

Test Monitoring Center

203 Armstrong Drive, Freeport, PA 16229, USA

www.astmtmc.org 412-365-1000

D4485 Information Letter 24-1 Sequence Number 16 March 25, 2024

ASTM consensus has not been obtained on this information letter. An appropriate ASTM ballot will be issued in order to achieve such consensus.

TO: D4485 Mailing List

SUBJECT: New EOEC Specification Limits using Reference Oil SL107.

At the June 29, 2022, meeting of the Heavy Duty Engine Oil Classification Panel, the Panel reviewed the successful letter ballot of the following revision to Standard D4485:

The current EOEC variable specification limits, using reference oil 1006, will be replaced by new variable specification limits using reference oil SL107. Revised versions of Tables 3, 4, & 5, along with a revised version of Annex A5, are attached.

The text of the revisions is shown in the attachment. These changes are effective with the approval of this information letter via ASTM ballot at Subcommittee B.

John flu

Joe Franklin Chairman ASTM Subcommittee B

Attachment c: <u>https://www.astmtmc.org/ftp/docs/d4485/procedure_and_ils/il24-1_D4485.pdf</u> Distribution: Email

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Jeffrey A. Clark Executive Director Test Monitoring Center

TABLE 3 Diesel Engine Oil Category CI-4

Required Test	Engine Test Method	R	ated or Measu	ured Parameter	Primary	y Performance Cr	iteria	
Method	U					True to at	Two toot	
		Weighted demerits			One-test 382	Two-test ^A 396	Three-test ^A 402	
				ito mov			-	
		Top groove carbon			52 31	57	59	
	D6923	Top land carbon (TI		– 252 h), g/h, average	13.1	35 13.1	36 13.1	
	D0923				IOC + 1.8	IOC + 1.8	IOC + 1.8	
		Piston, ring, and line		1 h), g/h, average, max	none			
1R (<mark>D6923</mark>) or		Ring sticking			none	none	none	
1P (D6681)		Weighted demerits			350	378	390	
		Top groove carbon		ite may	36	39	41	
		Top land carbon (TI			40	46	49	
	D6681	Average oil consum			12.4	40	49 12.4	
		-		·	12.4	12.4		
		Final oil consumptio		- 300 ff), fflax			14.6	
T-10	D6087/D6087M	Piston, ring, and line	erscunng		none	none	none	
(D6987/D6987M)	D6987/D6987M	Merit rating, ^A min			1000	1000	1000	
or T-12 (<mark>D7422</mark>)	D7422	Merit rating, ⁴ min	erit rating, ^A min			1000	1000	
		Average crosshead	mass loss n	ng max	20.0	21.8	22.6	
		Average crosshead mass. loss, mg, max			report	report	report	
M11 EGR	D6975	Average top ring mass loss, mg			275	320	341	
(D6975)		Oil filter differential pressure at 250 h, kPa, max Average engine sludge, CRC merits at EOT, min			7.8	7.6	7.5	
or ISM (D7468)		Crosshead wear, mg, max			7.5	7.8	7.9	
	D7468	Oil filter Δ pressure	-	may	55	67	74	
	07400	-		, 110	8.1	8.0	8.0	
Ext. T-8E (D5967) ^B	D5967	0 0	Sludge rating, CRC Merits, min Relative viscosity at 4.8 % soot ^c			1.9	2.0	
Sequence IIIF	D6984	Kinematic viscositv	Kinematic viscosity (at 40 °C), percent increase, max			275 (MTAC)	275 (MTAC)	
(D6984) ^D	D7320	Kinematic viscosity,			150	150 (MTAC)	150 (MTAC)	
or Sequence IIIG	D8111		-	increase at 40 °C max	370	370 (MTAC)	370 (MTAC)	
(D7320) [€] or Sequence IIIH (D8111) or Sequence IIIH70 (D8111 using Appendix X5)	D8111 (Using IIIH70 Appendix X5 guideline)	70 h Kinematic visc	osity, % incre	ase at 40 °C max	181	181 (MTAC)	181 (MTAC)	
		Weighted demerits	(WDK), max		332	347	353	
		Top groove fill (TGF	=), %, max		24	27	29	
		Top land heavy carl	bon (TLHC), %	6, max	4	5	5	
1K (D6750) ^G	D6750			g/kWh (0 h – 252 h), max	0.54	0.54	0.54	
		Average oil consum	ption	g/MJ (0 h – 252 h), max	0.15	0.15	0.15	
		Piston, ring, and line	er scuffing		none	none	none	
				mils, max	0.30	0.33	0.36	
RFWT (<mark>D5966</mark>)	D5966	Average pin wear		μm, max	7.6	8.4	9.1	
EOAT (<mark>D6894</mark>) ^{<i>H</i>}	D6894	Aeration, volume pe	ercent, max		8.0	8.0 (MTAC) [/]	8.0 (MTAC) [/]	
	CI-4 Bench Tests			Measured Parameter		Primary Perform	nance Criteria	
D4683 or D4741 o	r D5481 ^J		High tempera	ture/high shear viscosity at 150	°C ^k , min	3.5 m	Pa-s	
MRV-TP-1 (<mark>D4684</mark>)		The following limits are applied to SAE viscosity grades 0W, 5W, 10W, and 15W: Viscosity of 75 h used oil sample from T-10 test (or T-10A ^L test), or 100 h used oil sample from T-12 test (or T-12A ^M test, tested at -20 °C, mPa-s, max						
			If yield stress is detected, use modified D4684 ^N (external preheat), then mPa-s, max			25 0		
			and yield stress, Pa			<3		
Noack (<mark>D5800</mark>)			Evaporative le	oss at 250 °C, %, max		15	5	

