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May 28, 2002

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# Unapproved Minutes of the May 16, 2002 Joint Sequence IIIF Surveillance Panel Meeting held in Detroit, Michigan

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The meeting was called to order at 8:30 am by Stand-In Chairman Daryl Baumgartner. A membership list was circulated for members & guests to sign in. It's shown in Attachment 1.

### Agenda Review

Ben Weber is Action & Motion recorder.

The Agenda was accepted as attached (Attachment 2).

### Membership Changes

Tim Caudill will replace Carl Stephens.

Jim Carter replaces Gil Clark.

Meeting Minute Status
March 5, 2002 Approved.

### Action Item Review from March 5, 2002 Meeting

Action #1: TMC and Bill Nahumck will make changes to the IIIFHD Report forms and Procedure. A new IIIFHD report packet was issued. This tasked was completed.

Action Item #2: O&H will investigate the oil and temp control system including the OHT3F-081-1 one-piece oil filter adapter fitting. Get sump temperature data from OHT 7 tests. O&H panel will be making a recommendation this meeting to improve the system. This task is completed.

Action Item #3: O&H Panel will continue deriving solutions to the variations in the Kundinger Fluid Control Racks. This task is on-going and will be addressed by the O& H panel over the next ASTM period.

### TMC Sequence IIIF Semi-Annual Report

See TMC ftp site for report : <a href="ftp://astmtmc.cmu.edu/docs/gas/sequenceiii/semiannualreports/">ftp://astmtmc.cmu.edu/docs/gas/sequenceiii/semiannualreports/</a>

Average delta/s results are as follows:

|           | Industry Severity Summary |                                                |                                       |  |  |
|-----------|---------------------------|------------------------------------------------|---------------------------------------|--|--|
| Parameter | Average Δ/s               | Pooled standard deviation (degrees of freedom) | Average $\Delta$ , in reported units  |  |  |
| PVIS      | 0.122                     | 0.024 (df=17)                                  | 24.9% Viscosity Increase <sup>1</sup> |  |  |
| APV       | 0.006                     | 0.229 (df=17)                                  | 0.001 merits                          |  |  |
| WPD       | -0.578                    | 0.637 (df=17)                                  | -0.37 merits                          |  |  |
| PV60      | 0.610                     | 0.198 (df=17)                                  | 37.9 % Viscosity Increase             |  |  |

<sup>&</sup>lt;sup>1</sup> At the GF-3 Pass Limit of 275% Viscosity Increase

In general Viscosity Increase Severity and Precision for most of the period were in control. There were no alarms this period.

Average Weighted Piston Deposit indicated several severe severity alarms around January however, has since returned to in control conditions. Investigations indicate that this severe trend coincided with the introduction of 1006-2. Initial targets on 1006-2 will need to be updated when 10 tests are received. Precision was in control during the entire period. The TMC analysis of piston deposit data reference data indicated that lab differences exists for Groove 3 ratings across all labs and oils. The TMC was tasked with reviewing recent rating workshop data to determine if rater differences could explain these differences. Aside from this observation the reference oil data did not show any evidence of problems. However, the TMC will continue to monitor the situation.

APV was in is control for both severity and precision this report period.

Two failing reference oil tests for the period failed due to severe SACLW performance. No explanation for the severe SACLW results has been found at this time. Investigations into Sequence IIIF wear performance are ongoing but to date no solutions to the problem have been found.

A review of Percent Viscosity Increase at 60 Hours shows that the industry has been consistently mild of target on this parameter since it's introduction into the test. The TMC suggested a review of the targets was in order. The Surveillance Panel did not take any action on this item. This parameter is not a pass-fail parameter for the Sequence IIIF test and is only used for the Sequence IIIFHD test.

Reference oil 1006 targets have been updated at 35 data points. Reference oil 433-1 targets were updated at 11 tests. Reference oil 1006-2 targets were introduced based on 5 tests.

Reference oil 1008-1 will need to be introduced. The surveillance panel approved the introduction of 1008-1 using existing 1008 targets. Reference Oil 1008-1 targets will be established once five operationally valid tests are received. Motioned by Dwight Bowden/Michael Kasimirsky. Approved 13-0-0 (approve/oppose/waive)

Reference oil 1009 (new category 5W30 reference oil) introduction will be based upon TMC's ability to schedule simultaneous calibration tests. No formal vote taken – panel consensus.

QI Deviations: There was one QI Deviation for the period. There have been 22 deviations from the QI Limits since the test was introduced in June of 2000. The lone QI Deviation written this period was due to a negative QI result on engine load. The test experienced a few short periods of erratic control that resulted in a final QI value of –0.041 for the test. No cause for the periods of erratic control was found in the laboratory's investigation of the problem. The TMC's opinion of this test was that the operational conditions of this test did not deviate enough from the expected norm to cause it to be considered invalid. If this test were used to recalculate U & L values for this parameter, in all likelihood this test would result in the same U & L limits after the new limits were rounded according to past practice. However, the laboratory was urged to strive to improve it's control capabilities so that this problem did not recur in the future.

The TMC reported no hardware changes were made this period.

### LDRTF Report

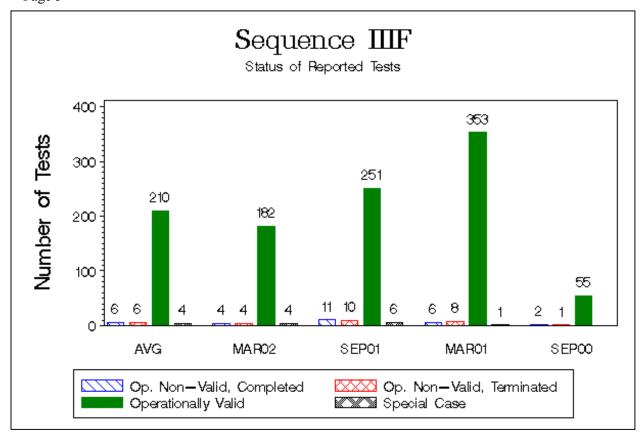
Scott Parke of the TMC has been tasked with leading the Light-Duty Rating Task Force. Because of the concern over severe Sequence IIIF WPD results the panel agreed to have a specific Sequence IIIF workshop prior to running the Sequence IIIG matrix. However, because of the aggressive schedule of starting the IIIG matrix the panel felt that having a workshop during the October timeframe may be more realistic. Under Sequence IIIG the panel agreed that a rater teleconference call should be conducted to address IIIG rating issues.

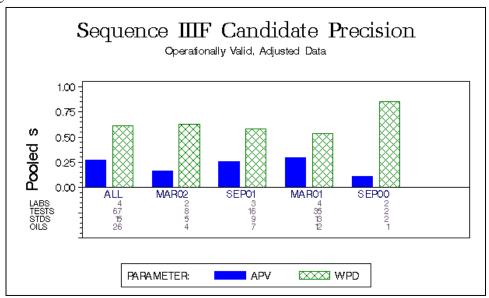
### RSI Report

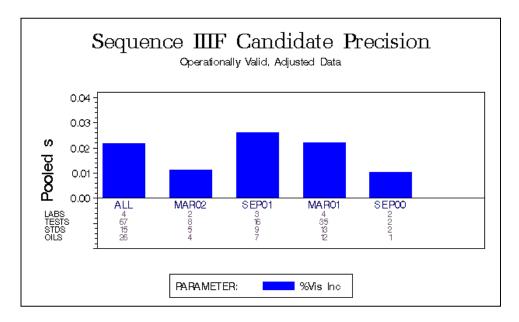
### RSI Sequence IIIF Semi-Annual Report Six-Month Period Ending March 31, 2002

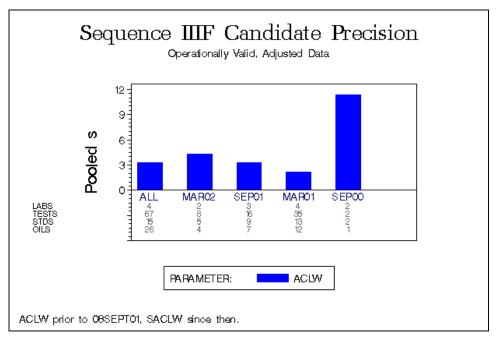
| STATUS OF REPORTED TESTS            |     |         |  |
|-------------------------------------|-----|---------|--|
| STATUS                              | N   | PERCENT |  |
| Operationally Non-Valid, Terminated | 4   | 2.1%    |  |
| Operationally Non-Valid, Completed  | 4   | 2.1%    |  |
| Operationally Valid                 | 182 | 93.8%   |  |
| Special Case                        | 4   | 2.1%    |  |
| Total Reported Tests                | 194 | 100.0%  |  |
| CAUSES FOR LOST TESTS               |     | N       |  |
| Oil Consumption                     | 1   |         |  |
| Control Problems 6                  |     | 6       |  |
| Sponsor Request 1                   |     |         |  |

| SEQUENCE IIIF PRECISION                                   |          |        |  |  |
|-----------------------------------------------------------|----------|--------|--|--|
| COMPONENTS OF REPLICATED DATA BASE                        | N        | 1      |  |  |
| Number of Tests                                           | 8        | 3      |  |  |
| Number of Oils                                            | 4        | 1      |  |  |
| Number of Labs                                            | 2        | 2      |  |  |
| Number of Stands                                          | 4        | 5      |  |  |
| Number of Severity Adjusted Avg C+L Wear Tests            | (        | )      |  |  |
| Number of Severity Adjusted Avg Piston Varnish Tests      | (        | )      |  |  |
| Number of Severity Adjusted % Vis Inc. Tests              | (        | )      |  |  |
| Number of Severity Adjusted Weighted Piston Deposit Tests | 4        | 1      |  |  |
|                                                           |          |        |  |  |
| VARIABLE                                                  | Pooled s | R      |  |  |
| Percent Vis Increase, Adjusted                            | 0.011    | 0.031  |  |  |
| Avg Piston Varnish, Adjusted                              | 0.162    | 0.454  |  |  |
| Weighted Piston Deposits, Adjusted                        | 0.630    | 1.763  |  |  |
| Avg Cam + Lifter Wear, Adjusted                           | 4.309    | 12.065 |  |  |
| Percent Vis Increase, Non-Adjusted                        | 0.011    | 0.031  |  |  |
| Avg Piston Varnish, Non-Adjusted                          | 0.162    | 0.454  |  |  |
| Weighted Piston Deposits, Non-Adjusted                    | 0.622    | 1.741  |  |  |
| Avg Cam + Lifter Wear, Non-Adjusted                       | 4.309    | 12.065 |  |  |









### Fuel Supplier Report

Jim Carter presented fuel batch analysis sheets for Detroit and Channelview distribution terminals for EEE fuel batches (Attachments 3 and 4, respectively). Note, that batches shipped from Channelview and Detroit are initially blended together at Channelview. EPA will be tentatively lowering and adding a window of ~25-35 ppm on sulfur soon. This will change the product for EPA emissions work. So supply of Sequence IIIF fuel (Product Code HF003) from Detroit will cease around September 2002 because of limited tankage and only will be available from Channelview. The product for Sequence IIIF testing will still be Product Code HF003. Detroit inventory 263,292, Channelview inventory 50,932. Report was accepted.

### **CPD Report**

The following information was distributed by Dwight Bowden as the CPD report:

### 1.) Rejections from 02/28/2002 to 05/01/2002:

Oil Coolers
Oxidation, 8 Pieces
Material replaced

### 2.) Technical Memos Issued

None for period (Last - Technical Memo 6, Dated 11/20/01)

### 3.) Batch Code Changes

None for period

### **GM Motorsport Report**

The following information was distributed by Sid Clark.

# **GM Raceshop:**

# **Sequence Test Part Inventory**

| Part #   | Description    | Qty. in<br>Stock | Comments               |
|----------|----------------|------------------|------------------------|
| 24502241 | Front Cover    | 60               |                        |
| 24502168 | Crankshaft     | 198              |                        |
| 24501696 | Connecting Rod | 627              | 5000 pcs. On order     |
| 24502260 | Cylinder Head  | 369              | 1188 castings in stock |
| 24502286 | Engine Block   | 67               | 186 castings on order  |

- Rejected materials
  - -1 Crankshaft for nicks, corrosion
- Returned materials
  - -4 Cylinder heads for failed exhaust seats
    - •2 run in IIIG testing
    - •2 run in IIIF testing (double length)

      —Processing dates;

»Jan. Oct. 2001 Jan. Feb. 2002

# **Cylinder Head Returns Investigative actions:**

- •2 Heads returned to Schwartz for Inspection
- •1 Head sent to Federal Mogul for inspection
- •Raceshop directed to perform 100% visual inspection on all outgoing materials

### To date:

Schwartz machine is still installing seats with 0.002" – 0.004" interference fit Federal Mogul confirms no changes in materials or processing Inspected heads show no signs of cracked seat pockets or other distress outside of high valve seat recession (intake and exhaust)

Cylinder heads will be 100% visual inspected by GM Race Shop prior to shipment to catch potential exhaust valve seat problems.

