IIIH Task Force Conference Call October 1, 2015 1:00PM Central Call-in 713-222-0377 Pass Code 5214824464

#### Attendees:

Chrysler: Haiying Tang Shell: Karin Haumann Oronite: Jo Martinez, Robert Stockwell, Kaustav, Sinha Afton: Ed Altman Ashland: Amol Savant Infineum: Andy Ritchie, Gordon Farnsworth, Mike McMillan Lubrizol: George Szappanos, Michael Conrad, Kevin OMalley Intertek: Adison Schweitzer SwRI: Pat Lang, Ankit Chaudhry, Travis Kostan, Sid Clark TMC: Rich Grundza OHT: Jason Bowden, Matt Bowden IMTS: Dave Passmore Ford: Ron Romano Idemitsu: Scott Rajala GM: Bruce Matthews

Karin opened the meeting announcing we had a hard stop at 3:00 Eastern / 2:00 Central

The Agenda is attached as (Attachment #1)

The first order of business was review of the E-Ballot concerning changes to the IIIH Engine Assembly Manual and Forms changes posted to the TMC Website. As there were no discerning comments, the E-Ballot is considered Approved and the information will be posted to the TMC Website.

The second order of business, Karin informed the group that since they last spoke, the core lab group had conducted a IIIH Data Review, of which she included as a smaller sub set for review during the call showing some of the parameters of interest from the larger data set in her presentation materials for this call identified as (Attachment #2 "IIIH Data Review"). Karin also informed the group they can review the complete, Full Data Set of this review on the TMC Website.

Karin reviewed the IIIH Data Review and appropriate lab personnel commented for each section of the review. Karin indicated that slides 7 & 8 should be disregarded as these variations were approved during the test review.

The labs agreed they were all working on Fuel Temperature Control and discussed the reasons for setting the temperature at 30°C. Discussion focused on fuel temperature settings during development and prove-out testing with the focus on not wanting to change the specifications from the prove-out data. The group discussed each parameter in detail with Rich Grundza agreeing the Test Monitoring

Center will review all limits looking at Prove-Out and Precision Matrix Data and base limits around the data after everything has been reviewed. After discussion the following Motion was made: Ed Altman / Addison Schweitzer Accept the as valid the tests reviewed in the current operational data review. The Test Keys accepted as valid are:

106768, 106755, 106786, 106793, 106795, 106792, 107872, 110227

Karin then called the question; Zero Objections Zero Waves Motion Passed Unanimously

Karin next reviewed the IIIH Reference Oils (Attachment #3 "IIIH Reference Oils") The group reviewed the Reference Oil Data understanding some of the data had yet to be reported to the TMC but was included in the presentation with exception the final run from Lab E.

The next order of business, Jo Martinez presented a statistical analysis review of the current available data (Attachment #4 IIIH Precision Matrix Data Analysis 092915).

After Jo Martinez's review of the data, Karin reminded everyone that the data discussed was based on four tests/stand from each lab with exception Lab "E" which was re-running their first test and setting up to run their final tests after making changes to correct problems found during the initial core group parameter review.

Karin asked Lab E to forward their presentation to the group for review (Attachment #5 "ASH  $1^{st}$  2 PM Tests validity discussion) and the group reviewed his presentation. Karin reminded the group that Ashland's  $1^{st}$  test was in-validated and the  $2^{nd}$  test was pending the core group's upcoming review.

Karin then tabled this conversation pending the outcome of that review.

Karin then indicated the complete data set will be forwarded to the full statistical review group once the data set was complete. Additionally, Karin reminded the group earlier in the call that the Precision Matrix was designed allowing Lab E to be excluded from the initial review thereby allowing acceptance and inclusion of their data to be included in the first 20 Reference Test Updated Limits.

The meeting adjourned at 3:00pm Eastern / 2:00pm Central.

