1011 |
| 3 | 300 129760-IVB | 1011 129763-IVB | 300 129761-IVB 300 130939-IVB | 1012 129755-IVB | 1011 125880-IVB | 1012 130945-IVB | 1011 130943-IVB | 300 |
| 4 | 1012 129768-IVB | 300 130938-D/B | 1011 129764-IVB | 300 111277-IVB | 1012 129756-IVB | | 300# 130940-IVB | |
| Reported | | | Invalid | | | | | |

* Laboratory is running additional test because of Lean AFR and lower fuel flow on original matrix test

Additional test donated by lab

Reference Oil Discrimination Comparison

The table below compares the numbers of standard deviations of separation between the highest and lowest reference oil across GF-6 test types. The median of other tests is approx. 3.55 and the mean (without PHOS) is 3.99.

| Test | Parameter | Oil 1 | Oil 2 | Range | Test s_i | SDs of Separation |
|-----------|---------------------|----------|----------|--------|------------|-------------------|
| IIHH | Ln(PVIS) | 4.7191 | 3.3289 | 1.3902 | 0.4641 | 3 |
| IIHH | WPD | 4.63 | 3.66 | 0.97 | 0.47 | 2.1 |
| IIIIHA | Ln(MRV) | 11.1107 | 9.7854 | 1.3253 | 0.4214 | 3.1 |
| IIIIHB | PHOS | 94.15 | 78.92 | 15.23 | 1.53 | 10 |
| VIE | FEI 1 | 2.56 | 1.3 | 1.26 | 0.29 | 4.3 |
| VIE | FEI 2 | 1.82 | 1.41 | 0.41 | 0.12 | 3.4 |
| VIF | FEI 1 | 2.23 | 1.45 | 0.78 | 0.21 | 3.7 |
| VIF | FEI 2 | 2.25 | 1.41 | 0.84 | 0.19 | 4.4 |
| IX (LSPI) | Sqrt(AVPIE + 0.5) | 4.2644 | 3.3819 | 0.8825 | 0.2856 | 3.1*1 |
| VH | AES | 8.43 | 6.47 | 1.96 | 0.5 | 3.9 |
| VH | Ln(10-RCS) | 0.9155 | -0.5294 | 1.4449 | 0.2194 | 6.6 |
| VH | AEV50 | 9.26 | 8.77 | 0.49 | 0.25 | 2 |
| VH | APV50 | 8.67 | 7.35 | 1.32 | 0.53 | 2.5 |
| X (CW) | Ln(CHST) | -2.10574 | -2.63174 | 0.526 | 0.14148 | 3.7*2 |
| IVB | Sqrt(AVLI) | 1.3931 | 1.1543 | 0.2388 | 0.168 | 1.4 |
| IVB | Ln(FEWMMEOT) | 5.25 | 4.9249 | 0.3251 | 0.2701 | 1.2 |
| IVB | Ln(FEWMMEOT_Ca_Adj) | 5.3987 | 5.0581 | 0.3406 | 0.2584 | 1.3 |

*1: Oil 220 not used as a reference oil. Including this oil would yield approx. 12 SDs of separation between 220 and 222.

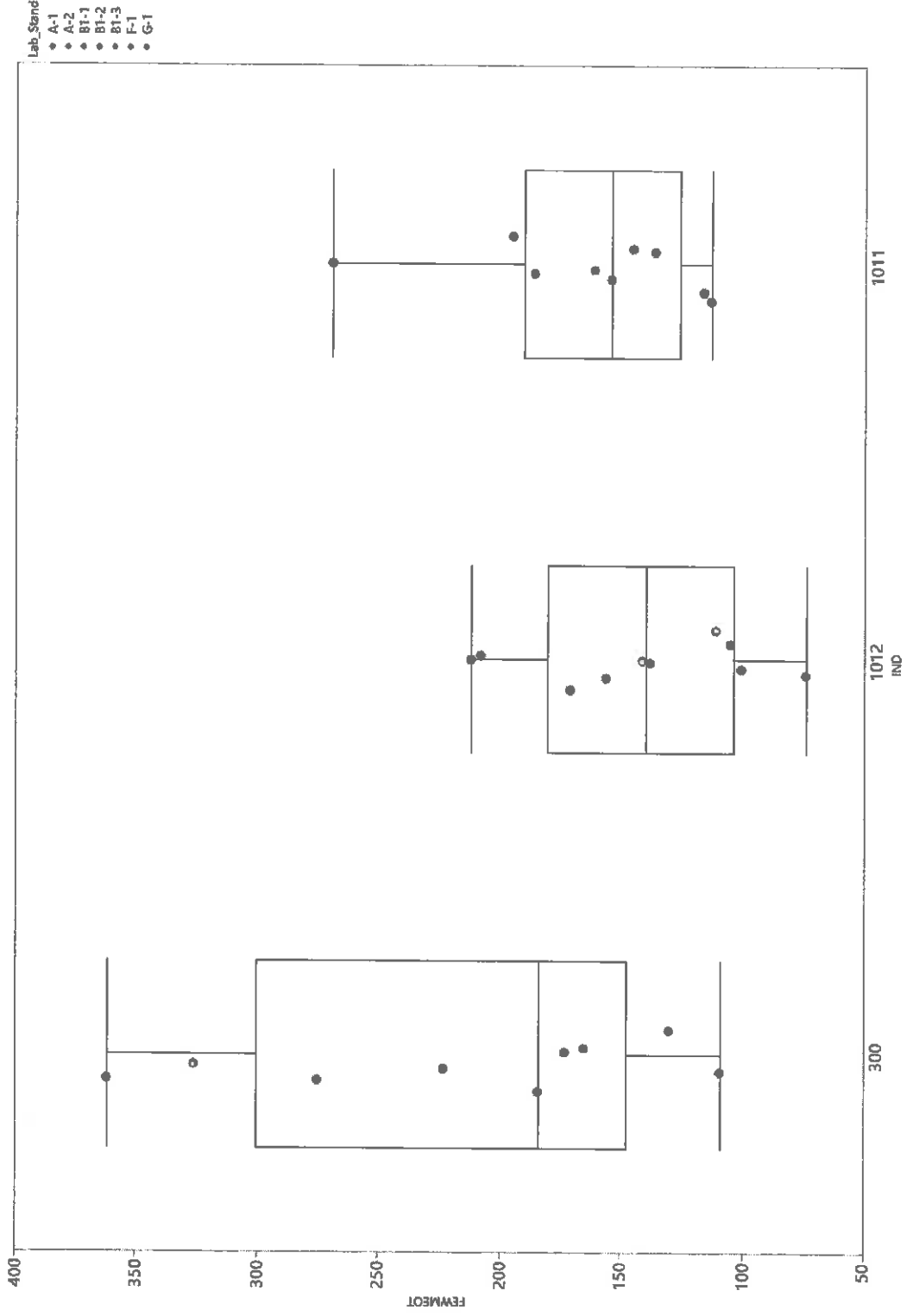
*2: 271 vs. 1011

FEWMEOT (n=28)

Fe-Wear Metals at end of test

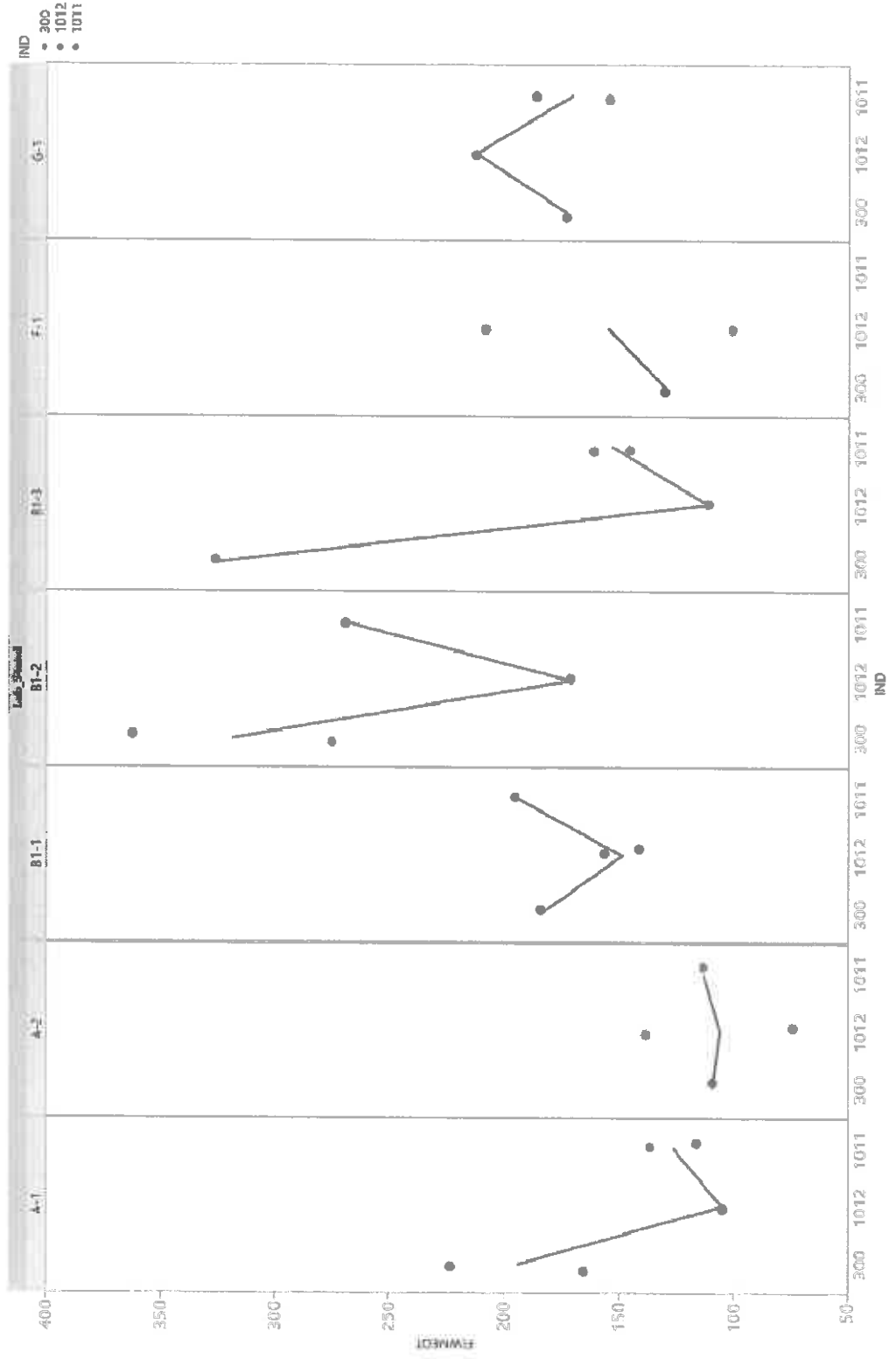
Fe-Wear Metals at EOT by Oil

- There is considerable overlap among the oils.



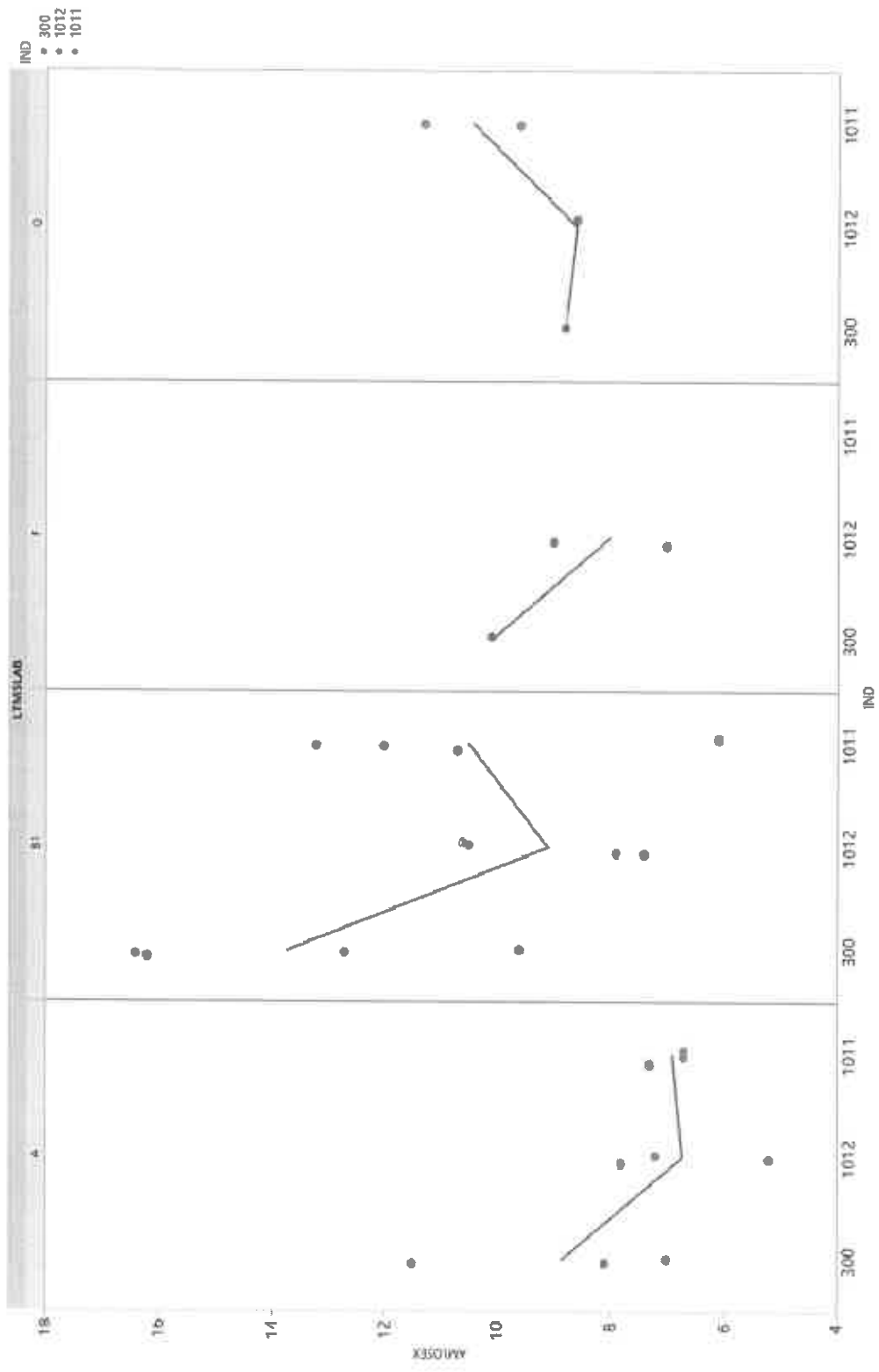
Fe-Wear Metals at EOT by Stand

- It appears that oil discrimination is not consistent among the stands; Stands rank oils differently



Fe-Wear Metals at EOT by Lab

- Below plot summarizes the FEWMEOT test result data by test Lab and reference oil



Ln(FEWMEOT) ANOVA Full Model

Statistically significant differences:

- Lab

Borderline significantly different:

- Oil

Not significantly different:

- Stands within Labs

Summary of Fit

| | |
|----------------------------|----------|
| RSquare | 0.624999 |
| RSquare Adj | 0.467104 |
| Root Mean Square Error | 0.270142 |
| Mean of Response | 5.08419 |
| Observations (or Sum Wgts) | 28 |

Analysis of Variance

| Source | DF | Sum of Squares | Mean Square | F Ratio |
|----------|----|----------------|-------------|----------|
| Model | 8 | 2.3109226 | 0.288865 | 3.9583 |
| Error | 19 | 1.3865568 | 0.072977 | Prob > F |
| C. Total | 27 | 3.6974793 | | 0.0066* |

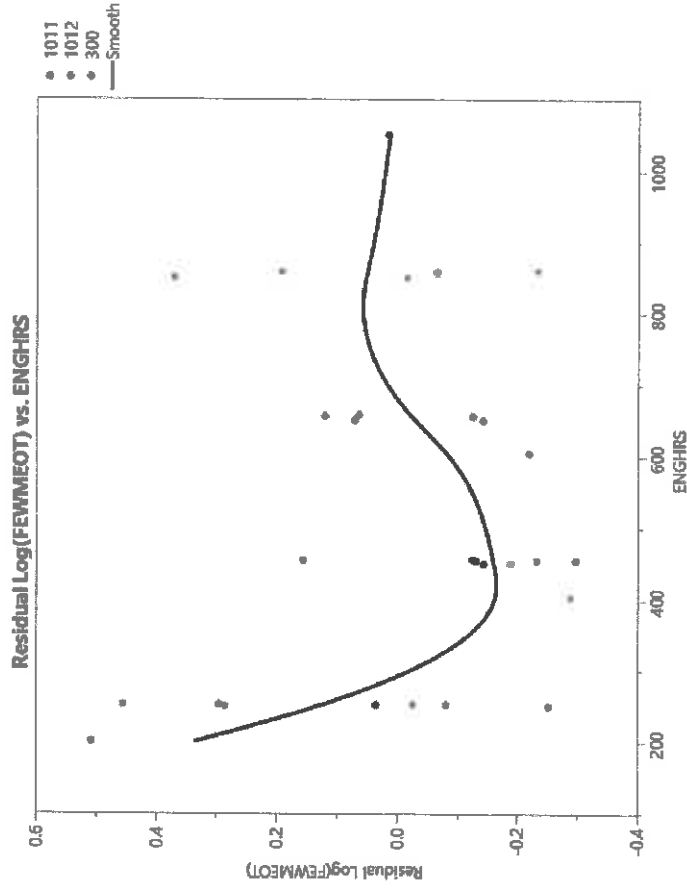
Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob > t |
|------------------------|-----------|-----------|---------|-----------|
| Intercept | 5.0668785 | 0.060112 | 84.29 | <.0001* |
| IND[300] | 0.1830866 | 0.074382 | 2.46 | 0.0236* |
| IND[1012] | -0.142024 | 0.075391 | -1.88 | 0.0750 |
| LTMSLAB[A] | -0.248739 | 0.087711 | -2.84 | 0.0106* |
| LTMSLAB[B1] | 0.206947 | 0.081573 | 2.54 | 0.0201* |
| LTMSLAB[F] | -0.09474 | 0.130769 | -0.72 | 0.4776 |
| LTMSLAB[A]:LTMSAPP[1] | 0.12012 | 0.092183 | 1.30 | 0.2081 |
| LTMSLAB[B1]:LTMSAPP[1] | -0.116682 | 0.111884 | -1.04 | 0.3101 |
| LTMSLAB[B1]:LTMSAPP[2] | 0.2416003 | 0.111842 | 2.16 | 0.0437* |

Effect Tests

| Source | Nparm | DF | Sum of Squares | F Ratio | Prob > F |
|------------------|-------|----|----------------|---------|----------|
| IND | 2 | 2 | 0.4918296 | 3.3698 | 0.0559 |
| LTMSLAB | 3 | 3 | 1.1459568 | 5.2344 | 0.0084* |
| LTMSAPP[LTMSLAB] | 3 | 3 | 0.4590705 | 2.0969 | 0.1345 |

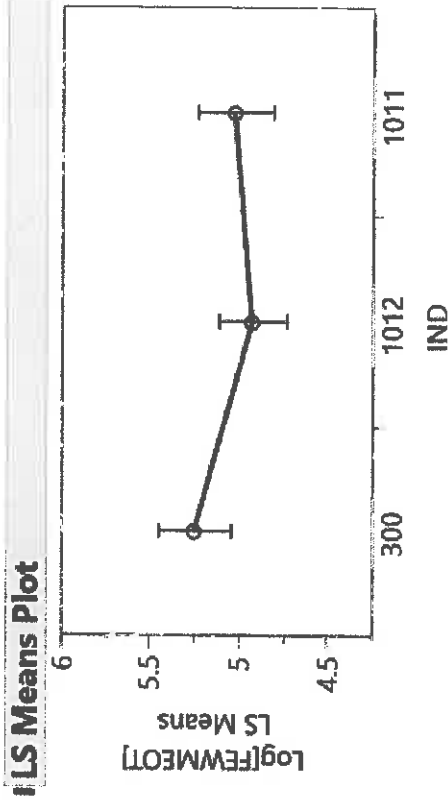
Engine Hours Adjustment



- The residuals of $\text{Ln}(\text{FEWMEOT})$ visually do not appear to be uniformly distributed on Engine Hours. (Engine Runs 2 and 3 appear to correlate with lower Fe than Runs 1 and 4)
- Engine Hours was added to the regression model in the following formats along with the result:
 - Engine Hours – Engine Hours not statistically significant and Oil borderline statistically significant.
 - Engine Run (Categorical) - Engine Run borderline statistically significant and Oil statistically significant.
 - Engine Run 1 and Others (Categorical) – Engine Run not statistically significant and Oil statistically significant.
 - Engine Run 1, 4 & 5 and 2 & 3 (Categorical) – Engine Run statistically significant and Oil statistically significant.
- More data is required to verify the pattern and establish for Runs 5 and higher.

Ln(FEWMEOT) Oil Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Oils significantly differ
 - Oil 300 is borderline significantly different than oil 1012
 - Oil 1011 is not statistically significantly different than oils 300 and 1012
- Plot shows $\text{Ln}(\text{FEWMEOT})$ LSMeans by Oil, with 95% confidence intervals



LSMeans by Oil

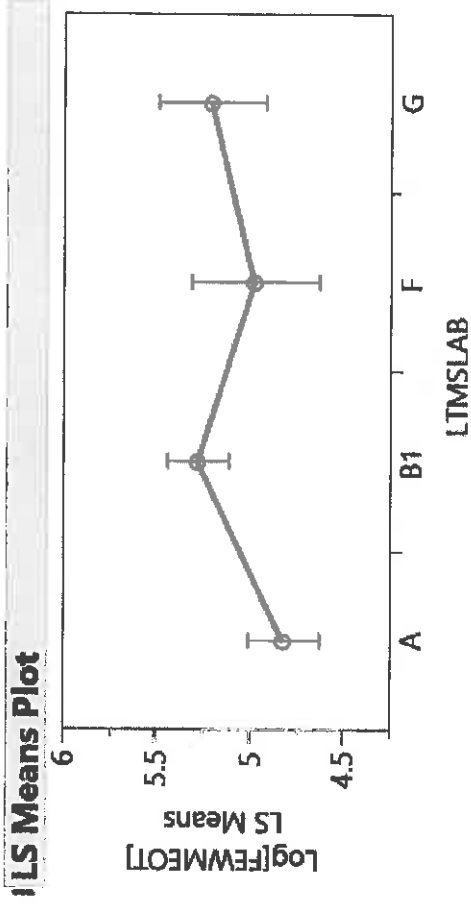
| Oil | Ln(FEWMEOT) LSMean | FEWMEOT LSMean |
|------|--------------------|----------------|
| 300 | 5.2500 | 191 |
| 1012 | 4.9249 | 138 |
| 1011 | 5.0258 | 152 |

LSMeans Differences Between Oils

| Oil1 | Oil2 | Ln(FEWMEOT) LSMean Difference | p-Value |
|------|------|-------------------------------|---------|
| 300 | 1012 | 0.3251 | 0.0508 |
| 300 | 1011 | 0.2241 | 0.2292 |
| 1011 | 1012 | 0.1010 | 0.7325 |

Ln(FEWMEOT) Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Plot below of $\text{Ln}(\text{FEWMEOT})$ LSMeans by Lab, with 95% confidence intervals
- Lab A is statistically significantly different than Lab B1.



LSMeans by Lab

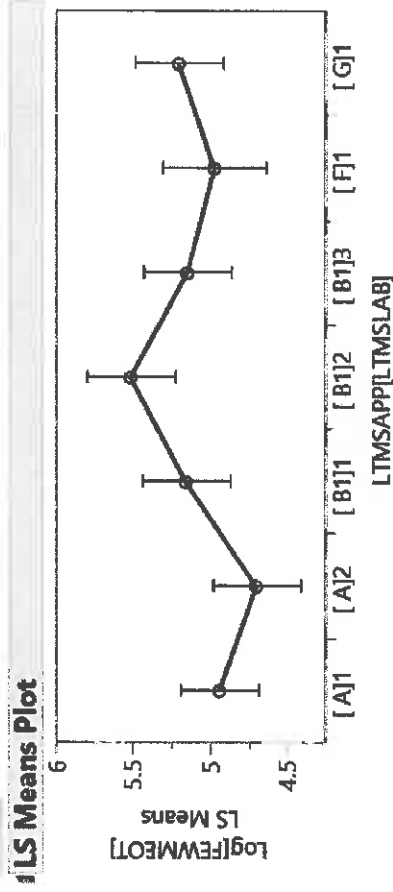
| Lab | Ln(FEWMEOT) LS Mean | FEWMEOT LS Mean |
|-----|---------------------|-----------------|
| A | 4.8181 | 124 |
| B1 | 5.2738 | 195 |
| F | 4.9721 | 144 |
| G | 5.2034 | 182 |

LSMeans Differences Between Labs

| Lab1 | Lab2 | Ln(FEWMEOT) LS Mean Difference | p-Value |
|------|------|--------------------------------|---------|
| B1 | A | 0.4557 | 0.01 |
| G | A | 0.3853 | 0.12 |
| B1 | F | 0.3017 | 0.36 |
| G | F | 0.2313 | 0.71 |
| F | A | 0.1540 | 0.84 |
| B1 | G | 0.0704 | 0.97 |

Ln(FEWMEOT) Stand within Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand(Lab)}$
- Plot below of $\text{Ln}(\text{FEWMEOT})$ LSMeans by Stand, with 95% confidence intervals
- Stands within labs are not statistically significantly different from each other



LSMeans by Stand

| Stand | Ln(FEWMEOT) LSMean | FEWMEOT LSMean |
|--------|--------------------|----------------|
| [A]1 | 4.9383 | 140 |
| [A]2 | 4.6980 | 110 |
| [B]1]1 | 5.1571 | 174 |
| [B]1]2 | 5.5154 | 248 |
| [B]1]3 | 5.1489 | 172 |
| [F]1 | 4.9721 | 144 |
| [G]1 | 5.2034 | 182 |

LSMeans Differences Between Stands within a Lab

| Stand1 | Stand2 | Ln(FEWMEOT) LSMean Difference | p-Value |
|--------|--------|-------------------------------|---------|
| [B]1]2 | [B]1]3 | 0.3665 | 0.51 |
| [B]1]2 | [B]1]1 | 0.3583 | 0.53 |
| [A]1 | [A]2 | 0.2402 | 0.84 |
| [B]1]1 | [B]1]3 | 0.0082 | 1 |

Ln(FEWMEOT) Precision

Repeatability Model: Ln(FEWMEOT) ~ Oil, Lab, Stand(Lab)
Reproducibility Model: Ln(FEWMEOT) ~ Oil

Model RMSE

- $S_r = 0.2701$

Repeatability

- $S_r = 0.2701$
- $r = 0.7487$

Reproducibility

- $S_R = 0.3426$
- $R = 0.9496$

Based upon the FEWMEOT pooled standard deviation (S_r) and ASTM's repeatability (r), there is no significant difference between an FEWMEOT result¹ of 200 and 423.

Note 1: An FEWMEOT result of 200 was arbitrarily selected for comparison

Reference Oil Targets

Model: $\text{Ln}(\text{FEWMEO}) \sim \text{Oil, Lab, Stand(Lab)}$

Iron at EOT (FEWMEO)

Unit of Measure: $\text{Ln}(\text{FEWMEO})$

| Ref. Oil | Target Mean $\text{Ln}(\text{FEWMEO})$ | Target Mean FEWMEO | St. Dev |
|----------|---|-----------------------|---------|
| 300 | 5.2500 | 191 | 0.4067 |
| 1012 | 4.9249 | 138 | 0.3365 |
| 1011 | 5.0258 | 152 | 0.2722 |

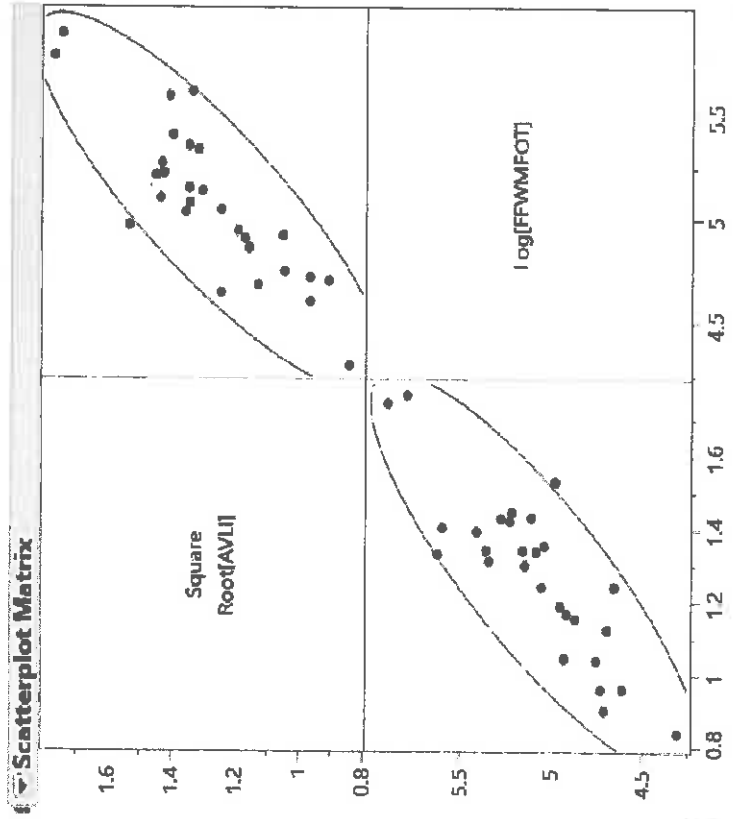
Target Means are the Oil LSMeans from the Model and Standard Deviations are calculated straight from $\text{Ln}(\text{FEWMEO})$.