Report Accepted.

### O & H Report

Pat Lang presented Attachment 5.

The O & H panel recommended using a modified oil filter adapter that utilizes a circular orifice(0.5" ID) as opposed to the current hex-shaped orifice. This part removes an internal restriction in the oil flow to the oil filter compared to the previous part. The data shows that this part does not affect oil temperature and also shows that the oil pressure delta has been reduced with this part.

Pat then presented the revised external oil bypass system that the O & H panel has been developing to eliminate the oil temperature control problems laboratories have been experiencing when the filter goes into bypass mode. This revised system moves the existing bypass valve to a new, external part that is downstream of the oil cooler. This allows the stand

to maintain oil temperature control even if the oil filter is plugged or the system is operating in bypass mode.

**Motion** (Pat Lang/Sid Clark) Introduce the OHT External Oil Bypass System and modified Oil Filter Adapter into the Sequence IIIF test. Install a thermocouple in the external system to monitor the temperature differentials to detect bypass operation. No reporting of this additional temperature data is required. If bypass is detected, a note in the comments section of the test report shall be made. This change does not affect the current guidelines for oil cooler or oil filter replacement during a test. This change must be in place by 6/1/02. The motion passed 13-0-0.

Labs are to monitor the use of the system and report back to the O & H panel by August 1 on standardization suggestions during filter bypass conditions.

Pat presented results from the cylinder head round robin where six labs participated. The evaluation was done a three different deflections where the highest difference on any single load was 12.5 lbf and the average difference was 7 lbf. Based upon this review the O & H panel felt there were no laboratory head calibration problems. However, the TMC was requested to review this process during the next round of lab visits.

### Other O &H Topics:

Flush cart modifications to prevent casting sand recirculation will be completed by August 15, 2002.

Fluid control rack specification documentation will be completed June 15, 2002.

One item of note was the use of Type 1 and Type 2 solvents in the Sequence IIIF test. More work on this issue needs to be completed.

Clarifications to the cylinder honing "zeroing" procedure in the assembly manual is expected to be completed by June 15, 2002.

Batch Concept/Hardware recommendations still need to be implemented.

Investigations into random exhaust valve seat failures/valve recessions problems will be followed-up next report period.

O&H Report accepted.

### Status Of Wear Investigation

Three negatives have been received on the Sequence IIIF Information Letter ballot (Attachments 6-8) concerning the phosphate camshaft. Gordon Farnsworth stated that he agreed with Bob Olree's second comment on the ballot that the phosphate camshaft appears to

Sequence III Surveillance Panel Minutes

Detroit, MI - May 16, 2002

Page 10

eliminate wear discrimination on the available data. The available data was on the heavier Sequence IIIG valve springs. Charlie Leverett motioned that the information letter be withdrawn. Vote was: 12-1-0.

### Sequence IIIG Development Update

Sid Clark presented attachment 9. Concern over tempering of the camshaft in the engine was discussed. GM noted that their investigation of several metallurgical studies on several camshafts indicates that there is no known metallurgy issues that would suggest a camshaft problem.

Sid then reviewed some of the IIIG vs IIIF diiferences:

Sequence IIIG has the following:

Phosphate Camshaft
205 lb valve springs
Piston Ring Gapping Strategy (0.025" Top, 0.042 2<sup>nd</sup>)
OHT external oil filter bypass
OHT 0.5" ID oil filter adapter
Spark Plugs (possibly colder range)
100 hour test length
20 hour oil levels
Coolant temp 115 deg c
Oil temp 150 deg c
Inlet Air temp 35 deg c
Torque 250 Nm

GM recommends releasing the Sequence IIIG for preliminary testing.

Bob Olree presented an alternative piston deposit weighting factor scheme (Attachment 10).

| Crown Land=   | 0.2  |
|---------------|------|
| Lands (2&3) = | 0.2  |
| Grooves1-3=   | 0.1  |
| Undercrown=   | 0.1. |

These weighting factors weight the upper part of the piston heavier than the current Sequence IIIF factors and include the crown land that is currently not part of the WPD. Piston Skirt Varnish will remain a separate item. The panel did not vote to modify the current weighting factors. This was left as an unresolved item.

GM also stated that it believes that 100 hours is appropriate for oxidation severity and recommends that this length be used for the Sequence IIIG (Attachment 11). However, to be certain that the *IIIG* is twice as severe as the IIIF, GM felt that the test length may require 120 test hours. Further evaluation of this issue will occur after the matrix is run.

### Update from GF-4 Matrix Design Task Force Report

Don Marn's presentation is Attachment 12. Don is the GF-4 Matrix Design Task Force leader. John Zalar (TMC) will be the matrix project manager.

Scope: Is to select matrix formulations and determine a testing plan.

Objective: Design Test Matrix, determine test precision and LTMS limits. BOI and VGRA may also be addressed.

The surveillance panel will need to set pre-matrix requirements for matrix test labs and offer some feedback to the Matrix Design Task Force on desired reference oil viscosity grades and number of potential reference oils.

A tentative August 1 matrix start date has been stated. The number of matrix tests needed could be as high as 40 tests depending on oil selection. Proposed matrix design requires 4 tests per stand. Both dependent and independent labs are to be included. Number of tests/oil has not yet been determined.

Don requested feedback from the Sequence III panel on several items from his presentation. The panel feedback is captured on subsequent pages.

### The Precision Matrix for ASTM Test Methods

Mike McMillan's presentation is Attachment 13. GM's opinion is that the ASTM matrix should be focused on precision not base oil interchange and viscosity grade read across. GM felt that each stand should run 2 'true reference oils' of which bracket the pass/fail performance limits. The matrix should ideally consist of three oils that bracket each parameter being measured by the test method. GM sees no need to fund and conduct a formal matrix. GM's position is that precision data should be obtained through normal stand calibration.

### ACC Template Update

Jennifer Van Mullekom's presentation is Attachment 14. The ACC template will be updated as work progresses.

### Sequence IIIG Pre-Matrix Items

TMC was tasked with contacting non-calibrated Sequence IIIF labs that are interested in being part of the IIIG matrix to see if they can meet Sequence IIIG matrix participation requirements. Labs are to communicate to Don Marn (LZ) their intent to be in the matrix and number of stands by June 1. A rater conference call is to be held to review crown land flaking prior to the start of the matrix (GM, TMC and LDRTF are to take the lead on this item).

### Sequence IIIG Matrix Participation Requirements

After much discussion the following was agreed upon:

- 1. GM will pick three oils to demonstrate discrimination on pass/fail parameters by June 1. Note, all oils need not discriminate on all parameters.
- 2. Matrix labs will need to have been TMC calibrated laboratories prior to running the demonstration oils.
- 3. By June 30, 2002 the demonstration oils will need to be completed at each matrix lab. It is anticipated that 3 discrimination oils are to be run such that two operationally valid tests are obtained per oil. Motioned by Dwight Bowden. Seconded by Dave Glaenzer. Vote: 12-1-0.

### Matrix Design Feedback Items

The panel recommends to the Matrix Design Task Force that a minimum of three oils be chosen for the matrix that could be used as reference oils. These oils should cover two viscosity grades. Motioned approved 12-1-0.

The panel voted on the following Sequence IIIG matrix calibration requirements: The first stand in a lab requires 2 operationally valid *reference oil* tests and is to be in control after the second run. Subsequent stands in a lab only require two operationally valid *reference oil* tests. Stand is calibrated with no alarms after the last matrix test run. Thom Smith motioned. Vote: 3-1-9.

### **IIIG Development Items**

Labs are instructed to save EOT samples for additional post test analysis if needed.

### **Drain Oil Request**

Chris May on behalf of the ASTM Section D02.07C requested Sequence IIIF/IIIG EOT drain oil samples. The panel agreed that this was a worthwhile activity and member labs were asked to comply with the request. The chair was going to contact Chris for additional details.

### **Data Dictionary Review**

Charlie Leverett requested that the Sequence IIIFHD report packet be modified to remove lifter designations from report forms. Motioned by Charlie. Approved by consensus.

Also the TMC was requested to report severity adjustments for Viscosity Increase to six decimal places to labs after their LTMS review. The request was made to provide compatibility with the current Sequence IIIF data dictionary mnemonic lengths.

### ASTM Sequence IIIF Standard

GM and TMC to review latest draft copy and resubmit to facilitator

### Review Scope and Objectives

Objectives are below:

Assembly Manual Revision System Fluid Rack System Clarification Issue Draft 5 of IIIF Test Method Resolution of unexplained IIIF Wear Revise IIIF ASTM Standard Develop Sequence IIIG Test Introduce GF-3 Category Oil Revised Oil Cooling System

November 2002 June 2002 Done November 2002 August 2002 July 2002 November 2002 Done

### **New Business**

None

### Motions & Action Items

Motions & Action Items Sequence IIIF Surveillance Panel May 16, 2002

As Recorded at the Meeting by Ben Weber

- 1. Previous meeting minutes accepted as written.
- 2. TMC report accepted as presented with the noted precision and severity shifts for some parameters like WPD.
- 3. Test labs should review the groove piston ratings to see if there is any precision improvements that can be made, or if this measurement is difficult to accurately perform. One suggestion at the meeting concerned cleaning of the pistons. Dual ratings have been taking place at some of the test labs, and rating differences have not been a problem.
- 4. [Dwight B & Mike K] 1008-1 will be brought into the system using the older 1008 targets during normal calibration testing. Targets will be reviewed after 5 tests, then updated at 10, 20 & 30. Passed unanimously.
- 5. TMC will check into the possibility of coordinating the introduction of 1009 during a given time period that is acceptable to all test labs.
- 6. The group agreed that the next light-duty rating workshop should be held during the October timeframe. It was left open for later discussion about having a workshop before the next scheduled fall workshop. Scott Parke of the TMC will coordinate these future workshops for both heavy- and light-duty ratings.

- 7. The RSI report was accepted as presented.
- 8. The fuel supplier report was accepted as presented. By September 2002 EEE HF003 fuel for the IIIF, which will now be different than the new EPA fuel in terms of sulfur limits (approx. 25 35 ppm for the EPA version), will all come from their Houston location in Channelview, Texas. The fuel supplier will review sulfur levels from previous batches over the last few years to see where the sulfur maximum has been and possibly determine a specification or range for EEE HF003. Most of the sulfur levels have been around 10-15 ppm for the EEE HF003 fuel.
- 9. CPD OHT report was accepted as presented.
- 10. CPD GM Motorsports report was accepted as presented. GM will continue to investigate the valve seat recession problems.
- 11. [Pat L & Sid Clark] Accept the OHT external oil bypass system in conjunction with the 0.500" oil filter adapter and specified thermocouple for use in the IIIF test. Place a note in the comments section of the test report when the bypass occurs and at what test hours. Use of this system does not change the current guidelines outlined in the IIIF procedure for changing the oil filter and cooler during a test. Effective June 1, 2002. Passed unanimously.
- 12. Labs will experiment with the external oil bypass system and report back to the O&H panel about standardization on what to do when you go into bypass by August 2002.
- 13. TMC will review the head calibration data and technique during their next lab visits.
- 14. The test labs need to notify the O&H chair on what type of solvent specification they are using. Bob Rumford expressed interest in helping the O&H chair with this task.
- 15. [Charlie L & Dwight B] The Sequence III surveillance panel recommends that the Information Letter concerning the use of the MnP coating in IIIF testing be withdrawn. The vote was 12-0-1.
- 16. The SP decided that IIIG lab visits and a IIIG engine build workshop is not required at this time due to the very similar nature of the IIIG to the IIIF test method.
- 17. IIIG WPD ratings should be done using the current method and a new method proposed by GM listed below. There is some concern about chipping of the thin carbon on the crown land. It was suggested that the raters get together and discuss GM's proposal and any other IIIG rating concerns via teleconference mentioned below.
  - Crown land at 0.2
  - 2<sup>nd</sup> land at 0.2
  - 3<sup>rd</sup> land at 0.2
  - 1<sup>st</sup> groove at 0.1
  - 2<sup>nd</sup> groove at 0.1
  - 3<sup>rd</sup> Groove at 0.1
  - Under-crown at 0.1
- 18. The SP is interested in seeing as much IIIG development data as possible like individual cam lobe wear data, etc. It was decided to e-mail the membership whatever extra data can be distributed to the SP.
- 19. [Sid C & Dwight B] The IIIG test sponsor report was accepted as presented with the above items noted.
- 20. [Dwight B & Dave G] Current labs will need to run one demonstration IIIG test to prove initial performance prior to any formal matrix testing. PerkinElmer and SwRI are exempt from this requirement due to their development work. This demonstration run needs to be completed by June 30, 2002. ILSAC will define the oil by June 1, 2002. The labs are to communicate to Don Marn, chair of the Matrix Design Task Force, by June 1, 2002 their intention to comply with these requirements. The SP will convene once all the data is complete and determine if acceptability has been achieved. Passed unanimously.
- 21. [Charlie L & Dwight B] The Surveillance Panel recommends to the MDTF that at a minimum, 3 oils will be used and at least two viscosity oils. ILSAC will choose these oils. Passed unanimously.