135 °C HTCBT (<mark>D659</mark> 4)			Copper, mg/kg increase, ma	20	20		
			Lead, mg/kg increase, max		12	120	
			Tin, mg/kg increase		rep	ort	
			Copper strip rating, ⁰ max		3		
D6278 or D7109 30 Cycles			Kinematic viscosity after she	aring	SAE XW-30	SAE XW-40	
			mm²/s at 100 °C, min	9.3	12.5		
			Foaming/settling, ^P mL, max				
	D892 (Option A not allowed)			Sequence I			
D892 (Option A not allow				Sequence II			
			Sequence III	10	/0		
		[D7216 (Elastomer Compatibi	lity)			
Note—These are the un calculation of which is de	adjusted specification limits for elast escribed in Annex A5.	omer o	compatibility. Candidate oils	shall, however, conform to the <i>adju</i>	isted specification li	<i>mits</i> , the	
Elastomer	Volume Change, %	ŀ	Hardness Change, Points	Tensile Strength Change, %	Elongation at Bre	ak Change, %	
Nitrile (NBR)	(+5, -3)	(+7,	-5)	(+10, -SL107-30)	(+10, -SL107-17)		
Silicone (VMQ)	(+SL107, -3)	(+5,	5, -SL107) (+10, -45) (-		(+20, -30)		
Polyacrylate (ACM)	(+5, -3)	(+8,	-5)	(+18, -15)	(+10, -35)		

Note—TMC SL107 is the designation for the reference oil used in this test method. This designation represents the original blend or subsequent approved re-blends of TMC SL107.

^A See Annex A4 for additional information.

Fluoroelastomer (FKM)

^B A passing T-11 (TGA % soot at 12.0 mm²/s increase, at 100 °C, min)—6.00 (first test), 5.89 (second test), and 5.85 (third test)—can be used in place of a T-8E in the applicable categories. This is not intended to indicate equivalence.

(+7, -5)

^c Relative Viscosity (RV) = viscosity at 4.8 % soot/viscosity of new oil sheared in Test Method D6278.

^D Refer to RR:D02-1391.

^{*E*} The Sequence IIIG limits shown are more restrictive than the corresponding limits in Sequence IIIF, and are not intended to indicate equivalence. Results meeting the Sequence IIIG criteria stated can be used in lieu of Sequence IIIF.

 $PVIS@(60 - 80)h = \left(\frac{\sqrt{PVIS@60 h} + \sqrt{PVIS@80 h}}{2}\right)$

(+10, -SL107+2)

, where PVIS@60 h is percent

(+10, -SL107)

^F 60-80 h value is interpolated according to the equation viscosity increase at 60 h and PVIS@80 h is percent viscosity increase at 80 h.

(+5, -2)

^G Refer to RR:D02-1273. Alternatively, Test Method D6750 (1N) can be used; if this test method is used, the measured parameters and primary performance criteria are the same as those shown for Test Method D6750 (1N) in the CJ-4 category.

^H Refer to RR:D02-1379.

[/] See Annex A2; use method without transformations.

^J Tests as allowed in SAE J300.

^K Noncritical specification as defined by Practice D3244; may be superseded only by applicable higher limits set by SAE J300.

^L The T-10A test is the name given to a T-10 test run for 75 h to generate the sample for measurement by Test Method D4684.

^M The T-12A test is the name given to a T-12 test run for 100 h to generate the sample for measurement by Test Method D4684.