Correlation

Appendix K Section A.3 Parameter Redundancy: Correlation between $\text{sqrt}(\text{AVLI})$ and $\text{Ln}(\text{FEWMEOT})$ is statistically significant. These two parameters are closely related in repeat tests within oils.

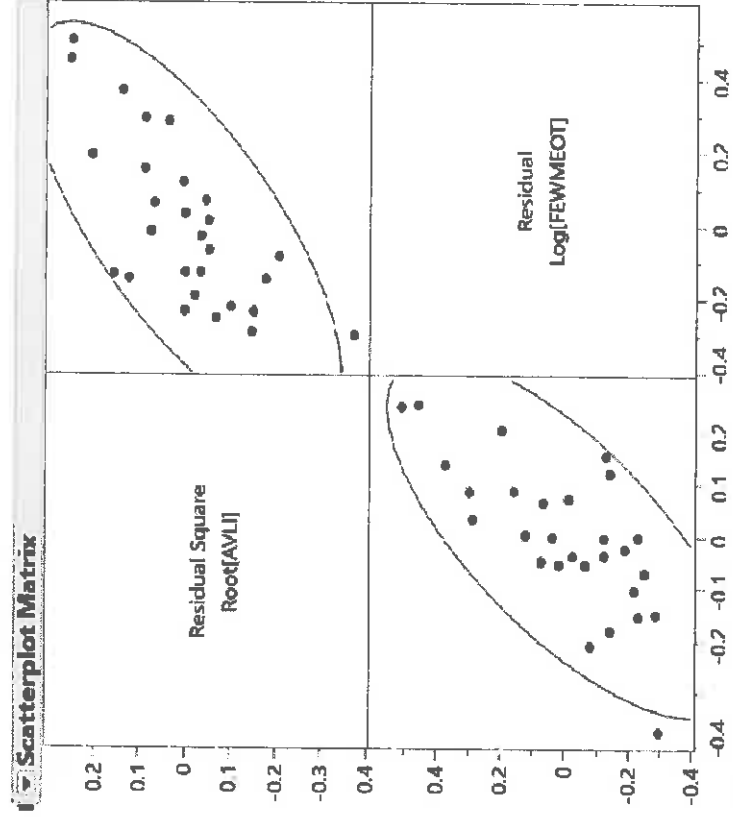
Correlations

| | | | |
|-------------------|--------|--------------------------------|--------|
| Square Root[AVLI] | 1.0000 | Square Root[AVLI] Log[FEWMEOT] | 0.8526 |
| Log[FEWMEOT] | 0.8526 | Log[FEWMEOT] | 1.0000 |



Correlations

| | | | |
|----------------------------|--------|--|--------|
| Residual Square Root[AVLI] | 1.0000 | Residual Square Root[AVLI] Residual Log[FEWMEOT] | 0.7272 |
| Residual Log[FEWMEOT] | 0.7272 | Residual Log[FEWMEOT] | 1.0000 |



Calcium Adj FEWMEOT (n=28)

Fe-Wear Metals at end of test

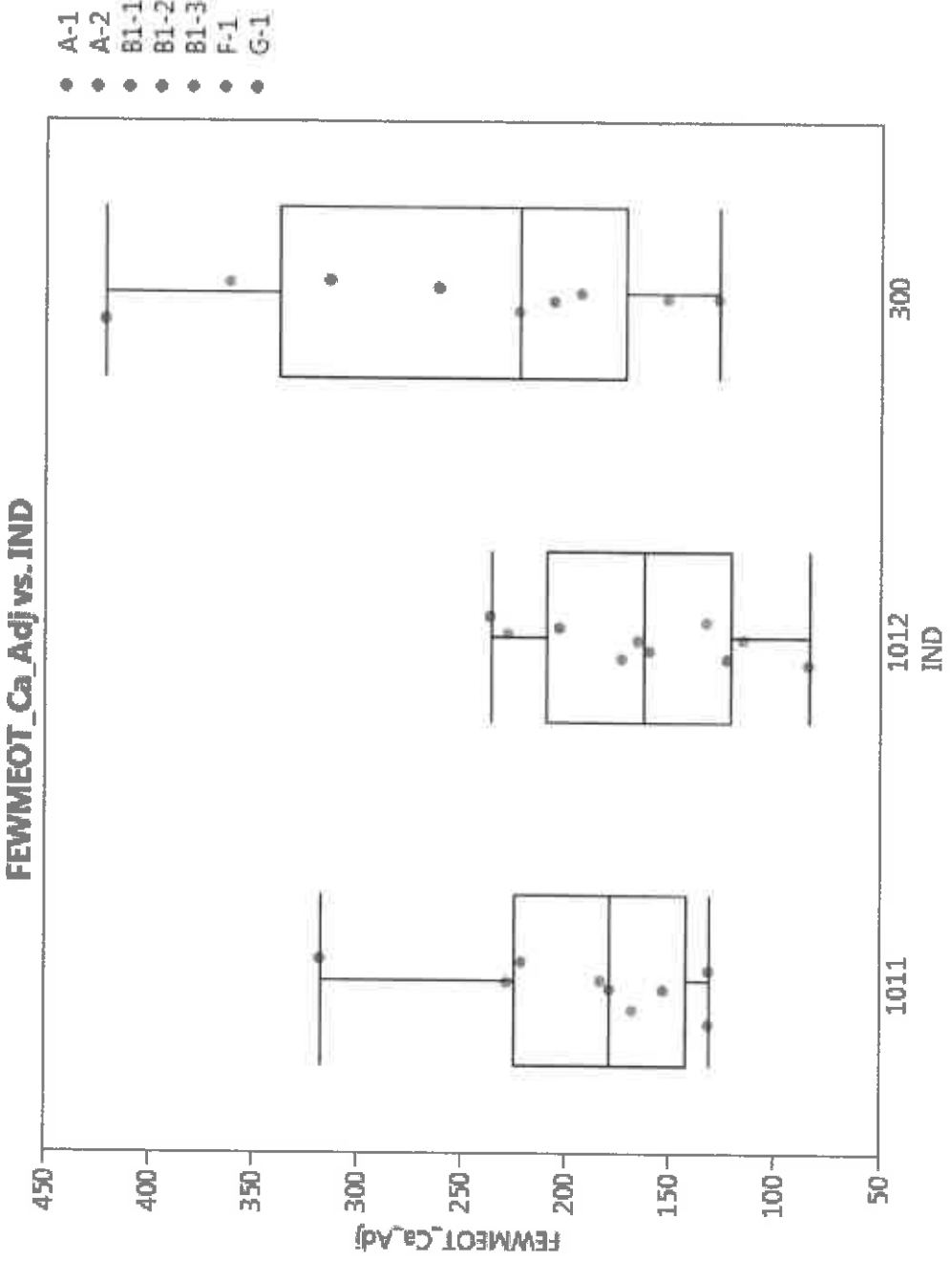
Fe-Wear Metals - Correction Approach

- Method Summary:
 - Calcium concentration is believed to remain constant from SOT to EOT
 - Reference ASTM 7320 - Sequence IIIGB for more information
 - Changes in Ca levels can be due to volatility or dilution (i.e. fuel, water, etc.)
 - Ratio of (Ca_SOT/Ca_EOT) is used to correct the FEWM/EOT data to equivalent SOT levels
 - Example of correction calculations are provided below

| TESTKEY | LTMSLAB | Stand | RefOil | ENGRHS | FEWM/EOT | Ca_SOT | Ca_EOT | Ca_SOT/Ca_EOT | FEWM/EOT | Ca_Adj | AVLI |
|------------|---------|-------|--------|--------|----------|--------|--------|---------------|----------|--------|------|
| 127173-IVB | B1 | S1 | RO1012 | 254 | 156 | 2400 | 2168 | 1.1070 | 172.7 | 1.55 | |
| 129759-IVB | B1 | S2 | RO300 | 254 | 275 | 2029 | 1781 | 1.1392 | 313.3 | 1.78 | |
| 125879-IVB | B1 | S3 | RO1011 | 254 | 161 | 2111 | 1861 | 1.1343 | 182.6 | 1.8 | |
| 125882-IVB | A | S2 | RO1012 | 252 | 74 | 2449 | 2163 | 1.1322 | 83.8 | 0.71 | |
| 129752-IVB | A | S1 | RO300 | 252 | 223 | 2076 | 1773 | 1.1709 | 261.1 | 1.95 | |
| 129762-IVB | B1 | S1 | RO1011 | 456 | 195 | 2107 | 1805 | 1.1673 | 227.6 | 2.05 | |
| 129766-IVB | B1 | S2 | RO1012 | 456 | 171 | 2439 | 2058 | 1.1851 | 202.7 | 1.7 | |
| 129767-IVB | B1 | S3 | RO1012 | 456 | 111 | 2419 | 2035 | 1.1887 | 131.9 | 0.82 | |
| 130948-IVB | A | S2 | RO300 | 452 | 109 | 2069 | 1783 | 1.1604 | 126.5 | 1.27 | |
| 129760-IVB | B1 | S1 | RO300 | 658 | 184 | 2056 | 1700 | 1.2094 | 222.5 | 2.1 | |
| 129763-IVB | B1 | S2 | RO1011 | 658 | 269 | 2137 | 1811 | 1.1800 | 317.4 | 1.98 | |
| 109201-IVB | A | S1 | RO1011 | 452 | 116 | 2115 | 1878 | 1.1262 | 130.6 | 1.09 | |
| 130944-IVB | G | S1 | RO1012 | 254 | 212 | 2521 | 2264 | 1.1135 | 236.1 | 1.81 | |
| 125183-IVB | F | S1 | RO1012 | 202 | 208 | 2396 | 2192 | 1.0931 | 227.4 | 1.73 | |
| 129768-IVB | B1 | S1 | RO1012 | 860 | 141 | 2401 | 2052 | 1.1701 | 165 | 1.42 | |
| 130938-IVB | B1 | S2 | RO300 | 860 | 362 | 2009 | 1726 | 1.1640 | 421.4 | 3.05 | |
| 129755-IVB | A | S1 | RO1012 | 652 | 105 | 2496 | 2148 | 1.1620 | 122 | 1.55 | |
| 125184-IVB | G | S1 | RO1011 | 458 | 154 | 2129 | 1840 | 1.1571 | 178.2 | 1.84 | |
| 125880-IVB | A | S2 | RO1011 | 652 | 113 | 2159 | 1866 | 1.1570 | 130.7 | 0.93 | |
| 130939-IVB | B1 | S3 | RO300 | 254 | 326 | 1993 | 1798 | 1.1085 | 361.4 | 3.13 | |
| 120739-IVB | F | S1 | RO300 | 404 | 130 | 1988 | 1711.7 | 1.1614 | 151 | 1.34 | |
| 131277-IVB | A | S1 | RO300 | 852 | 165 | 2100 | 1798 | 1.1680 | 192.7 | 2.06 | |
| 129756-IVB | A | S2 | RO1012 | 852 | 138 | 2478 | 2145 | 1.1552 | 159.4 | 1.1 | |
| 130943-IVB | G | S1 | RO1011 | 660 | 186 | 2186 | 1842 | 1.1868 | 220.7 | 2.03 | |
| 129764-IVB | B1 | S3 | RO1011 | 456 | 145 | 2094 | 1816 | 1.1531 | 167.2 | 2.35 | |
| 130940-IVB | G | S1 | RO300 | 862 | 173 | 2102 | 1767 | 1.1896 | 205.8 | 1.81 | |
| 130945-IVB | F | S1 | RO1012 | 606 | 101 | 2442.3 | 2158.1 | 1.1317 | 114.3 | 0.93 | |
| 125881-IVB | A | S1 | RO1011 | 1052 | 136 | 2121 | 1894 | 1.1199 | 152.3 | 1.37 | |

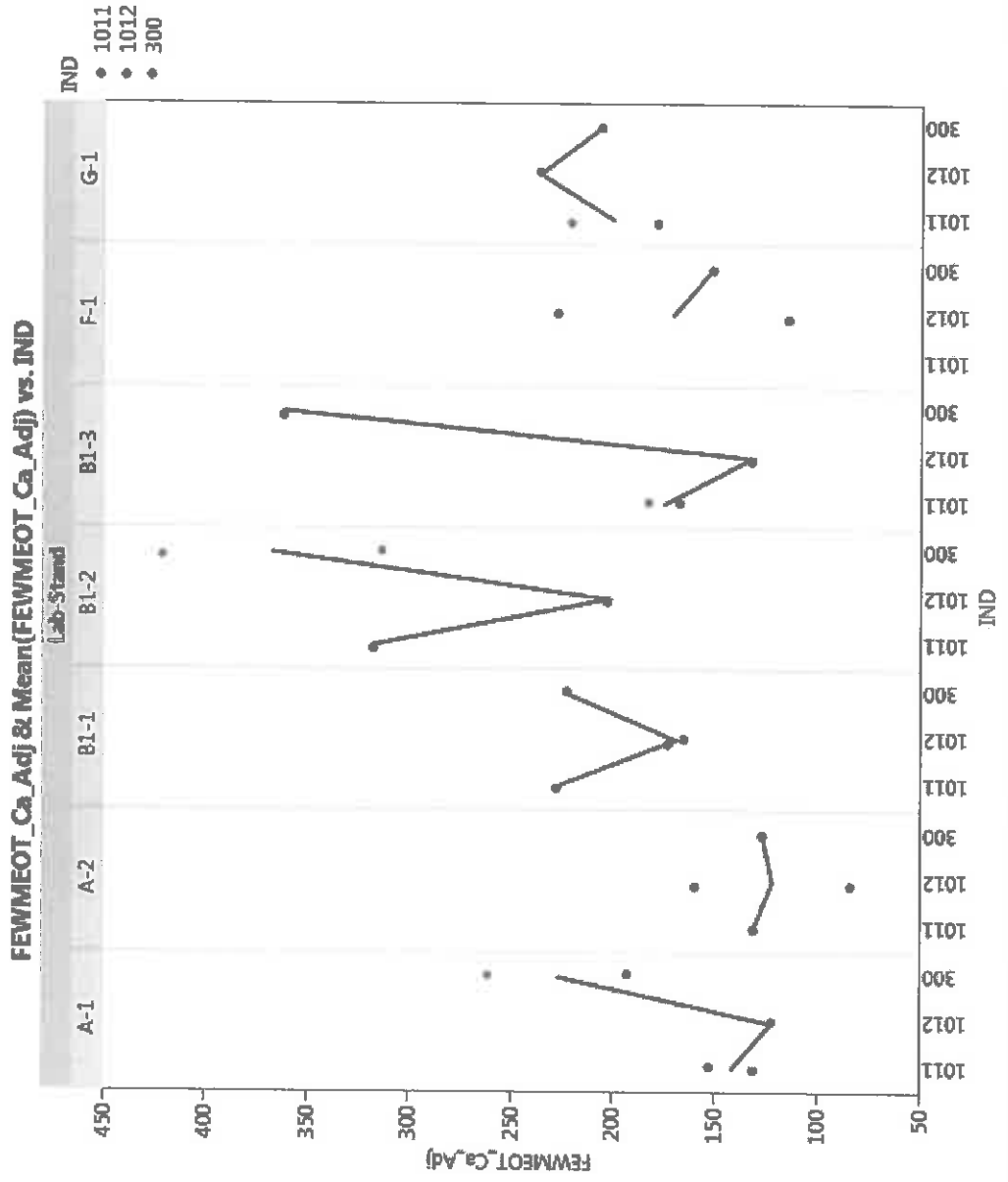
Calcium_Adj_Fe-Wear Metals at EOT by Oil

- There is considerable overlap among the oils.