This is a compilation from notes recorded during the call, with comments from member participants during the Draft Review. Certain subjects may not necessarily be in exact order; however, they are believed to represent an accurate account of the call. If anyone feels changes or additional content may be necessary, please contact Sid Clark @ 586-873-1255 or Sidney.Clark@swri.org

Thanks, Sid

#### Sequence IIIH Task Force October 1, 2015 1:00 pm CDT Call-in Number: 713-222-0377 Conference Number: 5214824464

#### Old Business:

E-ballot to approve proposed Engine Assembly Manual Changes and TMC Form Changes

#### **Matrix Test Validity**

IIIH Data Review 3 – Karin Haumann

#### **Matrix Data Collected**

Reference Oils – Karin Haumann IIIH Precision Matrix Data Analysis - Jo Martinez

#### **Matrix Status**

Status of outstanding tests – Amol Savant

#### Next Meeting

TBD

Attachment #2

## IIIH Precision Matrix Third Operational Data Review

1

Findings of anomalies in the data October 1, 2015

### Scatterplot of Coolant In Temp\_Deg C vs Test Time



2

### Scatterplot of Oil Gallery Temp vs Test Time



Panel variable: Testkey

### Scatterplot of Right Exhaust Temp\_Deg C vs Test Time



Panel variable: Testkey

### Scatterplot of Right AFR vs Test Time



Panel variable: Testkey

### Scatterplot of Left Nox vs Test Time



Panel variable: Testkey

6

#### Scatterplot of Fuel Rail Pressure vs Test Time



7

#### Scatterplot of Fuel Flow\_Kg/H vs Test Time





# **Test Monitoring Center**

http://astmtmc.cmu.edu

# QI Plots from 3rd Matrix Tests

# Summary of Controlled Parameters

- Most issues from previous tests have been resolved.
- Intake air pressure and fuel temperature continue to be slightly challenging.





# **Coolant Flow**

09:55 Thursday, September 3, 2015 1

Process



IIIH QUALITY INDEX OPERATIONAL REVIEW Engine Coolant Flow - L/min (CONTROL) LAB= G Stand= 2 CMIR= 110227

# **Fuel Temperature**



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Fuel Inlet Temperature — Degrees C (CONTROL) LAB= B Stand= 341 CMIR= 106795



Test Time – Hours

#### IIIH QUALITY INDEX OPERATIONAL REVIEW Fuel Inlet Temperature – Degrees C (CONTROL) LAB= G Stand= 1 CMIR= 110228



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Fuel Inlet Temperature – Degrees C (CONTROL) LAB= A Stand= 2 CMIR= 106775



# Intake Air Pressure



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Intake Air Pressure – kPa (CONTROL) LAB= G Stand= 1 CMIR= 106768



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Intake Air Pressure – kPa (CONTROL) LAB= G Stand= 2 CMIR= 110227



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Intake Air Pressure – kPa (CONTROL) LAB= G Stand= 1 CMIR= 110228



#### IIIH QUALITY INDEX OPERATIONAL REVIEW Intake Air Pressure – kPa (CONTROL) LAB= G Stand= 2 CMIR= 107872



# Conclusion

### Some minor anomalies were observed

- The root causes have been identified
- It is believed that the effect on the overall tests and the test results is negligible
- The data review group recommends that the Task Force accept these tests as operationally valid.

Attachment #3

# **IIIH Reference Oils**











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# Objectives for Reference Oils FCA

### ✓ Include:

- $\checkmark$  Borderline oils to identify shifts in test severity over time
- An oil that performs poorly on WPD to maintain test discrimination (438-1)
- An oil that performs poorly on pVis to maintain test discrimination (434-2)
- $\checkmark$  An oil that performs well on both WPD and pVis (436)

### Expectations of Reference Oils FCA

- ✓ 434-2 would discriminate on pVis as a failing oil  $\sqrt{436}$  would perform well on both pVis and WDD
- ✓ 436 would perform well on both pVis and WPD
- $\checkmark$  438-1 would discriminate on WPD as a failing oil

Trade-Offs:

- Potentially high variability on pVis for 438-1
- Potentially high variability on WPD for 434-2





### **Prove-Out IIIG and Data**

	IIIG WPD	IIIG kV40 Increase, %	Field Test kV100	Field Test Hot Stuck Rings	IIIG/field Performance
GF-5 limits	4.0	150	NA	NA	
TMC 435	2.43~4.75	96~331	-	-	Borderline pVis and failing WPD
TMC 434*	2.9~6.7	52~244	-	-	Borderline pVis and WPD
TMC 438*	2.54~3.86	68~138	-	-	Failing WPD
REO2 (TMC 436)*	>4.5	~100	Stay in grade	None	Passing
REO3	>5	<100	Stay in grade	None	High passing