Page 15

- 22. [Thom Smith & Tom Boschart] For calibrated IIIF laboratories, the 2-2 testing protocol will be used in the matrix. The vote was 3 for, 0 against, and 9 waives. This is a passing motion using the simple majority rule for Surveillance Panels.
- 23. The Memorandum of Agreement will need to be adjusted and reviewed to be in agreement with the decisions made by the Sequence III Surveillance Panel.
- 24. The SP or Matrix Design Task Force will need to discuss the proper quantity of oils blended to cover the future use of any of these oils as potential reference oils without having to go through a re-blend right after the matrix testing is complete.
- 25. TMC and GM will expedite the release of the IIIG test method and assembly manual. The target is to have this completed by the first week in June 2002.
- 26. The TMC will coordinate a IIIG rating teleconference by mid-June 2002.
- 27. The IIIG test labs will need to continue to measure MRV and CCS on EOT oil samples.
- 28. The test labs are also requested to send any of their IIIF EOT reference samples to Chris May of ASTM Section D02.07C by June 15, 2002. The sample size needed will be clarified later by Daryl B.
- 29. IIIF test method still needs to be completed as an ASTM standard.
- 30. [Charlie L & Dwight B] Remove the lifter designations from the IIIFHD test report. Passed unanimously.
- 31. [Charlie L & Dwight B] The TMC will start using 6 decimal places for the viscosity increase severity adjustment on their LTMS calibration sheets. Passed unanimously.

A motion for adjournment was made and accepted at 4:30 pm.

Attachment 1 1 Page 1 Reference

# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                       | PHONE / FAX / E-MAIL                                                                    |                                                                                                                           | SIGNATURE        |
|------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|------------------|
| Ed Altman<br>Ethyl Petroleum Additives, Inc.<br>P.O. Box 2158<br>Richmond, VA 23218-2158<br>USA      | 804-788-5279<br>804-788-6358<br>ed_altman@ethyl.com                                     | ☐ IIIF SURV PANEL  IIIF MAILING LIST  O&H SUBPANEL  O&H Mailing List                                                      | Present ###      |
| Beto Araiza<br>Test Engineering, Inc.<br>12718 Cimarron Path<br>#102<br>San Antonio, TX 78249<br>USA | 210-690-1958<br>210-690-1959<br>baraiza@ <del>lestong.com</del><br><i>TEI-NET</i> , Com | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present Ban Lawy |
| Zack Bishop Oronite Global Technology 4502 Centerview Drive Suite 210 San Antonio, TX 78228 USA      | 210-731-5605<br>210-731-5699<br>zrbi@chevron.com<br>DNOP FROM LIST.                     | ☐ IIIF SURV PANEL  ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☑ O&H Mailing List                                                  | Present          |
| Dwight H. Bowden OH Technologies, Inc. 9300 Progress Parkway P.O. Box 5039 Mentor, OH 44061-5039 USA | 440-354-7007<br>440-354-7080<br>dhbowden@ohtech.com                                     | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present Z        |
| Donald Bryant The Lubrizol Corporation 28400 Lakeland Boulevard Wickliffe, OH 44092 USA              | 440-347-2159<br>440-943-9004<br>debr@lubrizol.com                                       | ☐ IIIF SURV PANEL  IIIF MAILING LIST  O&H SUBPANEL  O&H Mailing List                                                      | Present          |

Page 2
Reference

# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                                       | PHONE / FAX / E-MAIL                                  |                                                                                                                           | SIGNATURE              |
|----------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|------------------------|
| Don Burnett ChevronPhillips Chemical Compan Chevron Tower 1301 McKinney Street Suite 2130 Houston, TX 77010-3030 USA | 713-289-4859 713-289-4865 burnede@cpchem.com          | ☐ IIIF SURV PANEL  IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List                                                    | Present                |
| William A. Buscher, Jr. Texaco Inc. P.O. Box 112 Hopewell Jet, NY 12533 USA                                          | 845-897-8069<br>845-897-8069<br>buschwa@aol.com       | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>☐ O&amp;H SUBPANEL</li><li>✓ O&amp;H Mailing List</li></ul> | Present                |
| James Carter Hialtermann Products 3520 Okemos Rd. Suite #6-176 Okemos, MI USA                                        | 517-347-3021<br>517-347-1024<br>JECarter@dow.com      | ☐ IIIF SURV PANEL  ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List                                                  | Present J. E. Ca       |
| Timothy L. Caudill Ashland Oil Inc. 22nd & Front Streets Ashland, KY 41101 USA                                       | 606-329-5708<br>606-329-3009<br>tlcaudill@ashland.com | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present Jumotly audill |
| Sid Clark GM Powertrain General Motors Corporation Mail Code 480-106-160 30500 Mound Rd. Warren, MI 48090-9055 USA   | 810-986-1929<br>810-986-2094<br>sidney.l.clark@gm.com | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present Sid            |

Attachment 1
Page 3
Reference

# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                                | PHONE / FAX / E-MAIL                                                                               |                                                                                                                           | SIGNATURE             |  |
|---------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|-----------------------|--|
| Francis R. Duffey DaimlerChrysler 800 Chrysler Road CIMS 482-00-13 Auburn Hills, MI 48236-2757 USA            | 248-576-7476<br>248-576-7490<br>fd13@daimlerchrysler.com                                           | ✓ IIIF SURV PANEL  ☐ IIIF MAILING LIST  ☐ O&H SUBPANEL  ☐ O&H Mailing List                                                | Present               |  |
| Frank Farber ASTM Test Monitoring Center 6555 Penn Avenue Pittsburgh, PA 15206 USA                            | 412-365-1030<br>412-365-1047<br>fmf@astmtmc.cmu.edu                                                | ☐ IIIF SURV PANEL  ✓ IIIF MAILING LIST  ☐ O&H SUBPANEL  ☐ O&H Mailing List                                                | Present frank fall    |  |
| Gordon R. Farnsworth<br>Infineum<br>P.O. Box 735<br>Linden, NJ 07036<br>USA                                   | 908-474-3351<br>908-474-3637<br>gordon.farnsworth@infineum.com                                     | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>☐ O&amp;H SUBPANEL</li><li>✓ O&amp;H Mailing List</li></ul> | Present               |  |
| Frank Fernandez  Oronite Global Technology  4502 Centerview Drive  Suite 210  San Antonio, TX 78228  USA      | 210-731-5603 210-731-5699 -ffer@shewron.con- FFer@shewron.con- FFer@shewron.con- FFer@shewron.con- | ☐ IIIF SURV PANEL  ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List                                                  | Present Frank Fernand |  |
| David L. Glaenzer Ethyl Petroleum Additives, Inc. 500 Spring Street P.O. Box 2158 Richmond, VA 23218-2158 USA | 804-788-5214<br>804-788-6358<br>dave_glaenzer@ethyl.com                                            | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>☐ O&amp;H SUBPANEL</li><li>✓ O&amp;H Mailing List</li></ul> | Present Land          |  |

| Attachment<br>Page | 4 |
|--------------------|---|
| Reference          |   |

# **ASTM SEQUENCE IIIF LIST**

May 16, 2002 Detroit, Michigan

| NAME / ADDRESS                                                                 | PHONE / FAX / E-MAIL                                    |                          | SIGNATURE               |
|--------------------------------------------------------------------------------|---------------------------------------------------------|--------------------------|-------------------------|
| Larry Hamilton                                                                 | 440-347-2326                                            | ☐ IIIF SURV PANEL        | Present                 |
| The Lubrizol Corporation<br>29400 Lakeland Boulevard                           | 440-347-4096<br>Idha@lubrizol.com                       | IIIF MAILING LIST        |                         |
| Wickliffe, OH 44092                                                            | Idild & Idbi[25].55fii                                  | ✓ O&H SUBPANEL           |                         |
| USA                                                                            |                                                         | O&H Mailing List         |                         |
|                                                                                |                                                         |                          | - R                     |
| Barry J. Jecewski<br>Ford Motor Company                                        | 313-594-6943<br>303-845-0613                            | ☑ IIIF SURV PANEL        | Present Sarry Ocean     |
| 21500 Oakwood Boulevard                                                        | bjecewsk@ford.com                                       | ☐ IIIF MAILING LIST      | $O^{\circ}$             |
| POEE Building, MD #34<br>P.O. Box 2053                                         |                                                         | ✓ O&H SUBPANEL           |                         |
| Dearborn, MI 48121-2053<br>USA                                                 |                                                         | O&H Mailing List         |                         |
| Michael T. Kasimirsky                                                          | 412-365-1033<br>412-365-1047<br>mtk@astmtmc.cmu.cdu     | <b>☑</b> IIIF SURV PANEL | Present Mile V. Rooming |
| ASTM Test Monitoring Center<br>6555 Penn Avenue<br>Pittsburgh, PA 15206<br>USA |                                                         | ☐ IIIF MAILING LIST      | V                       |
|                                                                                |                                                         | ✓ O&H SUBPANEL           |                         |
|                                                                                |                                                         | O&H Mailing List         |                         |
|                                                                                |                                                         |                          |                         |
| Brian Kundinger                                                                | 248-391-6100<br>248-391-6900<br>bkundinger@kundnger.com | ☑ IIIF SURV PANEL        | Present                 |
| Kundinger Controls<br>1771 Harmon Road                                         |                                                         | ☐ IIIF MAILING LIST      |                         |
| Auburn Hills, MI 48326                                                         |                                                         | ✓ O&H SUBPANEL           |                         |
| USA                                                                            |                                                         | O&H Mailing List         |                         |
| Patrick Lai                                                                    | 519-339-5611                                            | ☐ IIIF SURV PANEL        | Present                 |
| Imperial Oil Limited                                                           | 519-339-5866<br>patrick.k.lai@esso.com                  | ☐ IIIF MAILING LIST      |                         |
| 453 Christina Street Research Department                                       |                                                         | O&H SUBPANEL             | •                       |
| P.O. Box 3022                                                                  |                                                         | ─ O&H Mailing List       |                         |
| Sarnia, Ontario N7T7MI<br>CANADA                                               |                                                         | Ţ                        |                         |

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# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                                            | PHONE / FAX / E-MAIL                                                                                       |                                                                            | SIGNATURE    |
|---------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------|--------------|
| Patrick Lang<br>Southwest Research Institute<br>6220 Culebra Road<br>P.O. Box 28510<br>San Antonio, TX 78228<br>USA       | 210-522-2820<br>210-684-7523<br>plang@swri.edu<br>O&H Subpanel Chairman                                    | ✓ IIIF SURV PANEL  ☐ IIIF MAILING LIST  ✓ O&H SUBPANEL  ☐ O&H Mailing List | Present 16   |
| Charlie Leverett PerkinElmer Automotive Research, 5404 Bandera Road San Antonio, TX 78238 USA                             | 210-647-9422<br>210-523-4607<br>charlie.leverett@perkinelmer.com                                           | ✓ IIIF SURV PANEL  ☐ IIIF MAILING LIST  ✓ O&H SUBPANEL  ☐ O&H Mailing List | Present Junt |
| Vince Livoti Ciba Specialty Chemicals 540 White Plains Road P.O. Box 2005 Tarrytown, NY 10591-9005 USA                    | 914-785-4494<br>914-785-4249<br>vincent.livoti@cibasc.com                                                  | ✓ IIIF SURV PANEL  ☐ IIIF MAILING LIST  ☐ O&H SUBPANEL  ☐ O&H Mailing List | Present      |
| Mike McMillan GM R&D Center Building 1-6 Chemical & Environmental Science 12 Mile & Mound Roads Warren, MI 48090-9057 USA | 810-986-1935<br>810-986-2094<br>micheal.l.mcmillan@gm.com                                                  | ☐ IIIF SURV PANEL  IIIF MAILING LIST  O&H SUBPANEL  O&H Mailing List       | Present      |
| John Moffa Castrol International Technology Centre Whitchurch Reading, RG8 7QR ENGLAND                                    | 00441189765263<br>004411898 <del>41131-</del> SH1095<br>dohn_Moffa@burmahcastrol.com<br>Moffaj@Castrol.com | ✓ IIIF SURV PANEL ☐ IIIF MAILING LIST ✓ O&H SUBPANEL ☐ O&H Mailing List    | Present .    |