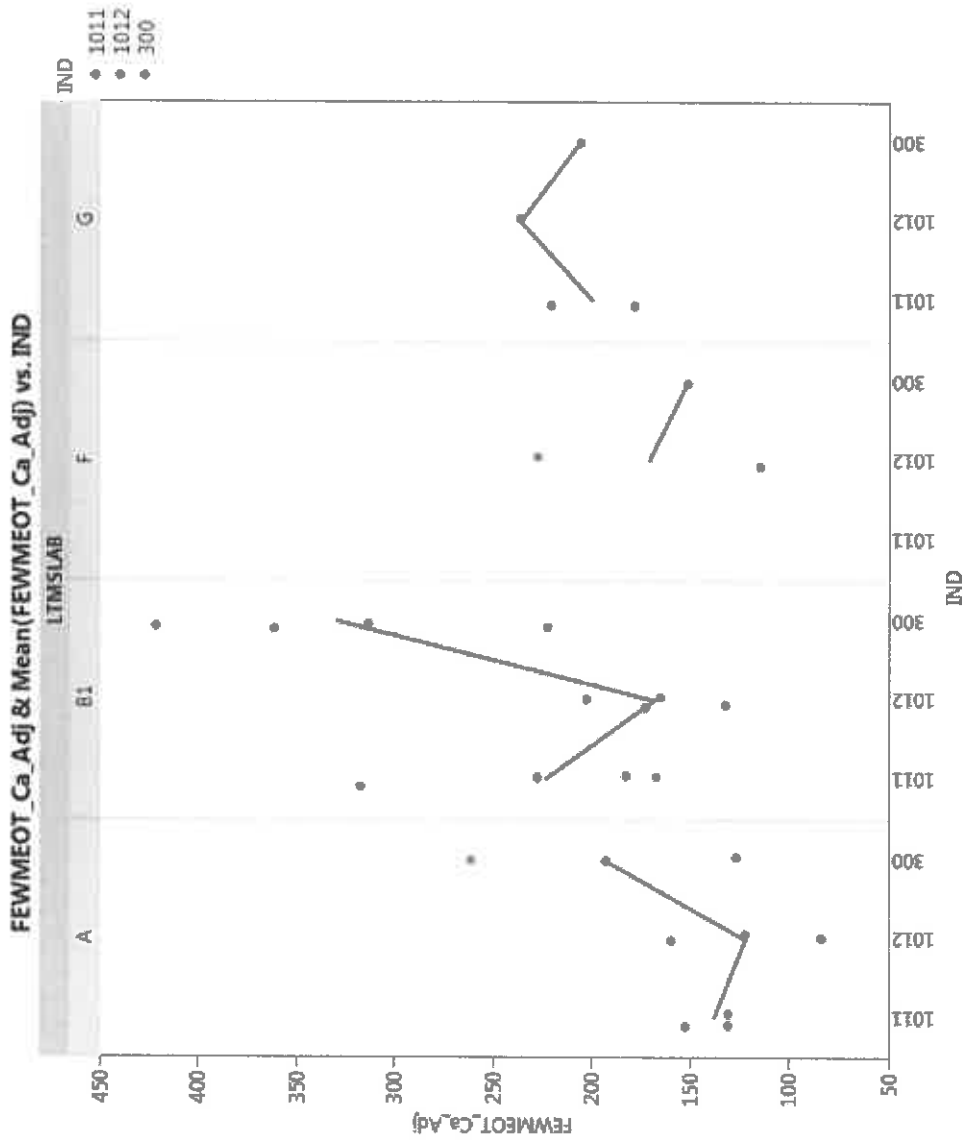
Calcium_Adj_Fe-Wear Metals at EOT by Stand

- It appears that oil discrimination is not consistent among the stands; Stands rank oils differently



Calcium_Adj_Fe-Wear Metals at EOT by Lab

- Below plot summarizes the FEWM EOT_Ca_Adj test result data by test Lab and reference oil



Ln(FEWMEOT_Ca_Adj) - ANOVA Full Model

Statistically significant differences:

- Lab, Oil

Not significantly different:

- Stands within Labs

Summary of Fit

| | |
|----------------------------|----------|
| RSquare | 0.657934 |
| RSquare Adj | 0.513907 |
| Root Mean Square Error | 0.258386 |
| Mean of Response | 5.226639 |
| Observations (or Sum Wgts) | 28 |

Analysis of Variance

| Source | DF | Squares | Mean Square | F Ratio |
|----------|----|-----------|-------------|----------|
| Model | 8 | 2.4398569 | 0.304982 | 4.5681 |
| Error | 19 | 1.2685020 | 0.066763 | Prob > F |
| C. Total | 27 | 3.7083589 | | 0.0031* |

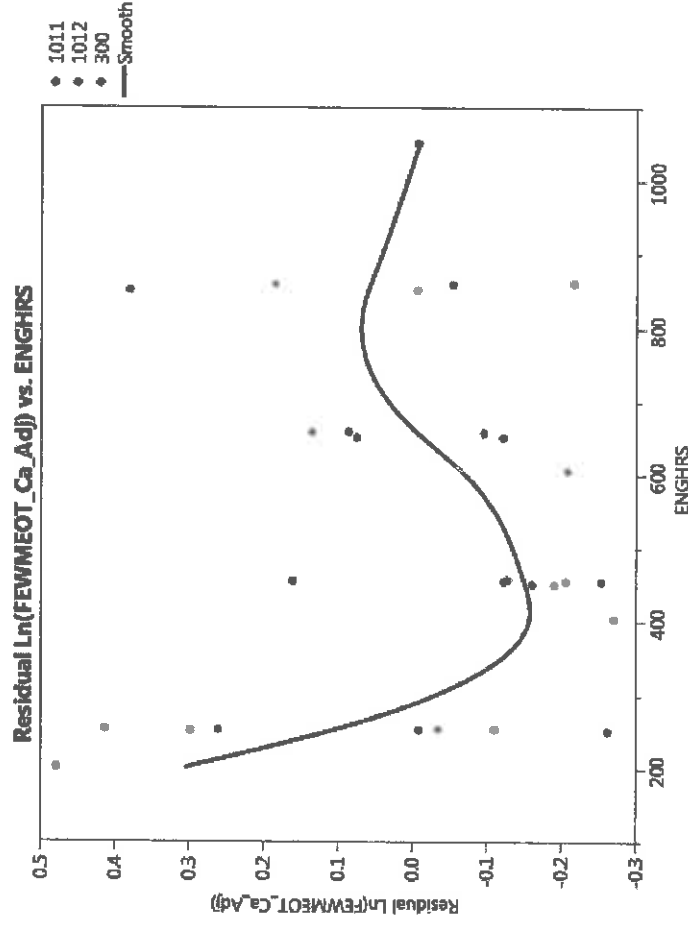
Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob > t |
|------------------------|-----------|-----------|---------|-----------|
| Intercept | 5.2072249 | 0.057496 | 90.57 | <.0001* |
| RefOil[[RO101]] | -0.042438 | 0.073795 | -0.58 | 0.5720 |
| RefOil[[RO1012]] | -0.149076 | 0.07211 | -2.07 | 0.0526 |
| LTMSLAB[A] | -0.249068 | 0.083894 | -2.97 | 0.0079* |
| LTMSLAB[B1] | 0.2137059 | 0.078023 | 2.74 | 0.0130* |
| LTMSLAB[F] | -0.11074 | 0.125078 | -0.89 | 0.3870 |
| LTMSLAB[A]:Stand[S1] | 0.1176384 | 0.088171 | 1.33 | 0.1979 |
| LTMSLAB[B1]:Stand[S1] | -0.111157 | 0.107015 | -1.04 | 0.3120 |
| LTMSLAB[B1]:Stand[S2] | 0.246849 | 0.106975 | 2.31 | 0.0324* |

Effect Tests

| Source | Nparm | DF | Sum of Squares | F Ratio | Prob > F |
|----------------|-------|----|----------------|---------|----------|
| RefOil | 2 | 2 | 0.5391278 | 4.0376 | 0.0346* |
| LTMSLAB | 3 | 3 | 1.1972860 | 5.9778 | 0.0048* |
| Stand[LTMSLAB] | 3 | 3 | 0.4703869 | 2.3485 | 0.1049 |

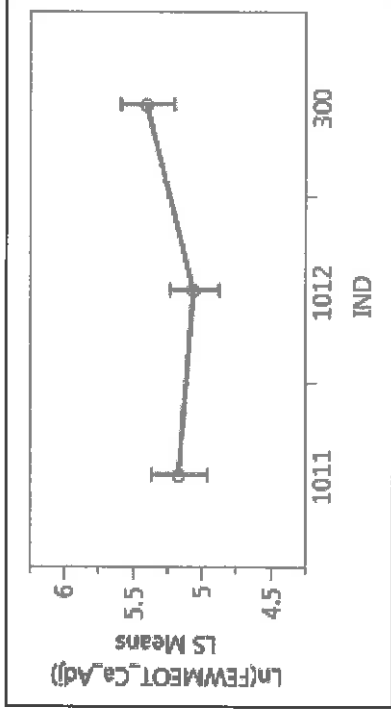
Engine Hours Adjustment



- The residuals of Ln(FEWMEOT_Ca_Adj) visually do not appear to be uniformly distributed on Engine Hours. (Engine Runs 2 and 3 appear to correlate with lower Fe than Runs 1 and 4)
- Engine Hours was added to the regression model in the following formats along with the result:
 - Engine Hours – Engine Hours not statistically significant and Oil statistically significant.
 - Engine Run (Categorical) – Engine Run not statistically significant and Oil statistically significant.
- More data is required to verify the pattern and establish for Runs 5 and higher.

Ln(FEWMEOT_Ca_Adj) Oil Differences

- Model is $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Oils significantly differ
 - Oil 300 is significantly different than oil 1012
 - Oil 1011 is not statistically significantly different than oils 300 and 1012
- Plot shows $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ LSMeans by Oil, with 95% Confidence Interval



LSMeans by Oil

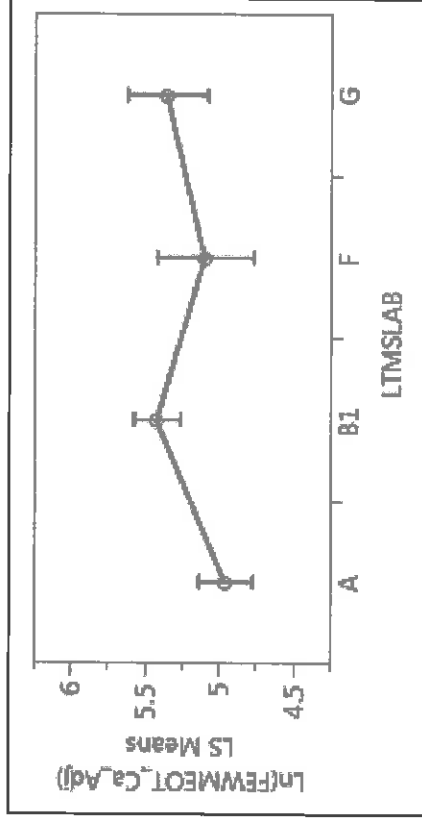
| Oil | Ln(FEWMEOT_Ca_Adj) LSMean | FEWMEOT_Ca_Adj LSMean |
|------|---------------------------|-----------------------|
| 1011 | 5.1648 | 175 |
| 1012 | 5.0581 | 157 |
| 300 | 5.3987 | 221 |

LSMeans Differences Between Oils

| Oil1 | Oil2 | Ln(FEWMEOT_Ca_Adj) LS Mean Difference | p-Value |
|------|------|---------------------------------------|---------|
| 300 | 1012 | 0.3406 | 0.0310 |
| 300 | 1011 | 0.2339 | 0.1775 |
| 1011 | 1012 | 0.1066 | 0.6852 |

Ln(FEWMEOT_Ca_Adj) Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Plot below of $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ LSMeans by Lab, with 95% confidence intervals
- Lab A is statistically significantly different than Lab B1.



LSMeans by Lab

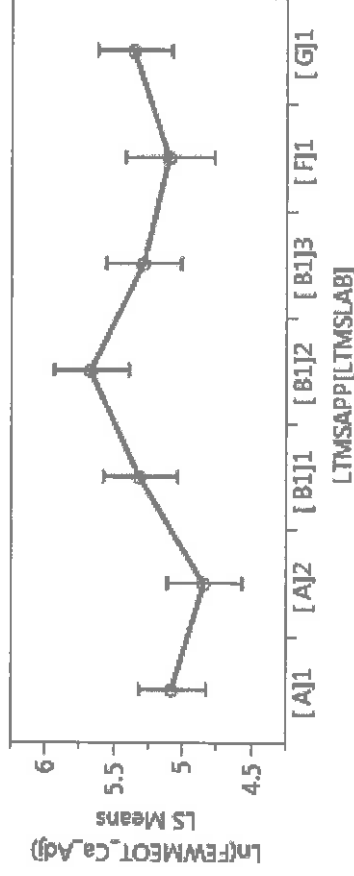
| Lab | Ln(FEWMEOT_Ca_Adj) LS Mean | FEWMEOT_Ca_Adj LS Mean |
|-----|----------------------------|------------------------|
| A | 4.9581 | 142 |
| B1 | 5.4209 | 226 |
| F | 5.0965 | 163 |
| G | 5.3533 | 211 |

LSMeans Differences Between Labs

| Lab1 | Lab2 | Ln(FEWMEOT_Ca_Adj) LSMean Difference | p-Value |
|------|------|--------------------------------------|---------|
| B1 | A | 0.4628 | 0.0035 |
| G | A | 0.3952 | 0.0886 |
| B1 | F | 0.3244 | 0.2672 |
| G | F | 0.2568 | 0.6063 |
| F | A | 0.1383 | 0.8625 |
| B1 | G | 0.0676 | 0.9689 |

Ln(FEWMEOT_Ca_Adj) Stand within Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand(Lab)}$
- Plot below of $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ LSMeans by Stand, with 95% confidence intervals
- Stands within labs are not statistically significantly different from each other



LSMeans by Stand

| Level | Ln(FEWMEOT_Ca_Adj) LS Mean | FEWMEOT_Ca_Adj LS Mean |
|-------|----------------------------|------------------------|
| [A]1 | 5.0758 | 160 |
| [A]2 | 4.8405 | 127 |
| [B]1 | 5.3098 | 202 |
| [B]2 | 5.6678 | 289 |
| [B]3 | 5.2852 | 197 |
| [F]1 | 5.0965 | 163 |
| [G]1 | 5.3533 | 211 |

LSMeans Differences Between Stands within a Lab

| Lab_Stand1 | Lab_Stand2 | Ln(FEWMEOT_Ca_Adj) LS Mean Difference | p-Value |
|------------|------------|---------------------------------------|---------|
| [B]2 | [B]3 | 0.3825 | 0.4108 |
| [B]2 | [B]1 | 0.3580 | 0.4847 |
| [A]1 | [A]2 | 0.2353 | 0.8278 |
| [B]1 | [B]3 | 0.0245 | 1.0000 |

Ln(FEWMEOT_Ca_Adj) Precision

Repeatability Model: $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand(Lab)}$
Reproducibility Model: $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil}$

Model RMSE

- $S_r = 0.2584$

Repeatability

- $S_r = 0.2584$
- $r = 0.7162$

Reproducibility

- $S_R = 0.3395$
- $R = 0.9410$

Based upon the Ln(FEWMEOT_Ca_Adj) pooled standard deviation (S_r) and ASTM's repeatability (r), there is no significant difference between an FEWMEOT_Ca_Adj result¹ of 200 and 409.