^N Refer to RR:D02-1517.

^o The rating system in Test Method D130 is used to rate the copper coupon in Test Method D6594.

^P Ten minutes for Sequence I, II, and III.

		TABLE 4 Diesel Engine Oli	Oalegoly 05-4				
Required Test Method	Engine Test Method	Rated or Measured Pa	rameter	Prima	ry Perform	ance (Criteria
				One-test	Two-te	est	Three-test
T-12 (<mark>D7422</mark>)	D7422	Merit rating, ^A min		1000	1000	0	1000
ISM (D7468)	D7468	Merit rating, ^A min		1000	1000	0	1000
ISIM (D7400)	D7400	Top ring mass loss, mg, max		100	100)	100
C12 (D7540)	D7540	Merit rating, ⁴ min		1000	1000	0	1000
C13 (D7549)	D7549	Hot-stuck piston ring		none	none	е	none
		TGA % Soot at 4.0 mm²/s increase, at 10	00 °C, min	3.5	3.4		3.3
T-11 (<mark>D7156</mark>)	D7156	TGA % Soot at 12.0 mm²/s increase, at ²	00 °C, min	6.0	5.9	J	5.9
		TGA % Soot at 15.0 mm ² /s increase, at ²	00 °C, min	6.7	6.6	i	6.5
		Slider tappet mass loss, mg, average, m	ax	100	108	3	112
ISB (<mark>D7484</mark>)	D7484	Cam lobe wear, µm, average, max		55	59		61
		Crosshead mass loss, mg, average		report	repoi	rt	report
		Weighted demerits (WDN), max		286.2	311.	.7	323.0
		Top groove fill (TGF), %, max		20	23		25
		Top land heavy carbon (TLHC), %, max		3	4		5
1N (<mark>D6750</mark>)	D6750	Oil consumption	g/kWh, (0 h – 252 h), max	0.54	0.54	l)	0.54
			g/MJ (0 h – 252 h), max	0.15	0.15	5	0.15
		Piston, ring, and liner scuffing		none	none	е	none
		Piston ring sticking		none	none	е	none
			mils, max	0.30	0.33	3	0.36
RFWT (<mark>D5966</mark>)	D5966	Average pin wear,	µm, max	(7.6)	(8.4)	·)	(9.1)
Sequence IIIF (D6984)	D6984	Kinematic viscosity (at 40 °C), % increas	e, max	275	275 (MT	FAC)	275 (MTAC)
or	D7320	Kinematic viscosity (at 40 °C), % increas		150	150 (MT		150 (MTAC)
Sequence IIIG (D7320) ^B or	D8111	60 – 80 h ^c Kinematic viscosity, % increas	370	370 (MT		370 (MTAC)	
Sequence IIIH (D8111) or Sequence IIIH70 (D8111 using Appendix X5)	D8111(Using IIIH70 Appendix X5 guideline)	70 h Kinematic viscosity, % increase at 4	0 °C max	181	181 (MT	FAC)	181 (MTAC)
EOAT (D6894)	D6894	Aeration, volume, %, max		8.0	8.0 (MT	AC)	8.0 (MTAC)
Bench Tes	t Methods	Measured Parame	ter	Primary Performance Criteria			
D4683 or D4171 or D548	31	High temperature/high shear viscosity at	150 °C, min		3.5 mP	a-s	
		Copper, mg/kg increase, max		20			
HTCBT, 135 °C (D6594)		Lead, mg/kg increase, max		120			
		Copper strip rating, ^D max		3			
D7400			24 4 4 9 9 9 9	SAE XW-	30	SA	E XW-40
D7109		Kinematic viscosity after 90 pass shearin	g, mm ² /s at 100 °C, min	9.3			12.5
				SAE < > 10\	N-30	SA	E 10W-30
Noack (D5800)		Evaporative loss at 250 °C, %, max		13			15
		Foaming/settling, ^{<i>E</i>} mL, max					
Foam (<mark>D892</mark>)		Sequence I			10/0)	
1 0dill (10032)		Sequence II			20/0)	
		Sequence III			10/0)	
MRV TP-1 (D6896)		Viscosity of the 180 h used oil drain sam tested at –20 °C, mPa-s, max	25 000				
		If yield stress is detected, use the modified preheat), then measure the viscosity, mF			25 00)0	
		Measure the yield stress, Pa			<35	; 	
		Chemical Limits (non-c	ritical)				
Bench Tes	t Methods	Measured Parame	ter	Prima	ry Perform	ance (Criteria
D874		Mass fraction sulfated ash, %, max			1.0		
D4951		Mass fraction phosphorus, %, max			0.12		
		Mass fraction sulfur, %, max			0.4		