\*IIIH Reference Oils

Attachment #4



### **Sequence IIIH Precision Matrix Data Analysis**

Jo Martinez Sep. 29, 2015







### Summary

- LnPVIS
  - Precision: RMSE,s=0.58 (prove-out s=0.61)
  - Oil Discrimination: 434-2 > 436
  - Lab/Stand Difference: A1 > D1
  - Influential observation: TK106788 D1 434-2 PVIS=13.6
- WPD
  - Precision: RMSE,s=0.47 (prove-out s=0.40)
  - Oil Discrimination: 436, 434-2 > 438-1
  - No significant lab difference
  - Influential observation: TK107872 G2 438-1 WPD=4.5



## 25 out of 28 Tests Included in the Analysis

	IIIH Matrix Test Status										
	Lab-Stand	D-1	E-1	B-1	G-1	G-2	A-1	A-2			
	1	434-2 106788-IIIH	438-1 106784-IIIH Low MAP and Fuel Flow	438-1 106796-IIIH Oil Leak 438-1 106797-IIIH	436 106763-IIIH	436 106764-IIIH	438-1 106774-IIIH	434-2 106778-IIIH			
Run Order	2	434-2 106789-IIIH Loss of Oil Pressure 434-2 106789A-IIIH	436 106782-IIIH	436 106 <mark>792-IIIH</mark>	438-1 106767-IIIH	434-2 107873-IIIH	438-1 107869-IIIH	438-1 107870-IIIH			
	3	436	434-2	436	438-1	434-2	434-2	436			
		106786-IIIH	106781-IIIH	106793-IIIH	106768-IIIH	110227-IIIH	106779-IIIH	106775-IIIH			
	4	438-1	434-2	434-2	434-2	438-1	436	436			
		106791-IIIH		106795-IIIH	110228-IIIH	107872-IIIH	106777-IIIH	106776-IIIH			
Test	Test Reported Invalid										





IND	PVIS	TESTKEY	WPD	PHOS	LTMSDATE	LTMSTIME	LTMSLAB	LTMSAPP
438-1	265.1	106774-IIIH	3.3	4 79.22	2 20150725	5 08:34	А	1
434-2	137.5	106778-IIIH	3.9	8 78.47	7 20150727	7 07:45	А	2
436	26.9	106764-IIIH	3.9	9 95.62	2 20150731	L 14:43	G	2
436	19.5	106763-IIIH	4.4	5 94.73	3 20150731	l 16:10	G	1
434-2	13.6	106788-IIIH	4.7	3 79.83	3 20150801	L 03:27	D	1
438-1	24.6	106797-IIIH	3.3	2 73.6	5 20150815	5 14:45	В	1
438-1	31.2	106767-IIIH	3.3	3 81.3	3 20150816	5 08:58	G	1
434-2	166.6	107873-IIIH	4.1	) 79.94	4 20150816	5 11:29	G	2
438-1	209.0	107869-IIIH	3.1	Э.	20150816	5 13:50	А	1
438-1	31.3	107870-IIIH	3.4	2.	20150817	7 12:30	А	2
436	19.5	106782-IIIH	4.2	5.	20150818	3 05:23	E	1
436	22.4	106792-IIIH	4.7	7 93.64	4 20150825	5 16:14	В	1
434-2	59.4	106789A-IIIH	5.6	78.85	5 20150829	9 05:05	D	1
438-1	29.4	106768-IIIH	3.4	5 80.85	5 20150829	9 13:06	G	1
434-2	180.9	110227-IIIH	3.3	5 81.28	8 20150829	9 17:48	G	2
436	31.3	106793-IIIH	4.9	5.	20150830	) 18:02	В	1
434-2	129.6	110228-IIIH	4.2	8 81.22	2 20150904	1 14:44	G	1
436	38.0	106775-IIIH	4.6	2 91.52	1 20150905	5 16:40	А	2
438-1	130.9	107872-IIIH	4.5	) 79.4	4 20150905	5 19:04	G	2
434-2	99.8	106795-IIIH	3.9	3 81.34	4 20150905	5 20:30	В	1
436	27.8	106786-IIIH	4.7	2 95.3	3 20150906	5 09:54	D	1
434-2	104.9	106779-IIIH	3.6	5 78.39	9 20150912	2 15:15	А	1
438-1	25.4	106791-IIIH	3.5	9 79.22	2 20150915	5 05:06	D	1
436	54.6	106777-IIIH	4.3	3			А	1
436	22.7	106776-IIIH	4.9	2			А	2