Note 1: An FEWMEOT_Ca_Adj result of 200 was arbitrarily selected for comparison

Reference Oil Targets

Model: $\text{Ln}(\text{FEWMEOT_Ca_Adj}) \sim \text{Oil, Lab, Stand}(\text{Lab})$

Iron at EOT (FEWMEOT_Ca_Adj)

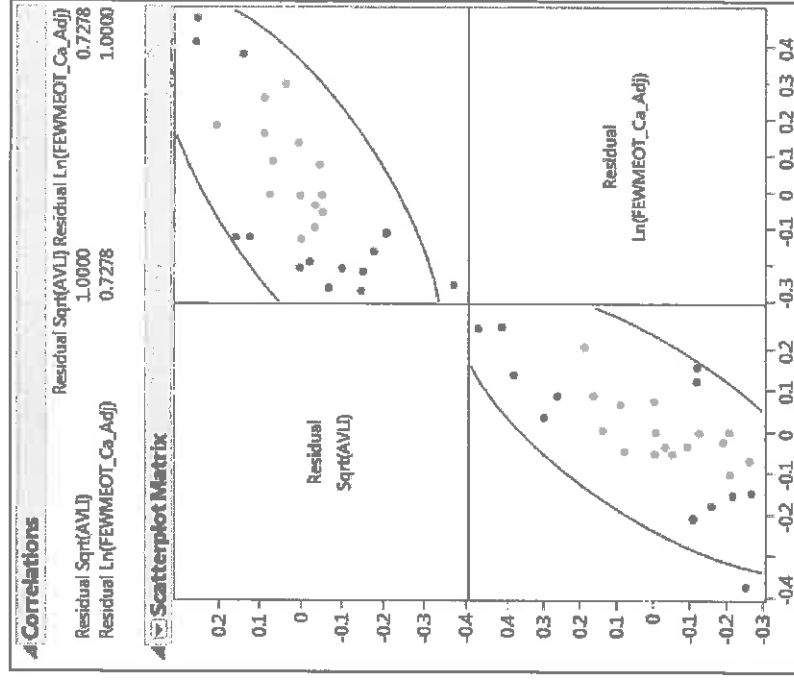
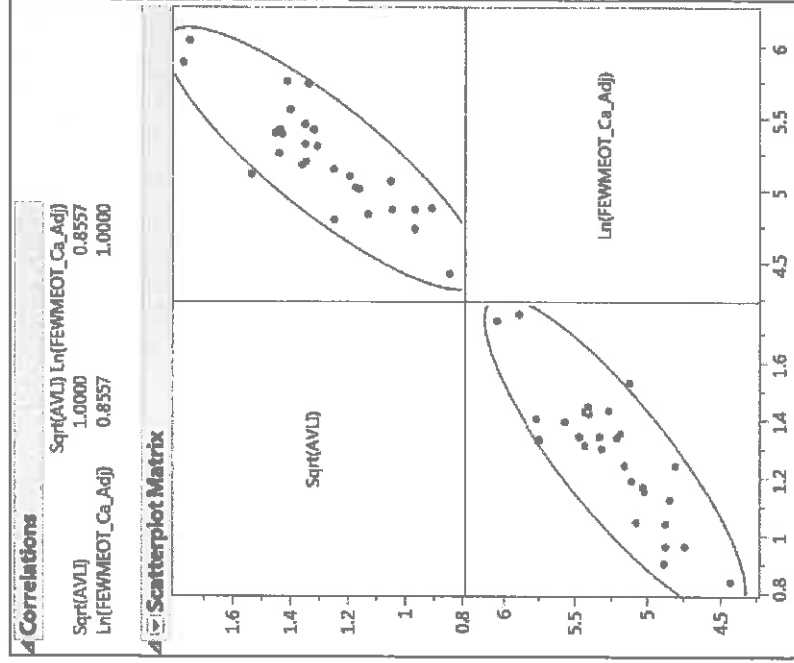
Unit of Measure: $\text{Ln}(\text{FEWMEOT_Ca_Adj})$

| Ref. Oil | Target Mean $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ | Target Mean FEWMEOT_Ca_Adj | St. Dev |
|----------|--|-------------------------------|---------|
| 300 | 5.3987 | 221 | 0.3967 |
| 1012 | 5.0581 | 157 | 0.3277 |
| 1011 | 5.1648 | 175 | 0.2863 |

Target Means are the Oil LSMeans from the Model and Standard Deviations are calculated straight from $\text{Ln}(\text{FEWMEOT_Ca_Adj})$.

Correlation

Appendix K Section A.3 Parameter Redundancy: Correlation between $\text{Sqrt}(\text{AVLI})$ and $\text{Ln}(\text{FEWMEOT_Ca_Adj})$ is statistically significant. These two parameters are closely related in repeat tests within oils.



Appendix A: FEWMEOT (n=21)

Fe- Wear Metals at end of test

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- This analysis includes the results of 21 valid precision matrix tests from independent laboratories
- Data supports the use of Ln(FEWMEOT) transformation
 - Significant oil difference: $1012 < 300$
 - Lab differences are statistically significant ($A < B1$)
 - Stand within Lab differences are not statistically significant
- Oil discrimination is better for FEWMEOt than FEWML25 (Fe increase over last 25 hours) and FEWML50 (Fe increase over last 50 hours).
- Correlation between sqrt(AVLI) and Ln(FEWMEOT) is high (parameter redundancy).

Executive Summary

Precision Matrix (PM) Analysis Highlights:

- Estimated within a stand test precision (r; ASTM repeatability)
 - $\text{Ln}(\text{FEWMEO}) = 0.6381$
- Estimated test precision across labs and stands (R; ASTM reproducibility)
 - $\text{Ln}(\text{FEWMEO}) = 0.9499$
- Oil means and standard deviations

| Oil | Number of Tests | Target Mean $\text{Ln}(\text{FEWMEO})$ | Target Mean FEWMEO | Target Standard Deviation $\text{Ln}(\text{FEWMEO})$ |
|------|-----------------|---|-----------------------|---|
| 300 | 7 | 5.3095 | 202 | 0.4204 |
| 1012 | 7 | 4.8146 | 123 | 0.2859 |
| 1011 | 7 | 5.0172 | 151 | 0.3064 |

- Same concerns with AVL I are seen in Fe analysis (discrimination not consistent among stands, test precision is large compared to the observed range of measurements)
- Calcium content data from all labs is not available at this time for adjusting iron content

Data Utilized

- Precision Matrix Data:
 - 2 Labs {A, B1}, independent labs only
 - 3 Reference Oils {300, 1012, and 1011}
 - 5 Stands {A-1, A-2, B1-1, B1-2, B1-3}
 - Total number of tests = 21
- Precision Matrix Data Table from Rich Grundza's 20180115 IVB Matrix update.

| Run order | B1-1 | B1-2 | B1-3 | A-1 | A-2 | F-1 | G-1 |
|-----------|--------------------|------------------------------|--|---|--------------------|------|--------------------|
| 1 | 1012 127173-IVB | 300 129759-IVB | 1011 125879-IVB | 300 129752-IVB | 1012 125882-IVB | | |
| 2 | 1011 129762-IVB | 1012 129766-IVB | 1012 129767-IVB | 1011 109201-IVB 1011* 125881-IVB | 300 130948-IVB | 1207 | 1011 |
| 3 | 300 129760-IVB | 1011 129763-IVB | 300 129761-IVB 300 130939-IVB | 1012 129755-IVB | 1011 125880-IVB | | 300 |
| 4 | 1012 129768-IVB | 300 129764-IVB | 1011 129764-IVB | 300 131277-IVB | 1012 129756-IVB | | 300# 130940-IVB |
| Reported | | | Invalid | | | | |

* Laboratory is running additional test because of Lean AFR and lower fuel flow on original matrix test

Additional test donated by lab

Reference Oil Discrimination Comparison

The table below compares the numbers of standard deviations of separation between the highest and lowest reference oil across GF-6 test types. The median of other tests is approx. 3.55 and the mean (without PHOS) is 3.99.

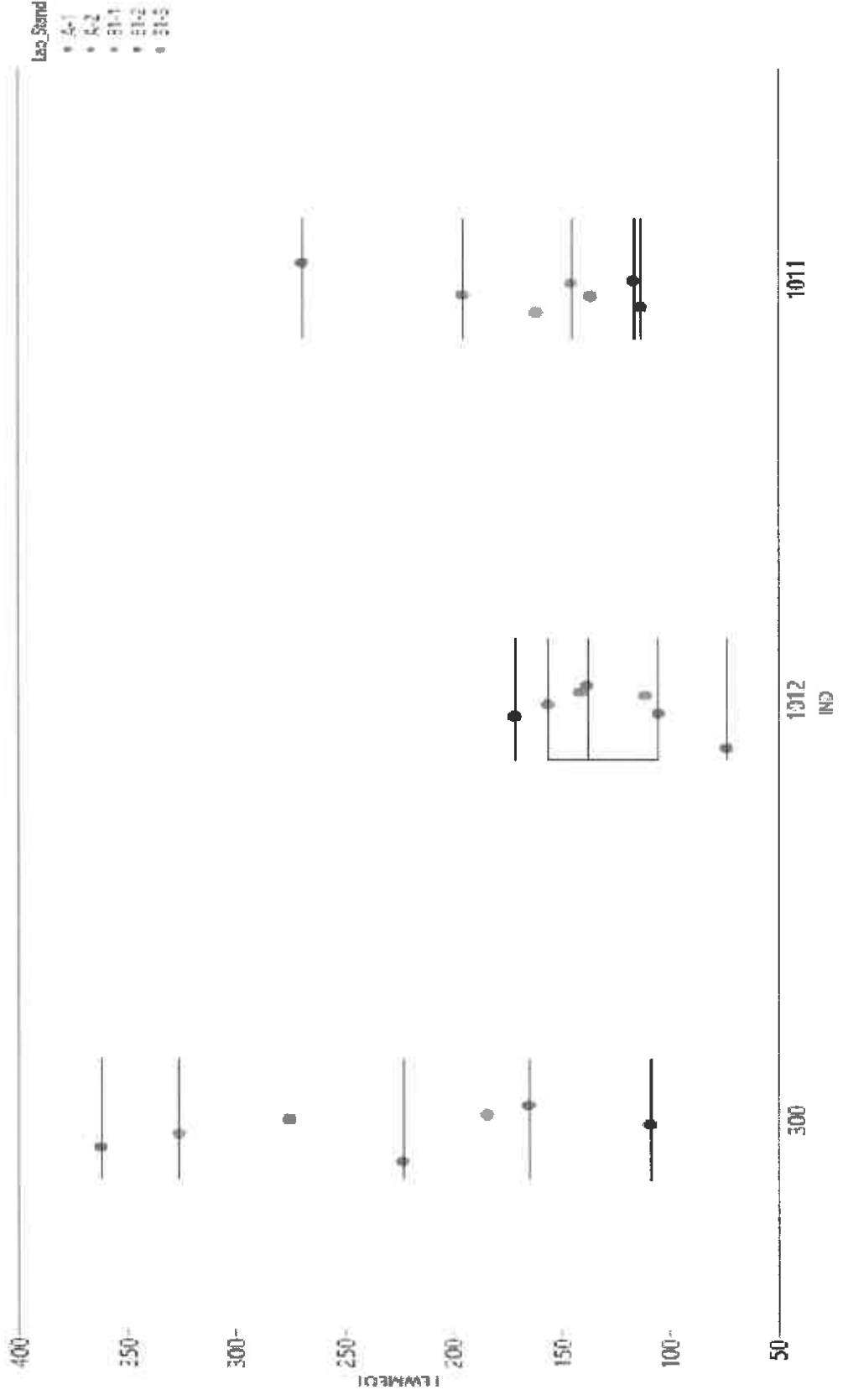
| Test | Parameter | Oil 1 | Oil 2 | Range | Test σ | SDs of Separation |
|-----------|-------------------|----------|----------|--------|---------------|-------------------|
| IIIH | Ln(PVIS) | 4.7191 | 3.3289 | 1.3902 | 0.4641 | 3.0 |
| IIIH | WPD | 4.63 | 3.66 | 0.97 | 0.47 | 2.1 |
| IIIIHA | Ln(MRV) | 11.1107 | 9.7854 | 1.3253 | 0.4214 | 3.1 |
| IIIIHB | PHOS | 94.15 | 78.92 | 15.23 | 1.53 | 10.0 |
| VIE | FEI 1 | 2.56 | 1.3 | 1.26 | 0.29 | 4.3 |
| VIE | FEI 2 | 1.82 | 1.41 | 0.41 | 0.12 | 3.4 |
| VIF | FEI 1 | 2.23 | 1.45 | 0.78 | 0.21 | 3.7 |
| VIF | FEI 2 | 2.25 | 1.41 | 0.84 | 0.19 | 4.4 |
| IX (LSPI) | Sqrt(AVPIE + 0.5) | 4.2644 | 3.3819 | 0.8825 | 0.2856 | 3.1*1 |
| VH | AES | 8.43 | 6.47 | 1.96 | 0.5 | 3.9 |
| VH | Ln(10-RCS) | 0.9155 | -0.5294 | 1.4449 | 0.2194 | 6.6 |
| VH | AEV50 | 9.26 | 8.77 | 0.49 | 0.25 | 2.0 |
| VH | APV50 | 8.67 | 7.35 | 1.32 | 0.53 | 2.5 |
| X (CW) | Ln(CHST) | -2.10574 | -2.63174 | 0.526 | 0.14148 | 3.7*2 |
| IVB | Sqrt(AVLI) | 1.4306 | 1.1104 | 0.3202 | 0.1657 | 1.9 |
| IVB | Ln(FEWMEOT) | 5.3095 | 4.8146 | 0.4949 | 0.2302 | 2.1 |

*1: Oil 220 not used as a reference oil. Including this oil would yield approx. 12 SDs of separation between 220 and 222.