TABLE 4 Diesel Engine Oil Category CJ-4

calculation of which is descri	ibed in Annex A5.		· · · ·	•
Elastomer	Volume Change, %	Hardness Change, Points	Tensile Strength Change, %	Elongation at Break Change, %
Nitrile (NBR)	(+5, -3)	(+7, -5)	(+10, -SL107-30)	(+10, -SL107-17)
Silicone (VMQ)	(+SL107, -3)	(+5, -SL107)	(+10, -45)	(+20, -30)
Polyacrylate (ACM)	(+5, -3)	(+8, -5)	(+18, -15)	(+10, -35)
Fluoroelastomer (FKM)	(+5, -2)	(+7, -5)	(+10, -SL107+2)	(+10, -SL107)
Vamac G	(+SL107+2, -3)	(+5, -SL107-2)	(+10, -SL107+2)	(+10, -SL107+10)

^A See Annex A6 for additional information.

^B The Sequence IIIG limits shown are more restrictive than the corresponding limits in Sequence IIIF, and are not intended to indicate equivalence. Results meeting the Sequence IIIG criteria stated can be used in lieu of Sequence IIIF. 2

$$PVIS@(60 - 80)h = \left(\frac{\sqrt{PVIS@60 h} + \sqrt{PVIS@80 h}}{2}\right)$$

, where PVIS@60 h is percent

^c 60 – 80 h value is interpolated according to the equation viscosity increase at 60 h and PVIS@80 h is percent viscosity increase at 80 h.
^p The rating system in Test Method D130 is used to rate the copper coupon in Test Method D6594.

^E Ten minutes for Sequence I, II, and III.

Required Test Method Engine Test Method Rated or			ured Pa	rameter		Primar	y Performanc	e Criteria
						One-test	Two-test ^A	Three-test ^A
	D7422	Top Ring Mass Loss, mg, max				105	105	105
T-12 (D7422)	D7422	Cylinder Liner Wear, µm, max				24.0	24.0	24.0
		IR Peak at EOT, Abs., cm ⁻¹				125	130	133
T-13 (<mark>D8048</mark>)	D8048	Kinematic Viscosity Increase at 40) °C, %	max		75	85	90
		Avg. Oil Consumption, 48 h to 192	2 h, g/h,	max		Report	Report	Report
		TGA % Soot at 4.0 mm ² /s increase	e, at 10	0 °C, min		3.5	3.4	3.3
T-11 (<mark>D7156</mark>)	D7156	TGA % Soot at 12.0 mm ² /s increa	se, at 1	00 °C, min		6.0	5.9	5.9
		TGA % Soot at 15.0 mm ² /s increa	TGA % Soot at 15.0 mm²/s increase, at 100 °C, min			6.7	6.6	6.5
C13 (<mark>D7549</mark>)	D7549	Merit rating, ^A min				1000	1000	1000
COAT (<mark>D8047</mark>)	D8047	Average Aeration, ^A 40 h to 50 h, %	6			11.8	11.8	11.8
		Slider tappet mass loss, mg, avera	age, ma	х		100	108	112
ISB (<mark>D7484</mark>)	D7484	Cam lobe wear, µm, average, max	x			55	59	61
		Crosshead mass loss, mg, averag	je			Report	Report	Report
	57100	Top Ring Mass Loss, mg, max				100	100	100
ISM (D7468)	D7468	Merit Rating, ^A				1000	1000	1000
		Weighted demerits (WDN), max				286.2	311.7	323.0
		Top groove fill (TGF), %, max				20	23	25
		Top land heavy carbon (TLHC), %, max				3	4	5
1N (D6750)	D6750	Oil consumption		g/kWh, (0 h to max	252 h),	0.54	0.54	0.54
				g/MJ (0 h to 25	52 h), max	0.15	0.15	0.15
		Piston, ring, and liner scuffing				none	none	none
		Piston ring sticking				none	none	none
RFWT (<mark>D5966</mark>)	D5966	Average pin wear,		mils, max µm, max		0.30 (7.6)	0.33 (8.4)	0.36 (9.1)
		CK-4 Category	Bench	•		(1.0)	(0.4)	(0.1)
Test Method		Measured Parameter	y Denon	10313		Primary Perf	formance Crite	Pria
1 Col Method		SAE J300 Viscosity Grade			SAE xW		SAE xW	
D4683 or D4741 or D5481	High temperature/high sł	hear viscosity at 150 °C, mPa⋅s	min max		3.5 N/A	5 Meets SAF J300		
	Copper, mg/kg increase,	max			20		20	
HTCBT, 135 °C	Lead, mg/kg increase, m				120			
(D6594)	Copper strip rating, ^B max				3		3	
Noack (<mark>D5800</mark>)	Evaporative loss at 250 °	°C, %, max			13			
	Foaming/settling, ^c Seque	ence I, mL, max			10/0		10/0	1
Foam (<mark>D892</mark>)	Foaming/settling, ^c Seque	ence II, mL, max			20/0		20/0	1
	Foaming/settling, ^c Seque	ence III, mL, max			10/0		10/0	
viscosity after 50	Kinematic viscosity after	90 pass shearing, mm²/s at 100 °C	, min	-	xW-30		W-40 12.5	Other xW-40 12.8
pass shearing (see above methods)	HTHS viscosity at 150 °C	CmPa⋅s min			3.4		N/A	N/A
Sooted Oil MRV TP-	Viscosity, 180 h used oil sample from a T-11/T-11A test, tested at –20 °C, mPa·s, 25				25 00		25 00	
(D7156 Engine test required)	max Yield stress of the 180 h used oil sample above, Pa max ≤			≤35		≤35		
		Chemical Limit	s (non-o	critical)		I		
Test Method		Measured Parameter				Primary Perf	formance Crite	eria
D874	Mass fraction sulfated	ash, %, max					1.0	
D4054	Mass fraction phospho	rus, %, max					0.12	
D4951	Mass fraction sulfur, %	, max				0.4		
Mass fraction sulfur, %, max				0.4				