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# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                       | PHONE / FAX / E-MAIL                                                         |                                                                                                                           | SIGNATURE                |
|------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------|--------------------------|
| Alfredo Montez<br>Chevron Oronite<br>4502 Centerview Drive<br>#210<br>San Antonio, TX 78228<br>USA   | 210-731-5604<br>210-731-5694<br>AMMN@chevron.com                             | ✓ IIIF SURV PANEL  ☐ IIIF MAILING LIST  ✓ O&H SUBPANEL  ☐ O&H Mailing List                                                | Present                  |
| Mark Mosher Conflict  Mobil Technelogy Company  Billingsport Road  Paulsboro, NJ 08066  USA          | 856-224-2132<br>856-224-3628<br>mark.r.mosher@exxonmobil.com                 | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present MLM              |
| William M. Nahumck The Lubrizol Corporation 29400 Lakeland Boulevard Wickliffe, OH 44092 USA         | 440-347-2596<br>440-347-4096<br>wmn@lubrizol.com<br>Surveillance Panel Chair | <ul><li>✓ IIIF SURV PANEL</li><li>☐ IIIF MAILING LIST</li><li>✓ O&amp;H SUBPANEL</li><li>☐ O&amp;H Mailing List</li></ul> | Present Rep. by Allander |
| Rick Oliver Registration Services Inc. 2805 Beverly Drive Flower Mound, TX 75022 USA                 | 972-724-2136<br>210-341-4038<br>crickoliver@attbi.com                        | ☐ IIIF SURV PANEL  ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List                                                  | Present                  |
| Robert Oiree<br>GM Powertrain<br>30500 Mound Road<br>m/c 480-106-160<br>Warren, MI 48090-9055<br>USA | 810-947-0069<br>810-986-2094<br>robert.olree@gm.com                          | ☐ IIIF SURV PANEL  IIIF MAILING LIST ☐ O&H SUBPANEL  O&H Mailing List                                                     | Present                  |

# **ASTM SEQUENCE IIIF LIST**

May 16, 2002

| NAME / ADDRESS                                                                                                       | PHONE / FAX / E-MAIL                                                             |                                                                          | SIGNATURE           |
|----------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|--------------------------------------------------------------------------|---------------------|
| Robert H. Rumford<br>Specified Fuels & Chemicals, LLC<br>1201South Sheldon Road<br>Channelview, TX 77530-0429<br>USA | 281-457-2768<br>281-457-1469<br>rhrumford@s <del>pecified1.com</del><br>dow. com | ✓ IIIF SURV PANEL ☐ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List  | Present Affillation |
| Jim Rutherford<br>Chevron<br>100 Chevron Way<br>Richmond, CA 94802<br>USA                                            | 510-242-3410<br>510-242-1930<br>jaru@chevron.com                                 | ☐ IIIF SURV PANEL ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List  | Present             |
| Philip R. Scinto The Lubrizol Corporation 29400 Lakeland Boulevard Wickliffe, OH 44092 USA                           | 440-347-2161<br>440-347-9031<br>prs@lubrizol.com                                 | ☐ IIIF SURV PANEL  IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List   | Present             |
| Ben Weber<br>Southwest Research Institute<br>6220 Culebra Road<br>P.O. Box 28510<br>San Antonio, TX 78228<br>USA     | 210-522-5911<br>210-684-7530<br>bweber@swri.edu<br>Sub-Committee D02.B01 Chair   | ☐ IIIF SURV PANEL  ☑ IIIF MAILING LIST ☐ O&H SUBPANEL ☐ O&H Mailing List | Present Mh Willy    |

SEQUENCE HIF SURVEILLANCE PANEL MEETING.

**GUEST LIST** 

May 16, 2002 Detroit, Michigan Attachment 1
Page 8
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| NAME/ADDRESS                                                                            | PHONE/FAX/EMAIL                                                                                               | SIGNATURE           |     |
|-----------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------|---------------------|-----|
| John Shipins                                                                            |                                                                                                               |                     | 7   |
| 70401A<br>1588 Woodride                                                                 | Shipinsk                                                                                                      | i a) ttx-u          | ro. |
| Jennifer Van Mullekom<br>Ine Lubrizol Corp<br>29400 Lakeland Blyd<br>Wickliffe OH 44092 | (440) 347 2603                                                                                                | jwhf@lubrizol.com   |     |
| Ton Boscurer                                                                            | 248-350-0640<br>240-350-0025                                                                                  | TOM_BOSCHERT@EIRYZ. | Con |
| HOM SMITH  THE VALVOLINE COMPANY  1.0. BOX 14000  LEXINGTON LY 40504-1400               | 459 357-2766<br>459 357-2176<br>615mith@ashland.com                                                           |                     |     |
| CLIFF VENIER  DENNZOIL-QUAKER STATE  P.O. BOX 7569  THE WOODLANDS, TX  77387-7569       | 281-363-8060<br>281-363-8002<br>CLIFFORD. VENIER @72608. CL                                                   |                     |     |
| Alex Bofta Oronita 100 Chevron Way Richmond CH 94802                                    | 5162425220<br>abofe Chevron Texaco.co                                                                         | urBh                |     |
| Jo Martinez<br>Chevron Oronite Congany<br>100 Chevron Way<br>Richmond, CA 94802         | (SID) 142 5563<br>(SID) 242 1930<br>jogn@chevrontexaco.com<br>(Please in dute me in the<br>email 48t. Thank!) | Monthy              |     |

# SEQUENCE HIF SURVEILLANCE PANEL MEETING

GUEST LIST May 16, 2002 Detroit, Michigan

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|                                                                                         | 1                                              | <del></del>   |
|-----------------------------------------------------------------------------------------|------------------------------------------------|---------------|
| NAME/ADDRESS                                                                            | PHONE/FAX/EMAIL                                | SIGNATURE     |
| L.D. HAMILTON 24300 LAKELAND BIND. WILKELEY OH 44032                                    | 440/347-232/                                   | Lang Hair     |
| B. D. Domonkos THE LUBRIZOL CON. 19400 LAKELAND. BLUD. WICKLIPPET, OH 44292             | 440 347-2624<br>bdd @ fubritoc.com             | B. D. Domakos |
| Bob Olree<br>GM Power Train<br>M/C 480-106-160<br>30500 Mound Rd<br>Warran MI 48090-903 | 586-947-0069                                   | BerOhn        |
| VALUOINE<br>Ashland Ky                                                                  | (LOS) 379-5964<br>(LOS) 329-3009 FAX<br>       |               |
| JACK Kelley<br>Lubrizal 1<br>Wildeliffe, Ot 44092                                       | 440 347-1638<br>Jackson Lubrizot- co.~         | Melle         |
| JASIN H. Buide<br>OH TECHNOJOGIES I.<br>P.B. BOX 5039<br>Montos, DH 44061-5039          | 440-354-7007<br>440-354-7080<br>Jabonde Dataha | Ja Ble        |
|                                                                                         |                                                |               |

# **AGENDA**

# SEQUENCE IIIF SURVEILLANCE PANEL MEETING

Detroit, Michigan May 16, 2002

| Attachment | 2 |
|------------|---|
| Page       |   |
| Reference  |   |

- 1. APPOINTMENT OF RECORDER OF ACTIONS/MOTIONS
- 2. AGENDA REVIEW
- 3. MEMBERSHIP CHANGES
- 4. APPROVAL OF MINUTES FROM March 5, 2002 (Available for viewing at the TMC website)
- 5. REVIEW OF ACTION ITEMS

### **SEQUENCE HIF**

- 1. TMC TEST STATUS UPDATE MIKE KASIMIRSKY
  - A. Highlights of the LTMS Control Charts
  - B. Introduction of RO1009?
- 2. RSI REPORT Rick Oliver
- 3. FUEL SUPPLIER REPORT
- 4. CPD SUPPLIER REPORTS
  - A. OHT
  - B. GM MOTORSPORTS
- 5. O&H SUBPANEL REPORT PAT LANG
  - A. Change to new OHT oil filter adapter part
  - B. External oil filter adapter bypass
  - C. Cylinder Head RR Review
- 6. STATUS OF THE WEAR INVESTIGATION
  - A. Ballot Status
- 7. SEQUENCE HIG DEVELOPMENT UPDATE SID CLARK
  - A. Is the test ready for a Precision Matrix?
  - B. Available test results
  - C. IIIG specific test parts/equipment
  - D. Rebuild workshop
  - E. Piston ratings
  - F. Used Oil Requirements
  - G. ACC Template Update Jennifer Van Mullekom
  - H. Need written procedure
- 8. OLD BUSINESS
  - A. Review of Scope & Objectives
  - B. Status of ASTM Standard Sid Clark
- 9. **NEW BUSINESS** 
  - A. Drain Oil Request from Chris May, Section D02.07C

### ADJOURNMENT

# **Detroit**

| Attachment | 3       |
|------------|---------|
| Page       |         |
| Reference  | <u></u> |