### **PVIS Data**







### **LnPVIS ANOVA Results**



**ADDING UP** 

Summary of Fit						
RSquare	0.716471					
RSquare Adj	0.574707					
Root Mean Square Error	0.584535					
Mean of Response	3.936889					
Observations (or Sum Wgts)	25					

#### **Analysis of Variance**

		Sum of		
Source	DF	Squares	Mean Square	F Ratio
Model	8	13.814745	1.72684	5.0540
Error	16	5.466896	0.34168	Prob > F
C. Total	24	19.281641		0.0029*

#### Lack Of Fit

#### Parameter Estimates

Effect lests									
			Sum of						
Source	Nparm	DF	Squares	F Ratio	Prob > F				
IND	2	2	4.9202105	7.2000	0.0059*				
LTMSLAB	4	4	4.4657561	3.2675	0.0387*				
LTMSAPP[LTMSLAB]	2	2	3.1433534	4.5998	0.0264*				

**Conclusions:** 

- 434-2 > 436•
- A1 > D1 •
- RMSE, s = 0.58 (Prove-out s=0.61) ٠



Level	- Level	Difference	Std Err Dif	Lower CL	Upper CL	p-Value
434-2	436	1.145307	0.3018525	0.366427	1.924186	0.0043*
438-1	436	0.588356	0.3018525	-0.190524	1.367235	0.1574
434-2	438-1	0.556951	0.3018525	-0.221928	1.335830	0.1870



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Levels not connected by same letter are significantly different.

# LnPVIS ANOVA Results - without TK106788

Summary	of Fit								C
RSquare			0.791041						
RSquare Adj			0.679597						•
Root Mean S	quare E	rror	0.49301						
Mean of Res	ponse		3.992173						•
Observations	s (or Sur	n Wgts)	24						•
Analysis o	of Vari	ance							
		Sum of	•			í .			
Source	DF	Squares	Mean S	quare	F Ratio				Ę
Model	8 1	13.801964	1	.72525	7.0981				
Error	15	3.645877	′ 0	.24306	Prob > F				_
C. Total	23 1	17.447841			0.0006*				
Lack Of Fi	t								
Paramete	r Estin	nates						L	.evel
Effect Tes	ts							4	134-2
				Sum	of			4	134-2
Source		Nparm	DF	Squar	es FRa	tio Pro	ob > F	4	1-001
IND		2	2 (	5.08140	73 12.51	102 0.	.0006*		5.5 -
LTMSLAB		4	4 2	2.39640	33 2.46	548 0.	0899	[S SI	4.5-
LTMSAPP[LT	MSLAB]	2	2 3	3.01446	34 6.20	011 <mark>0</mark> .	.0109*	g[PVI] Mear	4 -
								lo jo	3.5 -

Conclusions:

- 434-2 > 436, 438-1
- A1 > D1, G1
- RMSE, s = 0.49 (Prove-out s=0.61)

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**ADDING UP** 



Level	- Level	Difference	Std Err Dif	Lower CL	Upper CL	p-Value
434-2	436	1.306597	0.2613194	0.627827	1.985366	0.0004*
434-2	438-1	0.718241	0.2613194	0.039472	1.397011	0.0375*
438-1	436	0.588356	0.2545891	-0.072932	1.249643	0.0850
5.5 - 5 -	Į.		т	⊺ Le	vel	Least Sq Mean



Levels not connected by same letter are significantly different.