*2: 271 vs. 1011

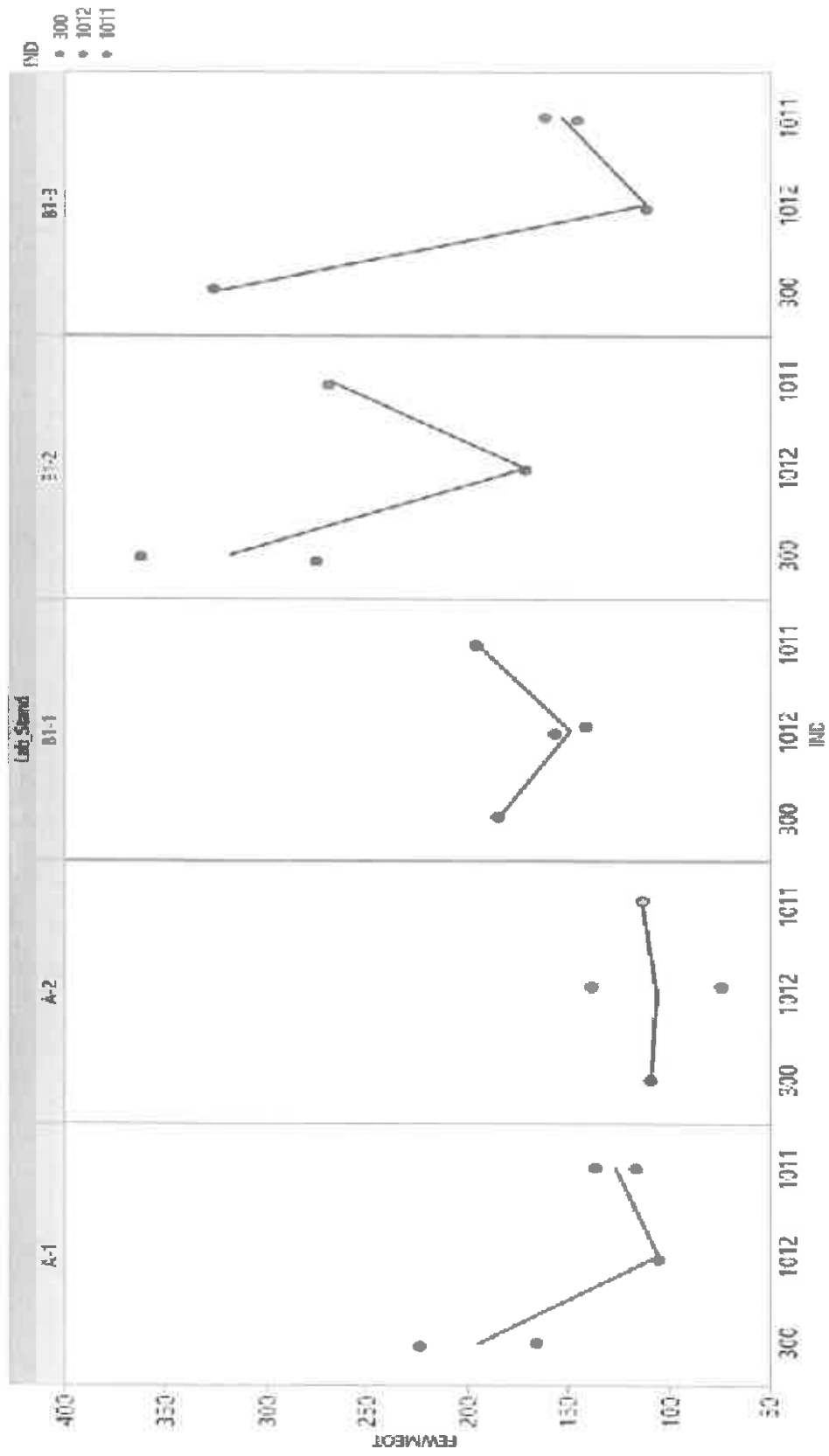
Fe-Wear Metals at EOT by Oil

- There is considerable overlap among the oils.



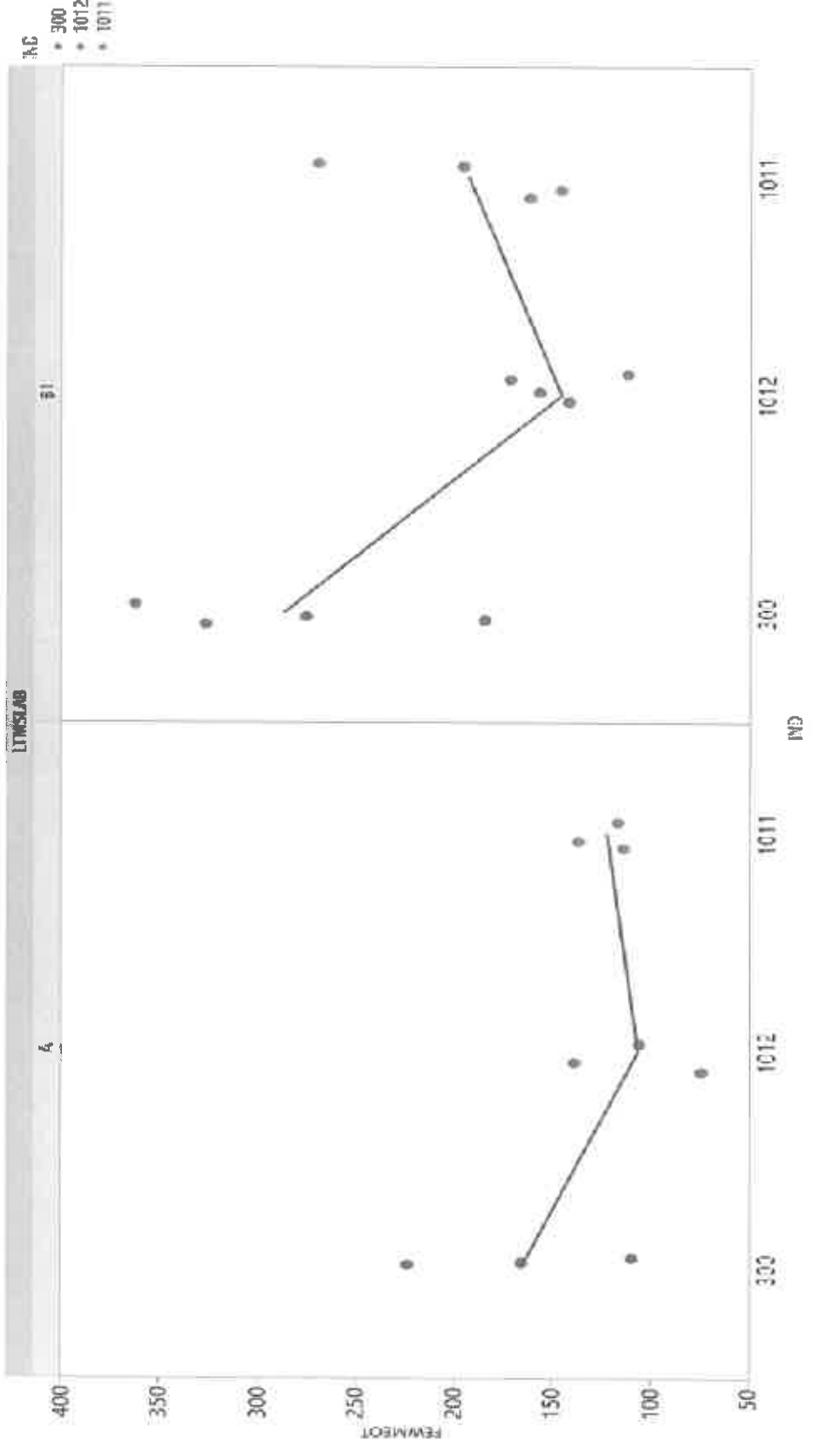
Fe-Wear Metals at EOT by Lab

- It appears that oil discrimination is not consistent among the stands; Stands rank oils differently



Fe-Wear Metals at EOT by Stand

- Below plot summarizes the FEWM EOT test result data by test Lab and reference oil



Ln(FEWMEOT) ANOVA Full Model

Statistically significant differences:

- Oil
- Lab

Not significantly different:

- Stands within Labs

Summary of Fit

| | |
|----------------------------|----------|
| RSquare | 0.772531 |
| RSquare Adj | 0.675045 |
| Root Mean Square Error | 0.230183 |
| Mean of Response | 5.084252 |
| Observations (or Sum Wgts) | 21 |

Analysis of Variance

| Source | DF | Squares | Mean Square | F Ratio |
|----------|----|-----------|-------------|----------|
| Model | 6 | 2.5192333 | 0.419872 | 7.9245 |
| Error | 14 | 0.7417780 | 0.052984 | Prob > F |
| C. Total | 20 | 3.2610112 | | 0.0007* |

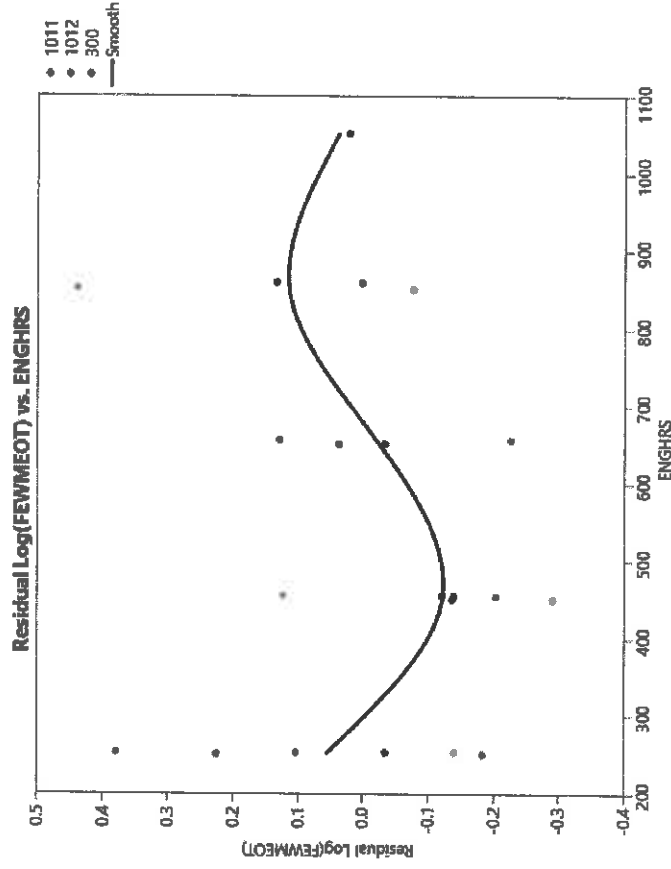
Parameter Estimates

| Term | Estimate | Std Error | t Ratio | Prob > t |
|-------------------------|------------|-----------|---------|-----------|
| Intercept | 5.0471138 | 0.05094 | 99.08 | <.0001* |
| IND[300] | 0.2623813 | 0.072759 | 3.61 | 0.0029* |
| IND[1012] | -0.232514 | 0.074003 | -3.14 | 0.0072* |
| LTMSLAB[A] | -0.2226712 | 0.05094 | -4.45 | 0.0005* |
| LTMSLAB[A];LTMSAPP[1] | 0.0997597 | 0.078981 | 1.26 | 0.2272 |
| LTMSLAB[B1];LTMSAPP[1] | -0.094059 | 0.095776 | -0.98 | 0.3427 |
| LTMSLAB[B1];LTMSAPP[2] | 0.2217766 | 0.095716 | 2.32 | 0.0362* |

Effect Tests

| Source | Nparm | DF | Sum of Squares | F Ratio | Prob > F |
|------------------|-------|----|----------------|---------|----------|
| IND | 2 | 2 | 0.8113142 | 7.6562 | 0.0057* |
| LTMSLAB | 1 | 1 | 1.0494905 | 19.8076 | 0.0005* |
| LTMSAPP[LTMSLAB] | 3 | 3 | 0.3660636 | 2.3030 | 0.1216 |

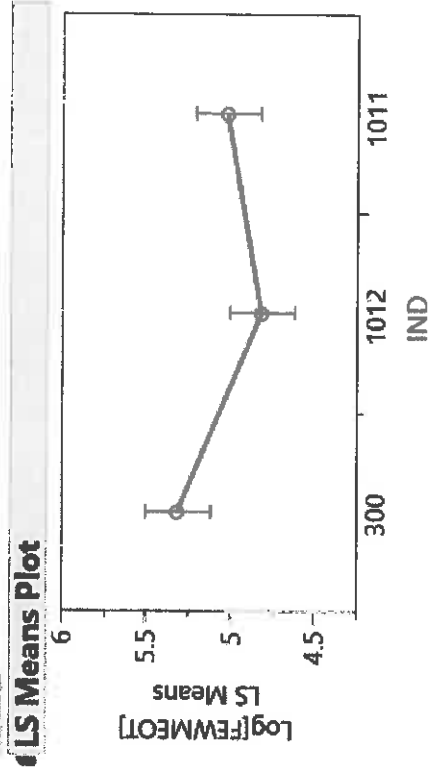
Engine Hours Adjustment



- The residuals of $\text{Ln}(\text{FEWMEOT})$ visually do not appear to be uniformly distributed on Engine Hours. (Engine Runs 2 and 3 appear to correlate with lower Fe than Runs 1 and 4)
- Engine Hours was added to the regression model in the following formats along with the result:
 - Engine Hours – Engine Hours not statistically significant and Oil statistically significant.
 - Engine Run (Categorical) - Engine Run not statistically significant and Oil statistically significant.
 - Engine Run 1 and Others (Categorical) – Engine Run not statistically significant and Oil statistically significant.
 - Engine Run 1, 4 & 5 and 2 & 3 (Categorical) – Engine Run borderline statistically significant and Oil statistically significant.
- For this dataset, Engine Hours/Run explains minimal additional variation. These terms should be re-evaluated after collecting additional data.