PRODUCT: PRODUCT CODE: **EEE Unleaded Gasoline** 

HF003

Batch No.: 02D-04

02D-02

01D-24

Tank No.: 106

105 106

|                                  |                          |                                         |      |       | Analysis Date: |           |       |                 | 2/28/2002      | 1/3/2002 |
|----------------------------------|--------------------------|-----------------------------------------|------|-------|----------------|-----------|-------|-----------------|----------------|----------|
| TEST                             | METHOD                   | UNITS                                   | FED  | Specs | HAL            | TERMANN S | pecs  | RESULTS         | RESULTS        | RESULTS  |
|                                  |                          |                                         | MIN  | MAX   | MIN            | TARGET    | MAX   |                 |                |          |
| Distillation - IBP               | ASTM D86                 | ٩F                                      | 75   | 95    | 75             |           | 95    | 90              | 85             | 85       |
| 5%                               |                          | ۴F                                      |      |       |                |           |       | 116             | 117            | 120      |
| 10%                              | 1                        | °F                                      | 120  | 135   | 120            |           | 135   | 130             | 130            | 132      |
| 20%                              | 1                        | °F                                      |      |       |                |           |       | 151             | 149            | 154      |
| 30%                              |                          | ۴                                       |      |       | l              |           |       | 175             | 172            | 178      |
| 40%                              |                          | °F                                      |      |       |                |           |       | 202             | 198            | 204      |
| 50%                              |                          | °F                                      | 200  | 230   | 200            |           | 230   | 221             | 219            | 223      |
| 60%                              |                          | °F                                      |      |       | ŀ              |           |       | 232             | 229            | 234      |
| 70%                              |                          | °F                                      |      |       |                |           |       | 241             | 239            | 246      |
| 80%                              |                          | °F                                      |      |       |                |           |       | 258             | 257            | 265      |
| 90%                              |                          | °F                                      | 305  | 325   | 305            |           | 325   | 312             | 311            | 320      |
| 95%                              |                          | °F                                      |      |       |                |           |       | 333             | 334            | 341      |
| Distillation - EP                |                          | ۴F                                      |      | 415   |                |           | 415   | 389             | 385            | 399      |
| Recovery                         |                          | vol %                                   |      |       |                | Report    |       | 97.6            | 98.6           | 98.0     |
| Residue                          |                          | vol %                                   |      |       |                | Report    |       | 1.0             | 1.0            | 1.0      |
| Loss                             | 1                        | vol %                                   |      |       |                | Report    |       | 1.4             | 0.4            | 1.0      |
| Gravity                          | ASTM D4052               | °API                                    | 58.7 | 61.2  | 58.7           |           | 61.2  | 58.9            | 59.2           | 59.4     |
| Density                          | ASTM D4052               | kg/l                                    |      |       | 0.734          |           | 0.744 | 0.743           | 0.741          | 0.741    |
| Reid Vapor Pressure              | ASTM D323                | psi                                     | 8.7  | 9.2   | 8.7            |           | 9.2   | 9.1             | 9.1            | 9.2      |
| Reid Vapor Pressure              | ASTM D5191               | psi                                     |      |       |                | Report    |       | 9.00            | 9.10           | 9.10     |
| Carbon                           | ASTM D3343               | wt fraction                             |      |       |                | Report    |       | 0.8660          | 0.8650         | 0.8651   |
| Carbon                           | ASTM E191                | wt fraction                             |      |       |                | Report    |       | 0.8663          | 0.8648         | 0.8639   |
| Hydrogen                         | ASTM E191                | wt fraction                             |      |       |                | Report    |       | 0.1322          | 0.1309         | 0.1330   |
| Hydrogen/Carbon ratio            | ASTM E191                | mole/mole                               |      |       |                | Report    |       | 1.818           | 1.816          | 1.834    |
| Oxygen                           | ASTM D4815               | wt %                                    |      |       | 1              | •         | 0.05  | < 0.05          | <0.05          | < 0.05   |
| Sulfur                           | ASTM D5453               | ppm                                     |      | 1000  |                |           | 1000  | 5               | 8              | 11       |
| Sulfur                           | ASTM D2622               | wt%                                     |      | 0.1   |                | Report    |       | <0.001          | <0.001         | 0.0015   |
| Lead                             | ASTM D3237               | g/gal                                   |      | 0.05  |                |           | 0.01  | < 0.01          | <0.01          | < 0.01   |
| Phosphorous                      | ASTM D3231               | g/gal                                   |      | 0.005 |                |           | 0.005 | <0.0008         | <0.0008        | <0.0008  |
| Composition, aromatics           | ASTM D1319               | vol %                                   |      | 35.0  |                |           | 35.0  | 29.7            | 27.5           | 28.0     |
| Composition, olefins             | ASTM D1319               | vol %                                   |      | 10.0  |                |           | 10.0  | 0.6             | 1.0            | 0.6      |
| Composition, saturates           | ASTM D1319               | vol %                                   |      |       |                | Report    |       | 69.7            | 71.5           | 71.4     |
| Particulate matter               | ASTM D5452               | mg/l                                    |      |       |                |           | 1     | 0.7             | 0.6            | 0.6      |
| Oxidation Stability              | ASTM D525                | minutes                                 |      |       | 240            |           |       | >1000           | >1000          | >1000    |
| Copper Corrosion                 | ASTM D130                | *************************************** |      |       |                |           | 1     | 1               | 1              | 1        |
| Gum content, washed              | ASTM D381                | mg/100mls                               |      |       | Į.             |           | 5     | 1               | i              | 1        |
| Fuel Economy Numerator/C Density | ASTM E191                |                                         |      |       | 2401           |           | 2441  | 2436            | 2429           | #REF!    |
| C Factor                         | ASTM E191                |                                         |      |       | ]•             | Report    | ~,~,  | 1.0033          | 0.9983         | #REF!    |
| Research Octane Number           | ASTM D2699               |                                         | 93.0 |       | 96.0           | · copore  |       | 97.8            | 97.0           | 96.8     |
| Motor Octane Number              | ASTM D2099<br>ASTM D2700 |                                         | 55.0 |       | 33.0           | Report    |       | 88.6            | 87.6           | 88.4     |
| Sensitivity                      | NO 181 D27 00            |                                         | 7.5  |       | 7.5            | report    | ļ     | 9.2             | 9.4            | 8.4      |
| Net Heating Value, btu/lb        | ASTM D3338               | btu/lb                                  | 1,0  |       | ,.5            | Report    |       | #REF!           | #REF!          | 18490    |
| Net Heating Value, btu/lb        | ASTM D3338               | btu/lb                                  |      |       |                | Report    |       | #KE1":<br>18485 | #REF:<br>18452 | 18350    |
| Color                            | VISUAL                   | 1.75 ptb                                |      |       |                | •         |       | 10+07           | 10432          | 10330    |
|                                  | INIONAL                  | 1.75 ptb                                |      |       |                | Report    |       | L               |                |          |

# Channelview

Attachment 4
Page 1
Reference

PRODUCT:
PRODUCT CODE:

**EEE Unleaded Gasoline** 

HF003

Batch No.:

02C-06

02C-05

02C-03

Tank No.: 2012 2012 2012 analysis Date: 4/18/2002 4/4/2002 2/20/2002

|                                  |            |             |      |       |       | Anaive    | sis Date: | 4/18/2002 | 4/4/2002 | 2/20/2002 |
|----------------------------------|------------|-------------|------|-------|-------|-----------|-----------|-----------|----------|-----------|
| TEST                             | METHOD     | UNITS       | FED  | Specs | HAL   | TERMANN S |           | RESULTS   |          | RESULTS   |
|                                  |            |             | MIN  | MAX   | MIN   | TARGET    | MAX       |           |          |           |
| Distillation - IBP               | ASTM D86   | °F          | 75   | 95    | 75    | <u> </u>  | 95        | 86        | 89       | 85        |
| 5%                               |            | °F          |      |       |       |           |           | 113       | 113      | 114       |
| 10%                              |            | ۰F          | 120  | 135   | 120   |           | 135       | 127       | 128      | 127       |
| 20%                              |            | °F          |      |       |       |           |           | 148       | 150      | 148       |
| 30%                              |            | ۰F          |      |       |       |           |           | 173       | 173      | 171       |
| 40%                              |            | ۰F          |      |       |       |           |           | 201       | 199      | 199       |
| 50%                              | 1          | l °F        | 200  | 230   | 200   |           | 230       | 221       | 220      | 220       |
| 60%                              |            | °F          |      |       |       |           |           | 231       | 233      | 230       |
| 70%                              | 1          | • • চ       |      |       |       |           |           | 242       | 244      | 240       |
| 80%                              |            | ۰F          |      |       |       |           |           | 261       | 261      | 259       |
| 90%                              | Ī          | °F          | 305  | 325   | 305   |           | 325       | 317       | 315      | 315       |
| 95%                              |            | °F          |      |       | 1     |           |           | 334       | 334      | 332       |
| Distillation - EP                |            | ۰F          |      | 415   |       |           | 415       | 392       | 393      | 386       |
| Recovery                         | <u> </u>   | vol %       |      |       |       | Report    |           | 97.5      | 97.0     | 98.0      |
| Residue                          |            | vol %       |      |       |       | Report    |           | 1.0       | 1.0      | 1.0       |
| Loss                             |            | vol %       |      |       |       | Report    |           | 1.5       | 2.0      | 1.0       |
| Gravity                          | ASTM D4052 | °API        | 58.7 | 61.2  | 58.7  |           | 61.2      | 59.1      | 59.5     | 59.3      |
| Density                          | ASTM D4052 | kg/l        |      |       | 0.734 |           | 0.744     | 0.742     | 0.741    | 0.741     |
| Reid Vapor Pressure              | ASTM D323  | psi         | 8.7  | 9.2   | 8.7   |           | 9.2       | 9.2       | 9.2      | 9.1       |
| Reid Vapor Pressure              | ASTM D5191 | psi         |      |       |       | Report    |           | 9.20      | 9.20     | 9.10      |
| Carbon                           | ASTM D3343 | wt fraction |      |       |       | Report    |           | 0.0000    | 0.0000   | 0.8650    |
| Carbon                           | ASTM E191  | wt fraction |      |       |       | Report    |           | 0.8629    | 0.8645   | 0.8633    |
| Hydrogen                         | ASTM E191  | wt fraction |      |       |       | Report    |           | 0.1331    | 0.1314   | 0.1316    |
| Hydrogen/Carbon ratio            | AŞTM E191  | mole/mole   |      |       |       | Report    |           | 1.838     | 1.811    | 1.816     |
| Oxygen                           | ASTM D4815 | wt %        |      |       |       | •         | 0.05      | < 0.05    | <0.05    | < 0.05    |
| Sulfur                           | ASTM D5453 | ppm         |      | 1000  |       |           | 1000      | 5         | 5        | 5         |
| Sulfur                           | ASTM D2622 | wt%         |      | 0.1   |       | Report    |           | <0.001    | < 0.001  | <0.001    |
| Lead                             | ASTM D3237 | g/gal       |      | 0.05  |       | •         | 0.01      | < 0.01    | <0.01    | < 0.01    |
| Phosphorous                      | ASTM D3231 | g/gal       |      | 0.005 |       |           | 0.005     | <0.0008   | <0.0008  | <0.0008   |
| Composition, aromatics           | ASTM D1319 | vol %       |      | 35.0  |       |           | 35.0      | 30.6      | 28.6     | 29.1      |
| Composition, olefins             | ASTM D1319 | vol %       |      | 10.0  |       |           | 10.0      | 0.4       | 0.4      | 0.9       |
| Composition, saturates           | ASTM D1319 | vol %       |      |       |       | Report    |           | 69.0      | 71.0     | 70.0      |
| Particulate matter               | ASTM D5452 | mg/l        |      |       |       | •         | 1         | 0.5       | 0.5      | 0.7       |
| Oxidation Stability              | ASTM D525  | minutes     |      |       | 240   |           |           | >1000     | >1000    | >1000     |
| Copper Corrosion                 | ASTM D130  |             |      |       |       |           | 1         | 1         | 1        | 1         |
| Gum content, washed              | ASTM D381  | mg/100mls   |      |       |       |           | 5         | 2         | 1        | 1 1       |
| Fuel Economy Numerator/C Density | ASTM E191  |             |      |       | 2401  |           | 2441      | 2429      | 2429     | 2429      |
| C Factor                         | ASTM E191  |             |      |       |       | Report    |           | 1.0019    | 0.9983   | 0.9983    |
| Research Octane Number           | ASTM D2699 |             | 93.0 |       | 96.0  | •         |           | 97.8      | 97.6     | 97.5      |
| Motor Octane Number              | ASTM D2700 |             |      |       |       | Report    |           | 88.3      | 88.6     | 88.3      |
| Sensitivity                      |            |             | 7.5  |       | 7.5   | •         |           | 9.5       | 9.0      | 9.2       |
| Net Heating Value, btu/lb        | ASTM D3338 | btu/lb      |      |       | 1     | Report    |           | 0         | 0        | 0         |
| Net Heating Value, btu/lb        | ASTM D240  | btu/lb      |      |       |       | Report    |           | 18394     | 18482    | 18435     |
| Color                            | VISUAL     | 1.75 ptb    |      |       |       | Report    |           | Red       | Red      | Red       |

| Sequence IIIF | Operations | and H | ardware | Subpanel | Report | 5/16/02 |
|---------------|------------|-------|---------|----------|--------|---------|
|---------------|------------|-------|---------|----------|--------|---------|

| Attachment | _5_ |
|------------|-----|
| Page       |     |
| Reference  |     |

### Sequence IIIF O&H Report

Presented by: Patrick Lang May 16, 2002 Detroit, Michigan

### **Current Activities**

- Modified OHT oil filter adapter w/0.500 inch internal diameter
  - Reduced flow restriction
  - Data supports that adapter does not affect oil temperature.
  - Data shows that the oil pressure delta is reduced.

HIF ORH Report 5/16/02

## Current Activities (cont'd)

- External oil filter bypass system
  - Had concerns that the current IIIF/IIIG system could be in partial oil filter bypass and we were not aware of it.
  - OH Technologies designed a system that moves the bypass valve external to allow gauging (temp, press and flow).
  - System uses the stock GM differential pressure valve.

ILIF OAH Report 5/16/02

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Sequence IIIF Operations and Hardware Subpanel Report 5/16/02

| Attachment | 5    |
|------------|------|
| Page       | _ 2_ |
| Reference  |      |

### External Bypass (cont'd)

- Forces oil to pass through the cooler even if you are in a bypass mode.
- Performance checked on OHT and GM sponsored full length IIIG testing.
- Testing suggests that we are NOT in partial bypass during normal operation.
- System offers the advantage of maintaining temperature control if in a bypass mode.

UIF O&H Report 5/16/02

### **MOTION**

 Accept the OHT external oil bypass system in conjunction with the 0.500" oil filter adapter for use in the IIIF test. Use of this system does not change the current guidelines outlined in the IIIF procedure for changing the oil filter and cooler during a test. Motion is effective June 1, 2002.