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### **WPD ANOVA Results**



Summary of Fit	
RSquare	0.618544
RSquare Adj	0.491392
Root Mean Square Error	0.466324
Mean of Response	4.1068
Observations (or Sum Wgts)	25

#### **Analysis of Variance**

		Sum of		
Source	DF	Squares	Mean Square	F Ratio
Model	6	6.347095	1.05785	4.8646
Error	18	3.914249	0.21746	Prob > F
C. Total	24	10.261344		0.0041*

#### Lack Of Fit

#### **Parameter Estimates**

#### Effect Tests

			Sum of		
Source	Nparm	DF	Squares	F Ratio	Prob > F
IND	2	2	4.4963511	10.3384	0.0010*
LTMSLAB	4	4	1.6040886	1.8441	0.1644

Conclusions:

- 436, 434-2 > 438-1
- No significant lab differences
- RMSE, s=0.47 (Prove-out, s = 0.40)



Levels not connected by same letter are significantly different.

## WPD ANOVA Results – without TK107872

Summary of Fit							
RSquare	0.817564						
RSquare Adj	0.720265						
Root Mean Square Error	0.35049						
Mean of Response	4.090417						
Observations (or Sum Wgts)	24						

#### Analysis of Variance

		Sum of		
Source	DF	Squares	Mean Square	F Ratio
Model	8	8.257643	1.03221	8.4026
Error	15	1.842653	0.12284	Prob > F
C. Total	23	10.100296		0.0002*

#### Lack Of Fit

#### Parameter Estimates

#### Effect Tests

			Sum of		
Source	Nparm	DF	Squares	F Ratio	Prob > F
IND	2	2	5.3858135	21.9214	<.0001*
LTMSLAB	4	4	1.9550917	3.9788	0.0214*
LTMSAPP[LTMSLAB]	2	2	0.6616185	2.6929	0.1002

Conclusions:

- 436, 434-2 > 438-1 •
- D1 > G2•

3.5

3

[A]1

[A]2

RMSE, s=0.35 (Prove-out, s = 0.40) •



Levels not connected by same letter are significantly different. 10

[D]1

LTMSAPP[LTMSLAB]

[E]1

[G]1

[G]2

[B]1

**ADDING UP** 

4.0994956

4.0561798

3.7761798

3.7079825

3.5241930

[ A]2

[G]1

[ A]1

[E]1

[G]2

ΑB

A B

ΑB

AΒ

B





### **PVIS Prove-out and PM Data**





### **PVIS Severity**



Prove-out (po): REO2, REO3, 438-1 < 434-1 Precision Matrix (pm): 436 < 434-2

No significant REO2/436 nor 438-1 severity shift between proveout and PM but marginal severity shift between 434-1 and 434-2



		Least				
Level		Sq Mean				
po434-1	А	5.5988583				
pm434-2	AB	4.5761904				
poREO2	BC	4.0103060				
pm438-1	BC	3.9498256				
po438-1	ВC	3.8860871				
pm436	C	3.2518872				
poREO3	BC	2.9848301				
Levels not	connected	l by same lette	er are signific	antly differe	nt.	
Level	- Level	Difference	Std Err Dif	Lower CL	Upper CL	p-Value
po434-1	poREO3	2.614028	0.5471598	0.91613	4.311930	0.0004*
po434-1	pm436	2.346971	0.3403868	1.29071	3.403232	<.0001*
po434-1	po438-1	1.712771	0.4327015	0.37005	3.055495	0.0052*
po434-1	pm438-1	1.649033	0.3441448	0.58111	2.716955	0.0004*
pm434-2	poREO3	1.591360	0.5499462	-0.11519	3.297909	0.0816
po434-1	poREO2	1.588552	0.3223861	0.58815	2.588955	0.0003*
pm434-2	pm436	1.324303	0.3333462	0.28989	2.358716	0.0050*
poREO2	poREO3	1.025476	0.5284110	-0.61425	2.665198	0.4668
p0434-1	pm434-2	1.022668	0.3574431	-0.08652	2.131856	0.0878
pm438-1	poREO3	0.964995	0.5407983	-0.71317	2.643157	0.5658
po438-1	poREO3	0.901257	0.6002278	-0.96132	2.763835	0.7422
poREO2	pm436	0.758419	0.2984470	-0.16770	1.684535	0.1723
pm438-1	pm436	0.697938	0.3192720	-0.29280	1.688677	0.3255
pm434-2	po438-1	0.690103	0.4162461	-0.60156	1.981764	0.6468
po438-1	pm436	0.634200	0.4120133	-0.64433	1.912726	0.7200
pm434-2	pm438-1	0.626365	0.3311919	-0.40136	1.654093	0.4976
pm434-2	poREO2	0.565884	0.3135160	-0.40699	1.538762	0.5526
pm436	poREO3	0.267057	0.5348261	-1.39257	1.926686	0.9987
poREO2	po438-1	0.124219	0.3970883	-1.10799	1.356431	0.9999
pm438-1	po438-1	0.063738	0.4097027	-1.20762	1.335095	1.0000
poREO2	pm438-1	0.060480	0.2988093	-0.86676	0.987721	1.0000