Ln(FEWMEOT) Oil Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Oils significantly differ
 - Oil 300 is significantly different than oil 1012
 - Oil 1011 is not statistically significantly different than oils 300 and 1012
- Plot shows $\text{Ln}(\text{FEWMEOT})$ LSMeans by Oil, with 95% confidence intervals



LSMeans by Oil

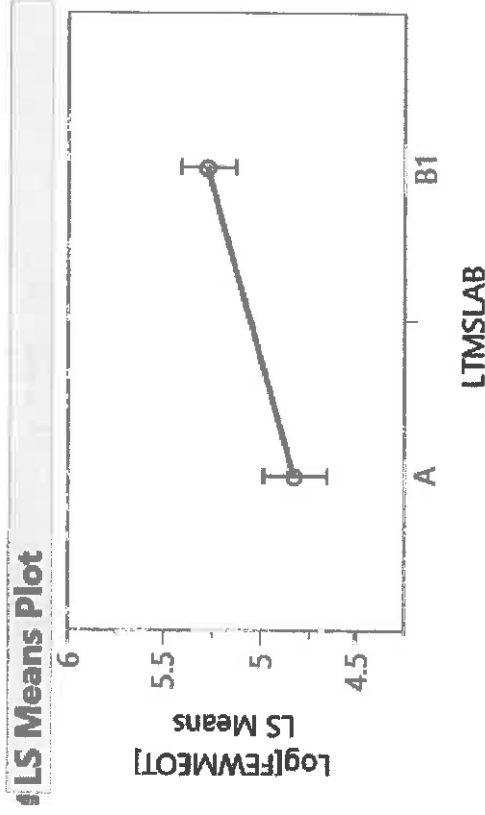
| Oil | Ln(FEWMEOT) LS Mean | FEWMEOT LS Mean |
|------|---------------------|-----------------|
| 300 | 5.3095 | 202 |
| 1012 | 4.8146 | 123 |
| 1011 | 5.0172 | 151 |

LSMeans Differences Between Oils

| Oil1 | Oil2 | Ln(FEWMEOT) LS Mean Difference | p-Value |
|------|------|--------------------------------|---------|
| 300 | 1012 | 0.4949 | 0.00 |
| 300 | 1011 | 0.2922 | 0.08 |
| 1011 | 1012 | 0.2026 | 0.28 |

Ln(FEWMEOT) Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand}(\text{Lab})$
- Plot below of $\text{Ln}(\text{FEWMEOT})$ LSMeans by Lab, with 95% confidence intervals
- Lab A is statistically significantly different than Lab B1.



LSMeans by Lab

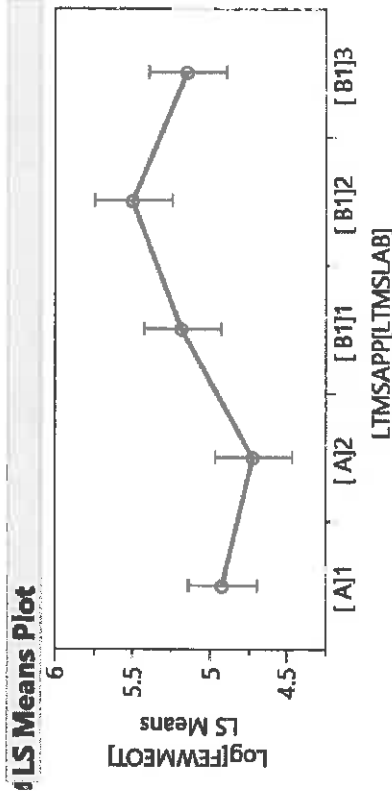
| Lab | Ln(FEWMEOT) LS Mean | FEWMEOT LS Mean |
|-----|---------------------|-----------------|
| A | 4.8204 | 124 |
| B1 | 5.2738 | 195 |

LSMeans Differences Between Labs

| Lab1 | Lab2 | Ln(FEWMEOT) LS Mean Difference | p-Value |
|------|------|--------------------------------|---------|
| B1 | A | 0.4534 | 0.00 |

Ln(FEWMEOT) Stand within Lab Differences

- Model is $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand(Lab)}$
- Plot below of $\text{Ln}(\text{FEWMEOT})$ LSMeans by Stand, with 95% confidence intervals
- Stands within labs are not statistically significantly different from each other



LSMeans by Stand

| Stand | Ln(FEWMEOT) LS Mean | FEWMEOT LS Mean |
|-------|---------------------|-----------------|
| [A]1 | 4.9202 | 137 |
| [A]2 | 4.7206 | 112 |
| [B]1 | 5.1798 | 178 |
| [B]2 | 5.4956 | 244 |
| [B]3 | 5.1461 | 172 |

LSMeans Differences Between Labs

| Stand1 | Stand2 | Ln(FEWMEOT) LS Mean Difference | p-Value |
|--------|--------|--------------------------------|---------|
| [B]2 | [B]3 | 0.3495 | 0.27 |
| [B]2 | [B]1 | 0.3158 | 0.36 |
| [A]1 | [A]2 | 0.1995 | 0.72 |
| [B]1 | [B]3 | 0.0337 | 1 |

Ln(FEWMEOT) Precision

Repeatability Model: $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand(Lab)}$
Reproducibility Model: $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil}$

Model RMSE

- $S_r = 0.2302$

Repeatability

- $S_r = 0.2302$
- $r = 0.6381$

Reproducibility

- $S_R = 0.3427$
- $R = 0.9499$

Based upon the FEWMEOT pooled standard deviation (S_r) and ASTM's repeatability (r), there is no significant difference between an FEWMEOT result¹ of 200 and 379.

Note 1: An FEWMEOT result of 200 was arbitrarily selected for comparison

Reference Oil Targets

Model: $\text{Ln}(\text{FEWMEOT}) \sim \text{Oil, Lab, Stand(Lab)}$

Iron at EOT (FEWMEOT)

Unit of Measure: $\text{Ln}(\text{FEWMEOT})$

| Ref. Oil | Target Mean $\text{Ln}(\text{FEWMEOT})$ | Target Mean FEWMEOT | St. Dev |
|----------|--|------------------------|---------|
| 300 | 5.3095 | 202 | 0.4204 |
| 1012 | 4.8146 | 123 | 0.2859 |
| 1011 | 5.0172 | 151 | 0.3064 |

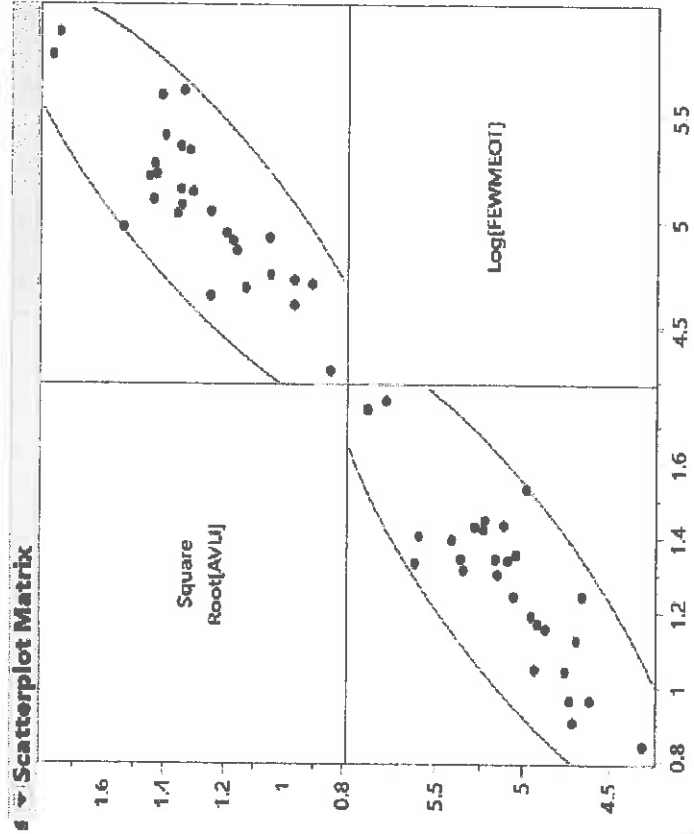
Target Means are the Oil LSMeans from the Model and Standard Deviations are calculated straight from $\text{Ln}(\text{FEWMEOT})$.

Correlation

Appendix K Section A.3 Parameter Redundancy: Correlation between $\sqrt{\text{AVLI}}$ and $\ln(\text{FEWMEOT})$ is statistically significant. These two parameters are closely related in repeat tests within oils.

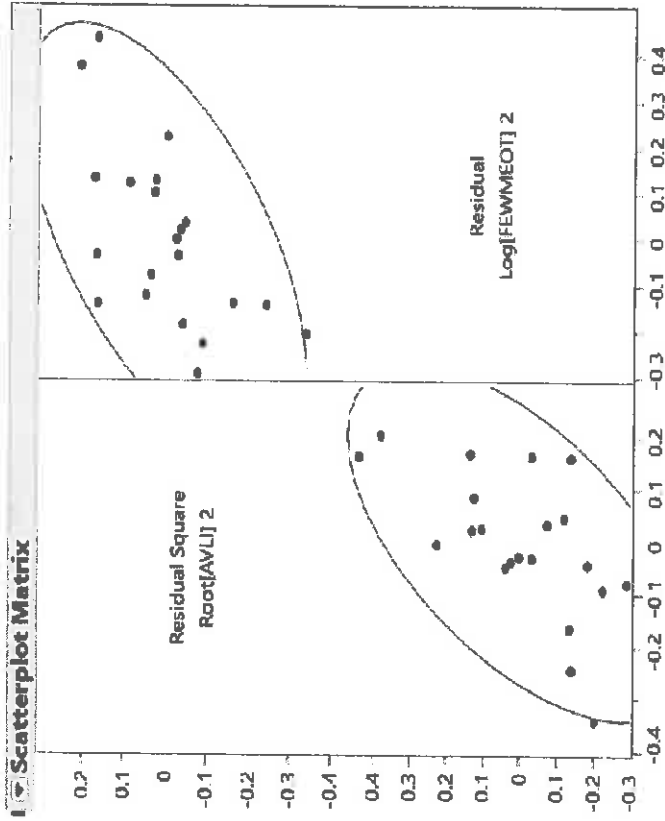
Correlations

| | | |
|-------------------|-------------------|--------------|
| Square Root[AVLI] | Square Root[AVLI] | Log[FEWMEOT] |
| 1.0000 | 0.8502 | 1.0000 |
| Log[FEWMEOT] | 0.8502 | 1.0000 |



Correlations

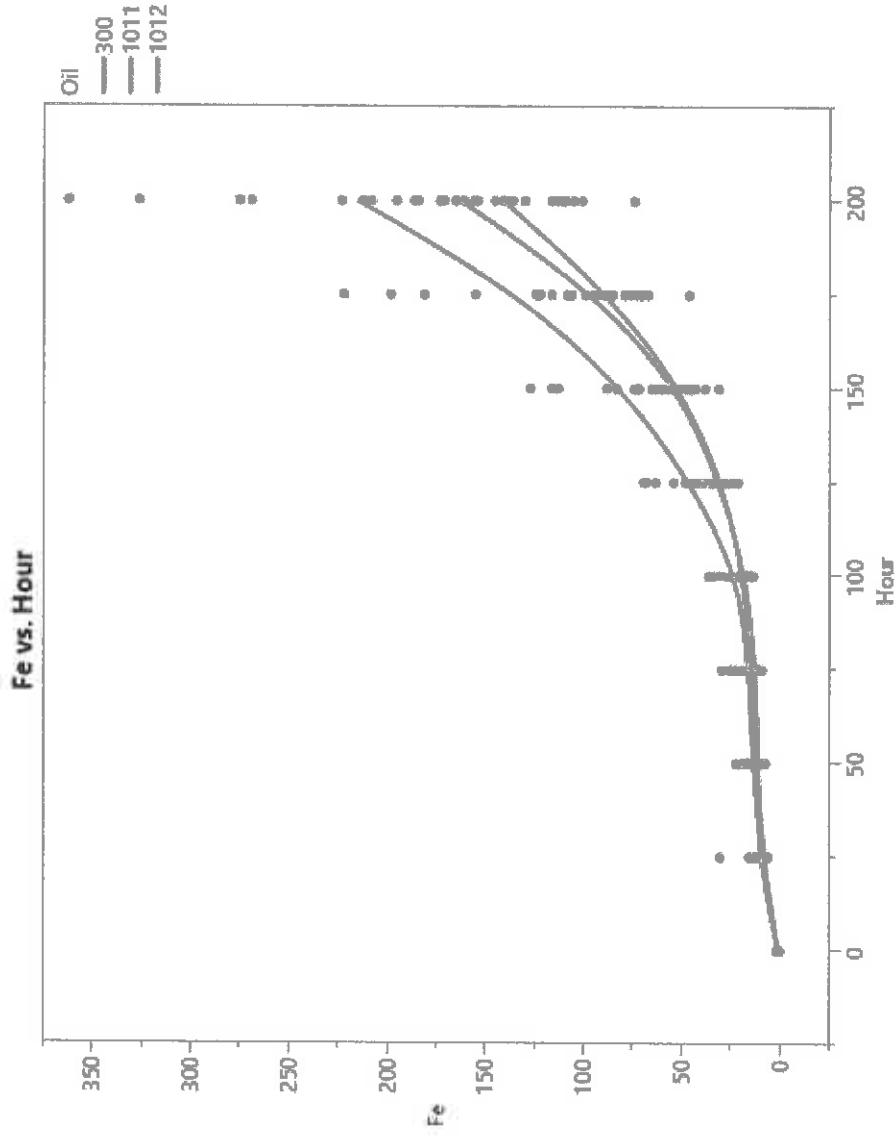
| | | |
|------------------------------|------------------------------|-------------------------|
| Residual Square Root[AVLI] 2 | Residual Square Root[AVLI] 2 | Residual Log[FEWMEOT] 2 |
| 1.0000 | 0.6108 | 1.0000 |
| Residual Log[FEWMEOT] 2 | 0.6108 | 1.0000 |



Appendix B: FEWML50 (n=28)

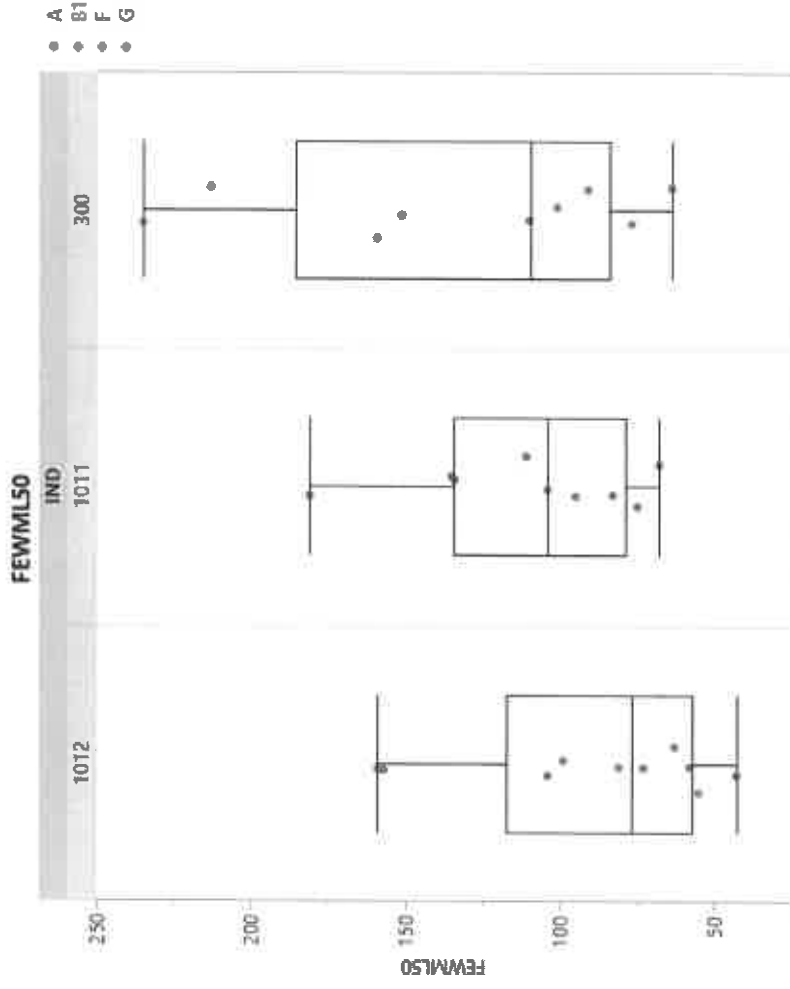
Change in Fe-Wear Metals over last 50 hours

Fe Content Profile



- The slope during the last 50 hours is highest for RO 300 and lowest for RO 1012.