IIIF OAH Report 5/16/02

### Current Activities (cont'd)

- · Cylinder head round-robin
  - Six labs participated
  - Assessment done at three different valve deflections
  - The highest difference (max -min) on any single position was 12.5 lbs.
  - The average difference across all positions was 7 lbs.

DIF ORH Report 5/16/02

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|  | Sequ | ience II | IF O | perations | and | Hardware | Sub | panel | Rei | oort | 5/1 | 6/ | 02 |
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| Attachment | _5 |
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| Page       | 3  |
| Reference  |    |

### O & H To-Do List

- Recommend changes to the flush cart to help prevent the recirculation of casting sand during the flush; complete by August 15, 2002
- Work with test developer to add the final touches on the documentation for the fluid control rack specification for incorporation into the procedure; complete by June 15, 2002.

### To -Do (cont'd)

- Clarify honing machine "zeroing" procedure in the assembly manual; complete by June 15, 2002
- Batch Concept/Hardware Control Task Force to generate Info. Letter 60 type document.
- Investigate random exhaust valve seat failures/valve recession.

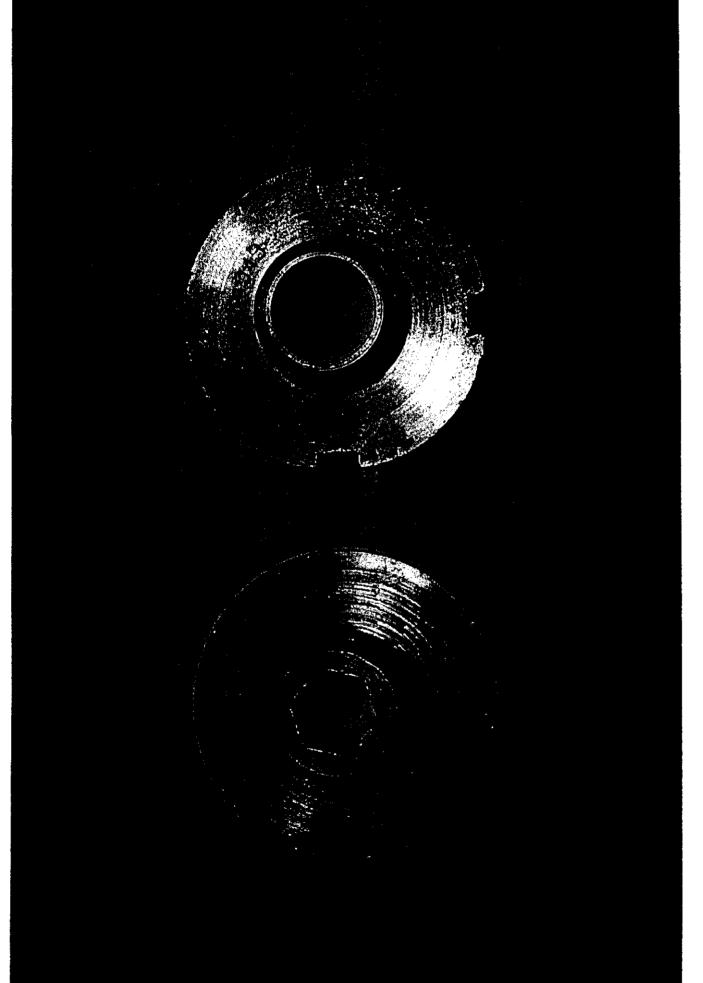
HIF OAH Report 5/16/02

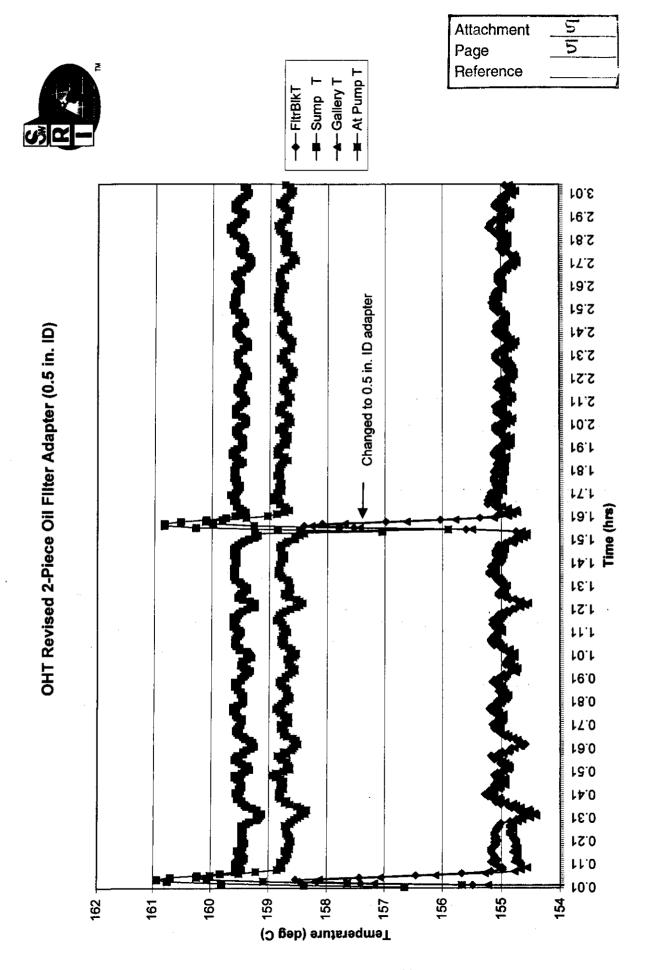
### To-Do (cont'd)

- · Solvent specification in IIIF procedure
  - Industry looking to settle on one type of solvent that can be used on both gas and diesel testing.
  - Push is towards specifying Type 2, flash point of approximately 140 deg. F
  - IIIF procedure states to use Type I, flash point of approximately 104 deg. F
  - Need to solicit IIIF labs to determine what is currently being used.

HIF OAH Report 3/16/02

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5 Attachment 6 Page At Pump P Reference ——OilGalyP → Oilln P 3.01 2.91 18.2 17.2 19.2 Changed to 0.5 in. ID adapter 15.5 OHT Revised 2-Piece Oil Filter Adapter (0.5 in. ID) 2.41 15.2 12.2 2.11 2.01 16.1 18.1 121 16.1 Time (hrs) 1.31 1.2.1 11.1 10.1 16.0 18.0 17.0 19.0 19.0 170 16.0 12.0 11.0 10.0 9 390 380 370 360 350 340 330 Pressure (kPa)

Attachment

Page Reference

# IIIF Round-Robin Cylinder Head Results

| 0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360         0.360 <th< th=""><th></th><th></th><th></th><th></th></th<>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |       |             |          |           |
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| 184.5     182.3     184     178       165.7     163.3     167     161.9       97.6     97.2     95     95       134.9     132.8     136     133.3       187.0     183.4     190     182.5       171.0     163.0     171     163.5       190.4     188.3     190     184.7       190.4     188.3     190     184.7       190.4     188.3     173     166.9       100.1     99.5     96     97.7       139.0     137.1     142     135.8       193.0     188.0     175     170       B     C     D     E     0.390       0.390     0.390     0.390     0.390     0.390       195.8     193.5     190     189.7       176.0     172.7     178.7     172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | Max   | Avg         | Std Dev  | Max - min |
| 165.7     163.3     167     161.9       97.6     97.2     95     95       134.9     132.8     136     133.3       187.0     183.4     190     182.5       171.0     163.0     171     163.5       171.0     163.0     171     163.5       190.4     188.3     190     184.7       190.4     188.3     190     184.7       190.4     188.3     173     166.9       100.1     99.5     96     97.7       193.0     137.1     142     135.8       193.0     188.0     175     170       B     C     D     E     0.390       0.390     0.390     0.390     0.390     0.390       195.8     193.5     190     189.7       176.0     172.7     178     172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 184.5 | 177.4 181.4 | 4 3.0    | 7.1       |
| 97.6 97.2 95 95 95 134.9 134.9 132.8 136 133.3 135.3 137.0 183.4 190 182.5 177.0 163.0 177 163.5 190.4 188.3 190 184.7 190.4 188.3 190 184.7 173 166.9 177.2 168.3 173 166.9 175.6 168.0 175.6 168.0 175.6 168.0 0.390 0.390 0.390 0.390 0.390 0.390 172.7 176.0 176.0 172.7 176.0 176.0 172.7 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 167.0 | 161.9 163.8 | 2.1      | 5.1       |
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| 187.0   183.4   190   182.5   171.0   163.0   171   163.5   171.0   163.0   171   163.5   190.4   188.3   190   184.7   172.2   199.5   199.5   199.5   199.5   199.6   197.7   175.6   168.0   175.6   168.0   175   170   195.8   193.0   0.390   0.390   0.390   0.390   0.390   0.390   0.390   0.390   0.390   0.390   172.7   172.9   172.9   172.9   172.9   172.9   172.9   172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | 136.0 | 132.8 133.9 | 1.3      | 3.2       |
| B C D E  0.375 0.375 0.375 0.375 190.4 188.3 190 184.7 171.2 168.3 173 166.9 100.1 99.5 96 97.7 139.0 137.1 142 135.8 193.0 188.0 198 187.9 175.6 168.0 175 170  B C D E  0.390 0.390 0.390 0.390 0.39 176.0 172.7 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 190.0 | 180.6 185.0 | 3.4      | 9.4       |
| B C D E  0.375 0.375 0.375 0.375 190.4 188.3 190 184.7 171.2 168.3 173 166.9 100.1 99.5 96 97.7 139.0 137.1 142 135.8 193.0 188.0 198 187.9 175.6 168.0 175 170  B C D E  0.390 0.390 0.390 0.390 0.391 176.0 172.7 178 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 171.0 | 163.0 166.2 | 3.8      | 8.0       |
| B C D E  0.375 0.375 0.375 0.375 190.4 188.3 190 184.7 171.2 168.3 173 166.9 100.1 99.5 96 97.7 139.0 137.1 142 135.8 193.0 188.0 198 187.9 175.6 168.0 175 170  B C D E  0.390 0.390 0.390 0.390 0.391 176.0 172.7 178 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |       |             | Average  | 5.9       |
| 0.375         0.375         0.375         0.375           190.4         188.3         190         184.7           171.2         168.3         173         166.9           100.1         99.5         96         97.7           139.0         137.1         142         135.8           193.0         188.0         198         187.9           175.6         168.0         175         170           B         C         D         E           0.390         0.390         0.390         0.390           195.8         193.5         190         189.7           176.0         172.7         178         172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |       |             |          |           |
| 190.4 188.3 190 184.7<br>171.2 168.3 173 166.9<br>100.1 99.5 96 97.7<br>139.0 137.1 142 135.8<br>193.0 188.0 198 187.9<br>175.6 168.0 175 170<br>B C D E<br>0.390 0.390 0.390 0.390 0.390 175.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Max   | Avg         | Std Dev  | Max - min |
| 171.2     168.3     173     166.9       100.1     99.5     96     97.7       139.0     137.1     142     135.8       193.0     188.0     198     187.9       175.6     168.0     175     170       B     C     D     E       0.390     0.390     0.390     0.390       176.8     172.7     178     172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 190.4 | 181.6 187.3 | <u> </u> | 8.8       |
| 139.0 137.1 142 135.8 139.0 137.1 142 135.8 139.0 137.1 142 135.8 135.8 175.6 168.0 175 170 175.6 168.0 175 170 E E O.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.39 | 173.0 | 166.9 169.0 |          | 6.1       |
| 139.0 137.1 142 135.8<br>193.0 188.0 198 187.9<br>175.6 168.0 175 170<br>B C D E<br>0.390 0.390 0.390 0.390 0.3<br>195.8 193.5 190 189.7                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 100.1 | 96.0 98.5   |          | 4.1       |
| 193.0 188.0 198 187.9<br>175.6 168.0 175 170<br>B C D E<br>0.390 0.390 0.390 0.390 0.3<br>176.0 172.7 178 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |       | 135.8 138.0 | 2.2      | 6.2       |
| B C D E C 0.390 0.390 0.390 0.175.0 176.0 172.7 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 198.0 | 185.5 190.8 | 8 4.6    | 12.5      |
| B C D E 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.30 | 175.6 | 168.0 171.3 | 3 3.3    | 7.6       |
| B C D E C D.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0.390 0. |       |             | Average  | 7.6       |
| 0.390         0.390         0.390         0.390         0.390         0.390           195.8         193.5         190         189.7           176.0         172.7         178         172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |       |             |          |           |
| 195.8         193.5         190         189.7           176.0         172.7         178         172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | Max   | Avg         | Std Dev  | Max - min |
| 176.0 172.7 178 172.9                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 195.8 | 185.9 191.3 | 3.5      | 9.6       |
| 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | 178.0 | 171.4 173.8 | 3 2.6    | 9.9       |
| 101.4 102.3 101.9 97 99.9 101.5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 102.3 | 97.0 100.7  | 7 2.0    | 5.3       |
| 146 140                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | 146.0 | 140.0 142.1 |          | 0.9       |
| 197.2 198.7 193.5 190 193.2 190.6                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 198.7 | 190.0 193.9 | 3.5      | 8.7       |
| 176.0 181.0 172.9 181 174 172.2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 181.0 | 172.2 176.2 | 3.9      | 8.8       |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |       |             |          | 31        |

# IIIF Operations and Hardware Subpanel

| Language Commence | Ь |
|-------------------|---|
| Page              |   |
| Reference         |   |

# Negative

Date:

4/24/02

Ballot Number:

D02.B0 (02-03)

Close Date: MAY 08, 2002

Item Number:

2 PROPOSED SEQUENCE IIIF INFORMATION LETTER 02-X

TECHNICAL CONTACT: JOHN L ZALAR (412) 365-1005

(REFERENCE Z9452Z)

Member's Name:

**ROBERT M OLREE** 

Address:

136 ECKFORD

TROY

MI 48098

Phone Nr:

8109470069

Fax Nr: 8109862094

Email Address:

Robert.Olree@GM.com

Comment:

My negative is based upon two issues:

1) Only one standard IIIF test was run with a phosphated camshaft on an oil that was expected to generate a failing result. It did not fail.