### PVIS 434-1 and 434-2 Data







### **WPD Prove-Out and PM Data**





### **WPD Severity**



### Prove-out (po): REO2, 434-1, 438-1 < REO3; 438-1 < REO2 Precision Matrix (pm): 438-1 < 436, 434-2

No significant oil severity shift between prove-out and PM



		Least				
Level		Sq Mean				
poREO3	Α	7.1299306				
pm436	В	4.5498729				
poREO2	В	4.5415829				
po434-1	ΒC	4.2128373				
pm434-2	ВC	4.1117757				
po438-1	C	3.5598085				
pm438-1	C	3.5264432				
Levels not	connected	l by same lette	er are signific	antly differe	nt.	
Level	- Level	Difference	Std Err Dif	Lower CL	Upper CL	p-Value
poREO3	pm438-1	3.603487	0.3622891	2.47926	4.727713	<.0001*
poREO3	po438-1	3.570122	0.4021017	2.32235	4.817892	<.0001*
poREO3	pm434-2	3.018155	0.3684174	1.87491	4.161398	<.0001*
poREO3	po434-1	2.917093	0.3665507	1.77964	4.054544	<.0001*
poREO3	poREO2	2.588348	0.3539906	1.48987	3.686823	<.0001*
poREO3	pm436	2.580058	0.3582882	1.46825	3.691868	<.0001*
pm436	pm438-1	1.023430	0.2138852	0.35972	1.687141	0.0004*
poREO2	pm438-1	1.015140	0.2001769	0.39397	1.636312	0.0002*
pm436	po438-1	0.990064	0.2760140	0.13356	1.846569	0.0145*
poREO2	po438-1	0.981774	0.2660155	0.15630	1.807252	0.0109*
po434-1	pm438-1	0.686394	0.2305479	-0.02902	1.401811	0.0674
po434-1	po438-1	0.653029	0.2898734	-0.24648	1.552540	0.2917
pm434-2	pm438-1	0.585332	0.2218705	-0.10316	1.273823	0.1418
pm434-2	po438-1	0.551967	0.2788496	-0.31334	1.417271	0.4430
pm436	pm434-2	0.438097	0.2233137	-0.25487	1.131066	0.4537
poREO2	pm434-2	0.429807	0.2100292	-0.22194	1.081553	0.4030
pm436	po434-1	0.337036	0.2280303	-0.37057	1.044641	0.7558
poREO2	po434-1	0.328746	0.2159714	-0.34144	0.998930	0.7301
po434-1	pm434-2	0.101062	0.2394566	-0.64200	0.844124	0.9995
po438-1	pm438-1	0.033365	0.2744661	-0.81834	0.885066	1.0000
pm436	poREO2	0.008290	0.1999342	-0.61213	0.628710	1.0000