FEWML50



- There is considerable FEWML50 overlap for the oils.

FEWML50 Regression Analysis

- $\ln(\text{FEWML50})$ is regressed

on:

- Lab
- Stand[Lab]
- Oil

- Oil discrimination of FEWML50 (p-Value = 0.1507) is worse than FEWMEOT (p-Value = 0.0559).

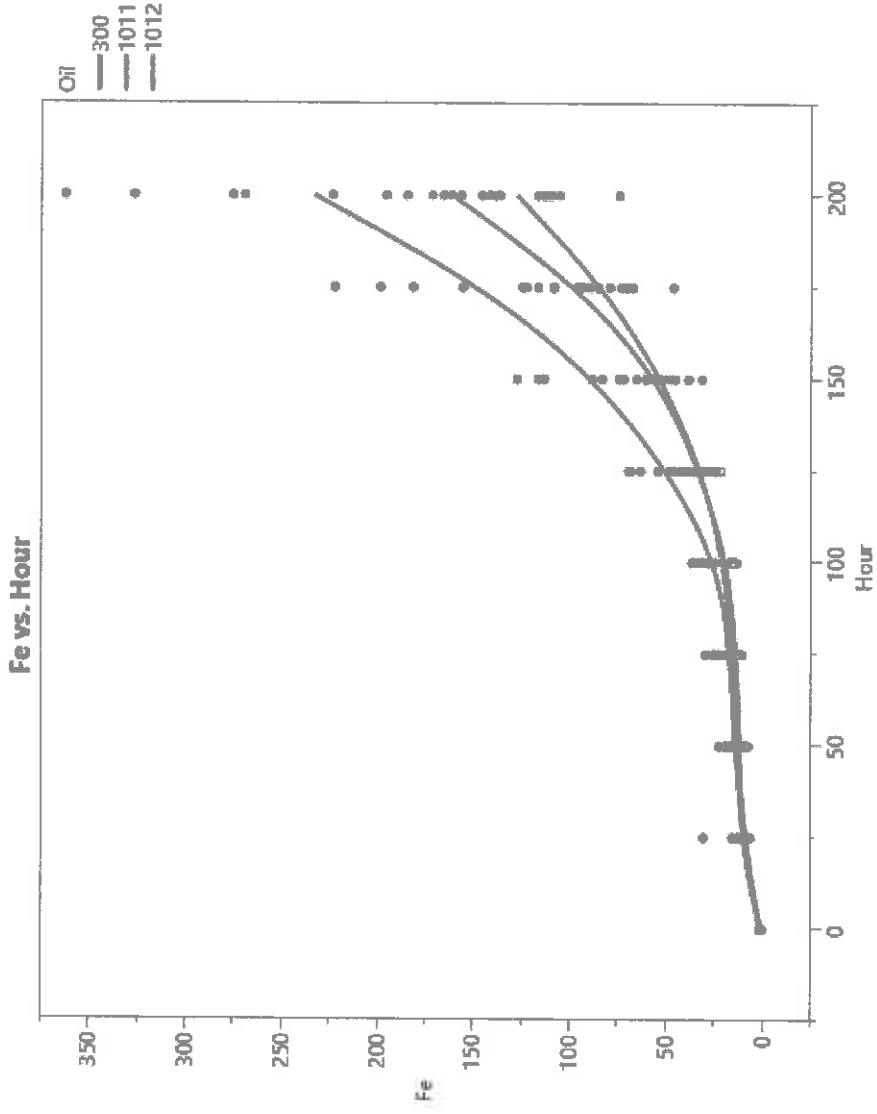
| Effect | DF | p-Value |
|------------|----|---------|
| Lab | 3 | 0.0165 |
| Stand[Lab] | 3 | 0.3006 |
| Oil | 2 | 0.1507 |

Appendix C:

FEWML50 (n=21)

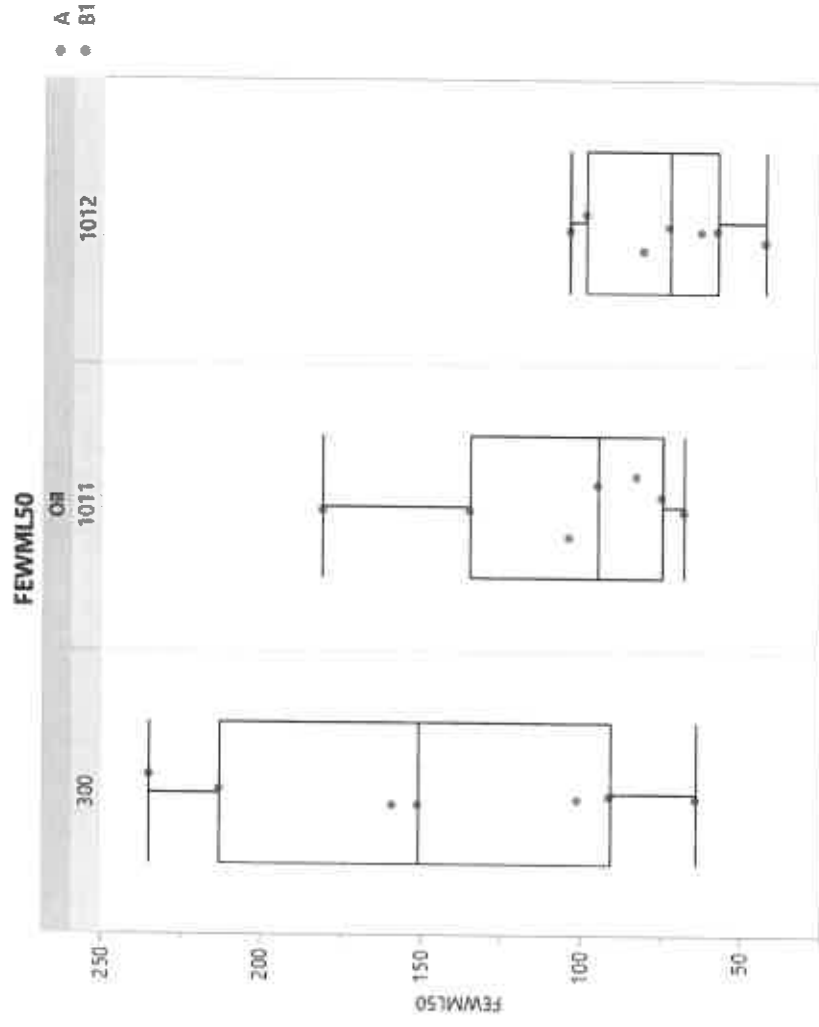
Change in Fe-Wear Metals over last 50 hours

Fe Content Profile



- As with $n = 28$, the slopes appear to differ by Oil.

FEWML50 by Oil



- The Oils overlap.

FEWML50 Regression Analysis

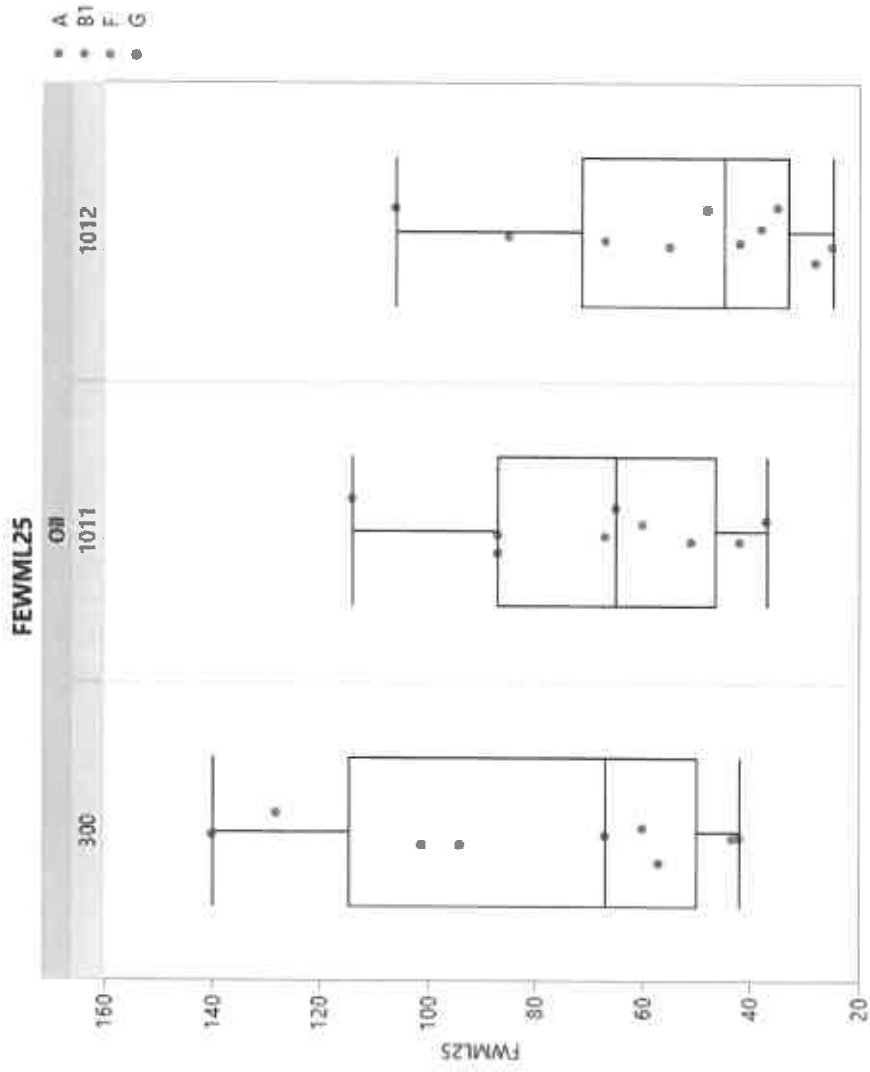
- $\ln(\text{FEWML50})$ is regressed on:
 - Lab
 - Stand[Lab]
 - Oil
- Oil discrimination of FEWML50 (p-Value = 0.0101) is slightly worse than FEWMEOT (p-Value = 0.0057).

| Effect | DF | p-Value |
|------------|----|---------|
| Lab | 1 | 0.001 |
| Stand[Lab] | 3 | 0.2493 |
| Oil | 2 | 0.0101 |

Appendix D: FEWML25 (n=28)

Change in Fe-Wear Metals over last 25 hours

FEWML25 by Oil



- The Oils overlap.

FEWML25 Regression Analysis

- $\ln(\text{FEWML25})$ is regressed on:
 - Lab
 - Stand[Lab]
 - Oil
- Oil discrimination of FEWML25 (p-Value = 0.1430) is worse than FEWMEOT (p-Value = 0.0559).

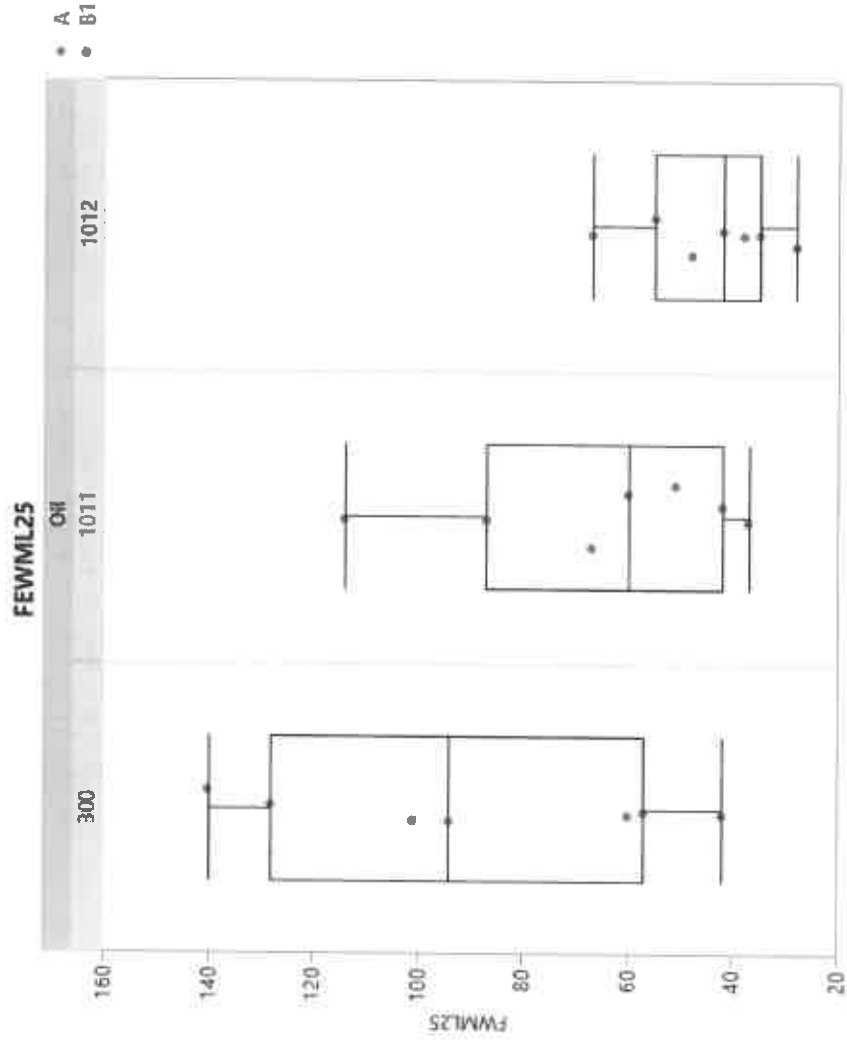
| Effect | DF | p-Value |
|------------|----|---------|
| Lab | 3 | 0.0189 |
| Stand[Lab] | 3 | 0.4659 |
| Oil | 2 | 0.1430 |

Appendix E:

FEWML25 (n=21)

Change in Fe- Wear Metals over last 25 hours

FEWML25 by Oil



- The Oils overlap.

FEWML25 Regression Analysis

- $\ln(\text{FEWML25})$ is regressed on:
 - Lab
 - Stand[Lab]
 - Oil
- Oil discrimination of FEWML25 (p-Value = 0.0098) is slightly worse than FEWMEOT (p-Value = 0.0057).

| Effect | DF | p-Value |
|------------|----|---------|
| Lab | 1 | 0.0015 |
| Stand[Lab] | 3 | 0.4006 |
| Oil | 2 | 0.0098 |