2) Supporting data run under non-standard test conditions using IIIG valve springs also indicated

that phosphating the camshaft eliminates wear discrimination.

All of the above indicats that phosphating the camshafts eliminates the ability of the Sequence IIIF Test to discriminate wear.

# Negative

Date:

5/10/02

Ballot Number:

D02.B0 (02-03)

Close Date: MAY 08, 2002

Item Number:

PROPOSED SEQUENCE IIIF INFORMATION LETTER 02-X

TECHNICAL CONTACT: JOHN L ZALAR (412) 365-1005

(REFERENCE Z9452Z)

Member's Name:

MICHAEL J RILEY

Address:

2848 WAKEFIELD DR

CANTON

MI 48188

Phone Nr:

3133903059

Fax Nr: 3138453169

Email Address:

MRILEY2@FORD.COM

Comment:

Ford votes negative because the manganese-phosphate coated camshaft is expected to change the IIIF tests ability to evaluate engine oil wear.

### Negative

Attachment 8
Page 1
Reference

Date:

4/19/02

**Ballot Number:** 

D02.B0 (02-03)

Close Date: MAY 08, 2002

Item Number:

002

PROPOSED SEQUENCE IIIF INFORMATION LETTER 02-X

TECHNICAL CONTACT: JOHN L ZALAR (412) 365-1005

(REFERENCE Z9452Z)

Member's Name:

MICHAEL L MC MILLAN

Address:

**GENERAL MOTORS CORP** 

R&D CNTR/BLDG 1-6

30500 MOUND RD-MC 480-106-160

WARREN

MI 48090

Phone Nr:

8109861935

Fax Nr: 8109862094

**Email Address:** 

MICHAEL.L.MCMILLAN@GM.COM

### Comment:

1. Insufficient data were presented at the Surveillance Panel meeting where the decision was made to issue this letter. Only one Sequence IIF test was run with a phosphated camshaft. That run was on an oil containing only 0.03% phosphorus, and would have been expected to produce high wear. It did not. Four other tests were run under non-standard IIIF test conditions with higher load springs. These tests again showed no discrimination between the 0.03% phosphorus oil and oils 433-1 and 1006-2. Because of the lack of IIIF data under standard test conditions, and because the data obtained under non-standard conditions indicates that phosphating the camshaft eliminates wear discrimination, we believe it is premature to issue this information letter.

Affectment 9
Page 1
Reference

## Sequence IIIG Development Update

Sid Clark

May 16, 2002

GM

Sequence IIIG Development Data 7.18 7.79 8.69 8.76 8.48 9.45 PSV 7.96 8.32 8.62 8.52 8.8 7.52 7.53 ₹ Ž 7.94 8.21 9.17 9.07 WPD 2.16 2.36 3.92 2.85 3.16 2.82 3.32 4.64 2.64 2.52 2.52 3.27 3.53 2.74 2.53 3.35 3.24 2.62 ¥ Wear 17.6 49.6 N/A 51.3 38.5 17.6 57.2 105 267 267 153 153 57 57 270 483 11.7 337 14 27 6467 1077 5601 <u>고</u> 130 130 130 133 138 149 293 173 170 170 92 102 198 175 587 88 Fe @ Initial ۲× 16 8 9 42 9 7 9 4 2 2 4 တ တ တ ဖ Bar 22222222222 Yes Yes Yes Yes ટ 2222 ō MK/P M ₹ F MK/P MK/P MK/P MΒ MB MB æ MΒ 8 98 MB MB MB ξ ¥ ₽ MΚ Spring Load 180

Proto-type GF-4

5W-20

PE/05

0.095 Phos.

5W-30 0W-30

PE/03

PE/04

SR/07

**GM-1** 

0.05 Phos.

0.05 Phos.

5W-30 5W-30

PE/02

@ 77.8h 4.66 @ 76.8h

4.47

4.63 4.98

3.61 @ 80h 4.09

窗窗

433-1 433-1

> 5W-30 5W-30 5W-30

433-1

Test Oil

Viscosity

Lab/Run#

SR/01 SR/02 PE/01 SR/03

4

180 180 180 180

1006 Reformulated 403 Reformulated

0.03 Phos. 0.03 Phos.

5W-30 5W-30

SR/04 SR/05 SR/06

8.4

3.78

3.99

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Attachment

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3.4 4.2

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3.5

12.8

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MK/P

Reference 538

SR/14

PE/11

3.92

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Proto-type GF-4

0.095 Phos.

5W-30 5W-20

0.03 Phos.

0.03 Phos.

GF-3 GF-3

5W-20

5W-20

PE/06 SR/08

5W-30 5W-30

SR/09 SR/10

PE/07

Proto-type GF-4

5W-20 5W-20

PE/09 SR/13 PE/10

Proto-type GF-4

0.095 Phos.

5W-30

GF-3

Proto-type GF-4

0.03 Phos.

5W-30 5W-20

PE/08

**SRV11** 

SR/12

4.3

8.8

# Sequence IIIG Tests with Phosphated Camshafts

| Lab/Run# | Viscosity | Test Oil          | %Vis. Inc. | Avg. Wear | WPD  | PSV  | Oil Cons. |
|----------|-----------|-------------------|------------|-----------|------|------|-----------|
| PE/08    | 5W-30     | 0.03 Phos.        | 170        | 51.3      | 3.53 | 9.07 | 3.78      |
| PE/09    | 5W-20     | Proto-type GF-4   | 102        | 57.2      | 2.53 | 7.74 | 3.78      |
| PE/10    | 5W-30     | 0.095 Phos.       | 166        | 17.6      | 3.35 | 9.45 | 60.9      |
| PE/11    | 10W-30    | GF-3              | 175        | 17.6      | 3.24 | 8.21 | 3.4       |
| SR/13    | 5W-20     | Proto-type GF-4   | 88         | 38.5      | 2.79 | 7.94 | 3.95      |
| SR/14    | 5W-20     | GF-3 TMC Ref. 538 | 118        | 12.8      | 3.5  | 9.16 | 4.2       |

| Attachment | ٩           |
|------------|-------------|
| Page       | 3           |
| Reference  |             |
|            | <del></del> |

Attachment Page

Reference

## IIIG / IIIF Hardware Differences Manganese phosphate coated camshaft

205 lb. valve springs

Piston rings (gapping strategy)

OHT external oil filter bypass system

OHT large "ID" oil filter adapters

Spark plugs

Currently investigating colder heat range

# IIIG vs IIIF Test Conditions

• Test length 100h vs 80h

• 20h levels vs 10h

-(5500ml initial with 472 ml additions)

• Coolant temp 115°C vs 122 °C

• Oil temp 150 °C vs 155 °C

• Inlet air temp 35 °C vs 27 °C

• 250 Nm vs 200Nm @ 3600 RPM

Rings .025 Top .042 2nd vs .042 / .038

# Sequence IIIG Development

- Next Steps;
- Release test for preliminary testing
- Outline Precision Matrix requirements
- Write Research Report
- Revise IIIF Operating Procedure & Assembly Manual to reflect IIIG testing requirements

<u>GM</u>

| Attachment | /0 |
|------------|----|
| Page       | 1  |
| Reference  |    |

### **DISCUSSION**

### ALTERNATIVE PISTON DEPOSIT WEIGHTING FACTORS

GM Powertrain is concerned that the crown land is not comprehended in the current ratings.

Possible alternative weighting factors:

| Crown La             | nd 0.2             | 1st Groove             | 0.1 |
|----------------------|--------------------|------------------------|-----|
| 2 <sup>nd</sup> Land | 0.2                | 2 <sup>nd</sup> Groove | 0.1 |
| 3 <sup>rd</sup> Land | 0.2                | 3rd Groove             | 0.1 |
|                      | <b>Under Crown</b> | 0.1                    |     |

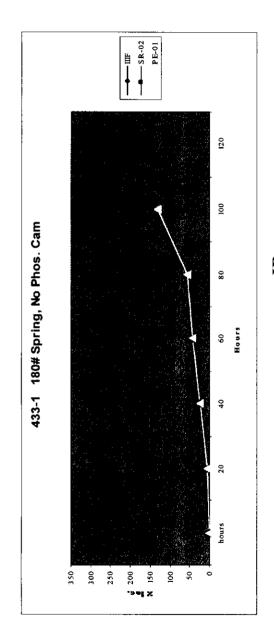
### For example:

| <u>Lab/Run#</u> | WPD OLD | WPD NEW     |
|-----------------|---------|-------------|
| <b>SR/6</b>     | 2.85    | 2.43        |
| <b>SR/7</b>     | 4.64    | 3.47        |
| SR/8            | 2.52    | 2.01        |
| SR/9            | 3.27    | 2.38        |
| <b>SR/10</b>    | 3.31    | 2.47        |
| <b>SR/12</b>    | 2.74    | 2.10        |
| <b>SR/13</b>    | 2.79    | <b>1.79</b> |
| <b>SR/14</b>    | 3.50    | 2.35        |

Piston skirt varnish (PSC) would remain a separate limit.

**Bob Olree** 

## Is the Test Long Enough?



| fion                   |      |      |      |
|------------------------|------|------|------|
| <u>IK</u><br>Nitration | 15   | 290  | 120  |
| Oxidation              | 230  | 3767 | 964  |
|                        | IIIF | SR-2 | PE-1 |

• Similar results to SR-2 were obtained on a 5W-20 GF-3+ oil (run outside GPSII Development Group)

Attachment

Page Reference

• To be certain that the IIIG test is twice as severe as the IIIF in oxidation severity, may require a 120 hour fest



## GF-4 Matrix Design Task Force Report to Sequence IIIG Surveillance Panel

Crowne Plaza Hotel Detroit Michigan May 16, 2001

| <u> </u> |
|----------|
|          |
|          |

# GF-4 Matrix Design Task Force

### SCOPE

- GF-4 Testing Matrix Design
- Select Formulations to be Used
- Determine a Testing Plan

### OBJECTIVE

- Design Test Matrix (For New GF-4 Tests) to Provide:
- Test Precision and LTMS Limits
- BOI and VGRA
- may be addressed
- Direction from ASTM PCEOCP, ILSAC, API and ACC

# **MATRIX PROJECT MANAGER**

12

Attachment

Reference

Page

John Zalar (TMC) (Accepted)

# GF-4 Matrix Design Task Force

# ILSAC / API / ACC Input

- Design Assumptions
- BOI and VGRA from GF-3 May be Adopted
- May need supplemental VGRA
- Use Three Technologies
- **Maximum Two New Tests**
- Sequence IIIG and Sequence VIC

# Assumptions Relating to Matrix Design

- **Testing Capacity**
- Seven Labs and Ten Test Positions
- Minimum Number of Formulations
- Dictated by Sequence IIIG (Three to Six Oils?)