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### **PHOS ANOVA Results**



Summa	ary of Fi	it				Co	nclus	ions:				
RSquare RSquare Root Mea Mean of Observati	Adj an Square Response ions (or S	e Error e um Wgts	0.971241 0.962782 1.399788 84.05043	3		•	436 > Lab ( RMS	> 438-1, 3 > Lab E, s=1.4	434-2 A 40 (IIIGI	3 LTM	S, s =	= 2.33)
Analysi	is of Va	riance				1	00	•	<b>`</b>			,
Source	DF	Sum Squai	of res Mean	Square	F Ratio	leans	95-	Ŧ		Level		Least So Mean
Model	5	1124.91	.64 2	224.983 1	14.8221	LS N	90-			/36	٨	94 49361 2
Error	17	33.30	99	1.959 P	rob > F	ыног	80 T			430	~ <sub>D</sub>	70 922201
C. Total	22	1158.22	63		<.0001*		75 ¥		A.	434-2	B	79138865
Lack Of	f Fit						434-2	2 436 IND	438-1			
Parame	eter Esti	imates				Level 436	- Level	15 35475	0.7365072	13 4653	17 24	CL p-Value
Effect 1	Facte					436	434-2	14.66041	0.7391051	12.7643	16.55	648 <.0001*
Lifect	10313		Sum of			434-2	438-1	0.69434	0.7086543	-1.1236	2.51	229 0.5991
Source	Nparm	DF	Squares	F Ratio	Prob > F	100	D					Land
IND	2	2	1055.9958	269.4682	<.0001*	s 9	5-					Least
LTMSLAB	3 3	3	23.7308	4.0371	0.0245*	ear 90	0-			Lev	el	Sq Mean
						I S I S	- -	Ŧ	T	G	A	85.543132
						SOH O	_ I	I	1	B	ΑB	84.888737
						- 8				D	AB	84.463840

Levels not connected by same letter are significantly different.

LTMSLAB

В

D

75

Α

**ADDING UP**<sup>TM</sup>

83.058528

А

G

В









### **LnMRV ANOVA Results**



Summa RSquare RSquare Root Mea Mean of Observati	Adj an Square Response ions (or Si	Error um Wgts)	0.7558 0.6419 <mark>0.5037</mark> 10.358	73 48 45 88 23			Co • •	nclus 434- A1 > RMS	sions: 2 > 436 D1 SE, s=0.	, 438-1 50 (IIIG		S, s =	0.32)
Analysi	is of Va	riance						12					
		Sum of					_ 1	1.5 — т					Least
Source	DF	Squares	Mea	n Square	F Ratio		/FNL] ans	11-			Level	5	Sq Mean
Model	7	11.785459		1.68364	6.6348		2 Me	0.5 -	·	Т	434-2	A 1	L.072899
Error	15	3.806384		0.25376	Prob > F		L	10-		ĺ	438-1	B 10	0.010153
C. Total	22	15.591843			0.0011*			9 434	L I-2 436	438-1	436	B S	9.752532
Lack O	f Fit						Level	- Level	Difference	Std Err Dif	Lower CL	Upper C	L p-Value
Parame	eter Esti	mates					434-2	436	1.320367	0.2734815	0.610007	2.03072	7 0.0006*
Effect 1	<b>Fests</b>						438-1	436	0.257621	0.2807113	-0.471518	0.98676	0.6378
				Sum	of								
Source		Nparm	DF	Squar	res F Rat	tio Prob > F	11 5	_ T					Least
IND		2	2	7.06712	46 13.92	49 0.0004*	₹., 11		т		Lev	el	Sq Mean
LTMSLAB	5	3	3	3.07863	14 4.04	40 0.0272*	Successfully 10.5			Ī	[ A]	1 A	11.091127
LTMSAPP	[LTMSLA	B] 2	2	1.48353	37 2.92	31 0.0847	¥ د م او ۲	)-		I	[ G]	2 A B	10.637142
							۲ 9.5	;-	T	¥ 1	[ B]	1 A B	10.446716
							g		C 410	1	[ A]	2 A B	10.244187
								[A]1		[D]1 [G]1 '	[G]2 [G]	1 A B	10.208968
									LINGAPP[LI	NOLADJ	[ D]	1 B	9.576684

Levels not connected by same letter are significantly different.

# Anomalies in uncontrolled (non-Qi) parameters noted by TF Op-data review group

- Explanation, action / resolution

- Test Validity assessment

-by Amol Savant

- Ashland Inc. / Valvoline





# Issues noted in TF Op-data review

Regarding 2 Non-controlled parameters : MAP and Fuel Flow

Test 1 – (CMIR106784) Found to have significantly lower MAP and significantly lower values and arbitrary shift in Fuel Flow in comparison with other tests

Test 2 – (CMIR106782) Found to have lower MAP compared to other tests

Three different characteristics were observed in the nature of the MAP plot

1) Overall average being lower

2) MAP seemed to start at higher number and drop to lower within 1st 20mins for each restart of the engine

3) Additionally, for 1<sup>st</sup> test MAP seemed to start at slightly different values at each restart.

This MAP behavior seemed to directly influence characteristics seen in fuel flow plot for these tests.

**PM Test 1** (CMIR106784)

**PM Test 2** (CMIR106782)



## Investigation findings

- After the non-conformities noted by TF on the 1<sup>st</sup> test, investigation was done on the stand –
- It was found that dyno. torque calibration was off (by ~ 4.5 Nm) due to offset in calib. arm length (0.25"). This was corrected before start of the 2<sup>nd</sup> test. Also, as per George's suggestion the dyno. calib. was done after stand warmup. (We believe, it was due to this change, it can be observed from the 2<sup>nd</sup> test plot that the Fuel Flow was in line with the other tests, higher compared to our 1<sup>st</sup> test.)
- Additionally, during running the test 2<sup>nd</sup> test, -ve 1.5 kPa offset was noted in DAQ- MAP channel in comparison to CAN - MAP channel. The MAP data from 2<sup>nd</sup> test was later corrected to reflect this offset. (MAP plot of 2<sup>nd</sup> test on previous slide does not show these corrected values, shown ahead).
- After correcting MAP values, the overall average of MAP for the 2<sup>nd</sup> test came out to be 82.7kPa closer to where other tests ran.

Above 2 changes helped to resolve 1<sup>st</sup> non-conformity characteristic noted in MAP waveform (overall avg.) while the other 2 were resolved later as discussed ahead.

## Investigation findings

Average values for entire test								
Test No.	Testkey	Oil	MAP Orig. Reported	MAP after Offset Corr.	Fuel Flow (as Orig.)			
PM 1	106784	438-1	<b>79.5</b> (kPa)	81.0 (kPa)	23.7 (kg/h)			
PM 2	106782	436	<b>81.2</b> (kPa)	82.7 (kPa)	24.6 (kg/h)			

- Findings and subsequent corrections described in previous slide means the 1<sup>st</sup> test ran significantly lower on MAP as well as on Fuel Flow compared to other tests, and we concur with TF Op data review group's assessment of invalidating the 1<sup>st</sup> test (CMIR106784)
- However, in case of the 2<sup>nd</sup> test –
  Fuel flow numbers were in line / comparable to the other tests and with the corrected MAP numbers, the MAP was closer to other tests (corrected values plotted ahead)

### Plot of corrected MAP values

### in comparison with some other PM tests



Even though, these corrected MAP values were slightly lower than other tests,

We do not believe that had any significant impact on the test results, especially as fuel flow ran correctly. Also, atleast one other test showed such deviation in MAP compared to the bulk grouped values and was deemed operationally valid. (exhibit shown ahead)

### Exhibit:



## Resolution of initial drift, arbitrary offset in MAP

(2<sup>nd</sup> & 3<sup>rd</sup> non-conformity characteristics noted in MAP waveform)

- It was found by subsequent investigations of our stand that due to the combination of type of loadcell that was being used and proximity of it to uncooled exhaust downpipes, the loadcell was receiving a lot of heat conducted through loadarm creating temp. distribution across the strain gage and therefore was exhibiting thermal drift in o/p voltage changing the torque value resulting in lowering of MAP during initial hour after engine start.
- This was resolved by increasing loadcell control temp to 55°C to provide thermal equilibrium and changing to pancake-type loadcell

### Resolution of initial drift, arbitrary offset in MAP

20+hr run data after loadcell changes was provided to TF and was validated to successfully resolve the load/MAP start-up drift and arbitrary shift issue

(it is now, not needed to calib. dyno after warm-up as loadcell is always in thermal equilibrium)



# Conclusion

- In light of information / evidences presented here –
- We concur with TF assessment of the 1<sup>st</sup> PM test that it ran at significantly lower load / MAP and can be / has been invalidated.
- However, in case of the 2<sup>nd</sup> PM test, the fuel flow was in line with other tests and MAP was also closer to other tests. Therefore, we believe that the 2<sup>nd</sup> test (CMIR106782) ran similar to others and should be deemed as 'valid'.