12

Attachment

Page Reference

€ LUBRIZOL

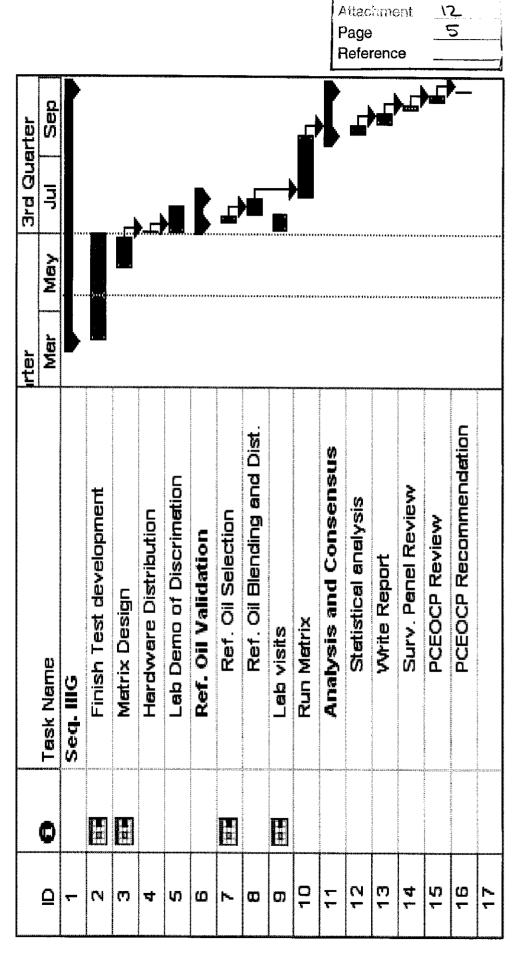
# **GF-4 Matrix Testing**

## • SEQUENCE IIIG

| Attachment | 12 |
|------------|----|
| Page       |    |
| Reference  |    |



# PROPOSED IIIG MATRIX TIMELINE



Attachment



# PROPOSED IIIG MATRIX

# **Assumptions** (To be confirmed)

Number of Labs --

Independent --

Dependent --

Number of Stands --

Stand Calibration Protocol --

Number of Tests / Stand --

Number of Formulations --

Number of Viscosity Grades Number of Technologies Number of Base Oils

Number of Tests / Oil

10 3/2

**TBD** 

Attechment

Reference

Page

1 (Slate) 2 or 3?

12

6

TBD

# PROPOSED IIIG MATRIX

### Next Steps?

Next GF-4 MDTF Meeting -

--- Today / Here / Next

 Future Decisions Based on Input from Sequence IIIG Task Group Be Aware of Timeline Needs & Constraints!

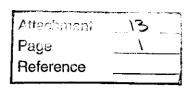
Attachment

Page Reference

We need your help!

## The Precision Matrix for ASTM Test Methods

BOI And/Or VGRA Included?



# The Role of ASTM

precision statements as a mandatory ASTM develops test methods with part of the test method BOI and VGRA issues are outside the domain of ASTM

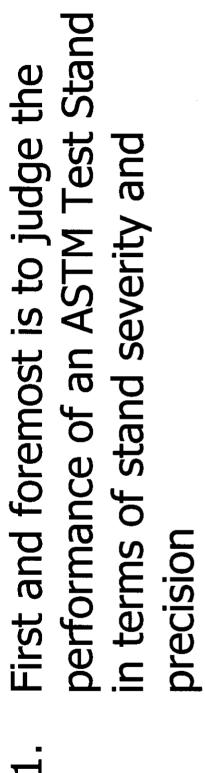
should focus on precision and not BOI Therefore, the Surveillance Panel or VGRA issues

Attachment

Reference

Page

### The Goals of the ASTM **Precision** Matrix



Determine stand-to-stand severity and precision within a laboratory

Attachment

Reference

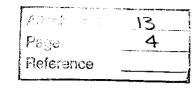
Page

Determine laboratory-to-laboratory precision and severity differences



## Determination of Test Stand Severity and Precision

- In the past, this has been done by running a minimum of two 'true' reference oils in each stand
- This would <u>not</u> include running a reference oil in a different viscosity grade or base oil
- Thus, each test stand in the precision matrix would run, at a minimum, two 'true' reference oils.

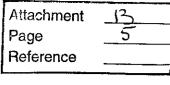


## The Goals of the Reference Oils (or Calibration Oils)



It may include more than 3 oils, but 5 seems to much, and 1 is not enough

closely represent the chemistries that And ideally, the reference oils should the test method is trying to measure



### Summary

- focus on the *precision* requirements of The ASTM Surveillance Panels should any proposed matrix
- BOI and VGRA is not a function of **ASTM**
- STM Funding for BOI and VGRA is not a function
  - Any BOI and/or VGRA matrix can not compromise the precision matrix

13

### Adada ear 13 Page 7 Reference

### Conclusion

Based on these requirements,

- GM sees no need to fund and conduct a formal precision matrix
- parameters should be obtained through normal calibration of referenced stands Sufficient data to establish all precision

| Attachment | 14 |
|------------|----|
| Page       |    |
| Reference  |    |
|            |    |

### **ADDENDUM K1**

### DRAFT TEMPLATE CHECKLIST

### **Purpose**

The Checklist for Comparing Tests to the Template is used to assess progress in new engine test development against the Code Acceptance Criteria and Action Plans. The checklist is updated periodically during the course of test development and is provided to, and discussed with, the appropriate ASTM test development task force.

The rating scale for comparing test development to the Template is as follows:

- A -- Completed
- B -- In Progress
- C -- Planned
- D -- No Action

Test Name Sequence IIIG Assessment Date

American Chemistry Council Code of Practice Appendix K - Template for Acceptance of New Tests

| 14 |
|----|
|    |
|    |
|    |

### A. Precision, Discrimination and Parameter Independence

A.1 Precision

 $E_p = d_p/Spp$ ,  $E_p \ge 1.0$  for all pass/fail parameters  $d_p = Smallest$  difference of practical importance Spp = Pooled standard deviation at target level of performance

| Parameter              | dp | Spp | Ep | ≥1.0? |
|------------------------|----|-----|----|-------|
| Viscosity Increase (%) |    |     |    |       |
| Viscosity Increase (%) |    |     |    |       |
| WPD                    |    |     |    |       |
| APV                    |    |     |    |       |
| ACLW                   |    |     |    |       |
| OC                     |    |     |    |       |

### Comments:

A survey was not performed for Oil Consumption

### A.2 Discrimination

For each test parameter in A.1, at least one of the oils used in proof-of-concept testing, matrix testing, or calibration testing must be statistically significantly different from at least one of the remaining oils. This difference must be in the correct direction, i.e., a poor oil should not test out as significantly better than a good oil. Significant difference may be declared with a p-value of 10% or less. Multiple comparison techniques (Tukey, Scheffe, Bonferroni, etc.) for the least-square means of the oils are preferred comparison techniques and should be stated in the analysis. Note that these least-squares means are not necessarily proposed LTMS targets.

RATING SCALE: A - Completed; B - In Progress; C - Planned; D - No Action

**Comments:** 

| 17 |
|----|
| 3  |
|    |
|    |

|                    |                                                                                               | Attachment _    | \4       |  |  |  |
|--------------------|-----------------------------------------------------------------------------------------------|-----------------|----------|--|--|--|
| В.                 | Severity and Precision Control Charting                                                       | Page            | 4        |  |  |  |
|                    |                                                                                               | Reference       |          |  |  |  |
|                    | R1 Is an ITMS for reference oil tests in place which is                                       | consistent      |          |  |  |  |
|                    | B.1 Is an LTMS for reference oil tests in place which is consistent with CMA Code Appendix A? |                 |          |  |  |  |
|                    | with civil code ripperdix ri.                                                                 |                 |          |  |  |  |
|                    | B.2 Are appropriate data transforms applied to test re                                        | sults?          | _C_      |  |  |  |
|                    | Comments: Inverse Square Root is used for Viscosity Increase.                                 |                 |          |  |  |  |
| C.                 | C. Interpretation of Multiple Tests                                                           |                 |          |  |  |  |
|                    | <u>Requirements</u>                                                                           |                 |          |  |  |  |
|                    | C.1 Is a suitable system in place to handle repeat tests                                      | on a            |          |  |  |  |
|                    | candidate oil?                                                                                |                 | C        |  |  |  |
|                    | Type: MTAC                                                                                    |                 |          |  |  |  |
|                    | C.2 Has a method for the determination and handling of outlier results been defined?          |                 |          |  |  |  |
|                    | Comments:                                                                                     |                 |          |  |  |  |
| D.                 | Action Plan                                                                                   |                 |          |  |  |  |
| D.1 Reference Oils |                                                                                               |                 |          |  |  |  |
|                    | Do the majority of reference oils represent current tech                                      | nnology?        | _C_      |  |  |  |
|                    | Are the majority of reference oils of passing or borderline pass/fail                         |                 |          |  |  |  |
|                    | performance?                                                                                  | <b>A</b>        | C        |  |  |  |
| D۵                 | Decouvered of Assessments                                                                     |                 |          |  |  |  |
| <u>180</u>         | Recommended Approaches  D.1.1 Is reference oil supply and distribution handled through        |                 |          |  |  |  |
|                    | an independent organization?                                                                  | unougn          | С        |  |  |  |
|                    | 1,                                                                                            |                 | C        |  |  |  |
|                    | D.1.2 Is a quality control plan defined and in place?                                         |                 | C        |  |  |  |
|                    |                                                                                               |                 |          |  |  |  |
|                    | D.1.3 Is a turnover plan defined/in place to ensure u                                         | -               | <b>A</b> |  |  |  |
|                    | supply of reference oil and an orderly transition                                             | ii to rebienas? | A        |  |  |  |
|                    |                                                                                               |                 |          |  |  |  |
|                    |                                                                                               |                 |          |  |  |  |

RATING SCALE: A - Completed; B - In Progress; C - Planned; D - No Action

May 2002 revised

**Attachment** Page Reference Recommended Approaches D.3.1 Is the fuel specified and the supplier(s) identified? Specified Fuels, EEE. Is a process in place to monitor fuel stability over time? Specified Fuels sampling. Are approval guidelines in place for fuel certification? FTP Certification process D.3.2 If the test fuel is treated as a critical part of the test procedure: Is an approval plan and severity monitoring plan for each fuel batch in place? FTP Certification process Is a quality control plan defined and in place to assure long term quality of the fuel? FTP Certification process Is a turnover plan defined, in place and demonstrated to ensure uninterrupted supply of fuel? FTP Certification process turnover plan

**Comments:** The impact of fuel batch changes has been assumed to be non-critical.

RATING SCALE: A - Completed; B - In Progress; C - Planned; D - No Action

|                                              |                                                                                                                                                 | Attachment        | 14  |  |  |  |
|----------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------|-------------------|-----|--|--|--|
|                                              |                                                                                                                                                 | Page<br>Reference | 60  |  |  |  |
| D.5.5                                        | Are routine rater workshops conducted/planned?                                                                                                  |                   | C   |  |  |  |
| Comr                                         | nents:                                                                                                                                          |                   |     |  |  |  |
| D.6 Calibration, Monitoring and Surveillance |                                                                                                                                                 |                   |     |  |  |  |
|                                              | imended Approaches  Is a process in place for independent monitoring of a precision with an action plan for maintaining calibratellaboratories? |                   | C   |  |  |  |
| D.6.2                                        | Are stand, lab, and industry reference oil control chapass/fail criteria parameters used to judge calibration                                   |                   | C   |  |  |  |
| D.6.3                                        | Does the specified calibration test interval allow no 15 non-reference oil test between successful calibration                                  |                   | _C_ |  |  |  |
| D.6.4                                        | Is an industry surveillance panel in place?                                                                                                     |                   | C   |  |  |  |
| Comr                                         | nents:                                                                                                                                          |                   |     |  |  |  |
|                                              |                                                                                                                                                 |                   |     |  |  |  |
| D.7 Guidelines for Read Across               |                                                                                                                                                 |                   |     |  |  |  |
|                                              | <u>mended Approaches</u><br>Is a plan defined to establish data for development o<br>BOI and VGRA?                                              | of                | _C_ |  |  |  |
| D.7.2                                        | Has VGRA and BOI data been summarized and include the technical report in D.4.1?                                                                | uded in           | _C_ |  |  |  |
| Comr                                         | ments:                                                                                                                                          |                   |     |  |  |  |

RATING SCALE: A - Completed; B - In Progress; C - Planned; D - No Action