TABLE 5 Diesel Engine Oil Category CK-4

D7216 (Elastomer Compatibility)								
Note—These are the unadjusted specification limits for elastomer compatibility. Candidate oils shall, however, conform to the adjusted specification limits, the calculation of which is described in Annex A5.								
Elastomer	astomer Volume Change, % Hardness Change, Points Tensile Strength Change, % Elongation at Break Change							
Nitrile (NBR)	(+5, -3)	(+7, -5)	(+10, -SL107-30)	(+10, -SL107-17)				
Silicone (VMQ)	(+SL107, -3)	(+5, –SL107)	(+10, -45)	(+20, -30)				
Polyacrylate (ACM)	(+5, -3)	(+8, -5)	(+18, –15)	(+10, -35)				
Fluoroelastomer (FKM)	(+5, -2)	(+7, –5)	(+10, -SL107+2)	(+10, -SL107)				
Vamac G	(+SL107+2, -3)	(+5, -SL107-2)	(+10, -SL107+2)	(+10, -SL107+10)				
Note—TMC SL107 is the designation for the reference oil used in this test method. This designation represents the original blend or subsequent approved re- blends of TMC SL107.								

^A See Annex A7 for additional information.
^B The rating system in Test Method D130 is used to rate the copper coupon in Test Method D6594.
^C Ten minutes for Sequence I, II, and III.

Required Test Method	Engine Test Method	Rated or Measured Paramet	Prima	ry Performanc	e Criteria		
Method				One-test	Two-test ^A	Three-test	
		Top Ring Mass Loss, mg, max		105	105	105	
T-12 (<mark>D7422</mark>)	D7422	Cylinder Liner Wear, µm, max		24.0	24.0	24.0	
		IR Peak at EOT, Abs., cm ⁻¹		125	130	133	
T-13 (D8048) D8048		Kinematic Viscosity Increase at 40 °C, % max		75	85	90	
		Avg. Oil Consumption, 48 h to 192 h, g/h, max		Report	Report	Report	
		TGA % Soot at 4.0 mm ² /s increase, at 100 °C, m	in	3.5	3.4	3.3	
T-11 (<mark>D7156</mark>)	D7156	TGA % Soot at 12.0 mm ² /s increase, at 100 °C, in		6.0	5.9	5.9	
1-11 (07100)	DTIO	TGA % Soot at 15.0 mm²/s increase, at 100 °C, min			6.6	6.5	
C13 (D7549)	D7549		6.7 1000	1000	1000		
		Merit rating, ^A min					
COAT (<mark>D8047</mark>)	D8047	Average Aeration, ⁴ 40 h to 50 h, %		11.8	11.8	11.8	
		Slider tappet mass loss, mg, average, max		100	108	112	
ISB (D7484)	D7484	Cam lobe wear, µm, average, max		55	59	61	
		Crosshead mass loss, mg, average		Report	Report	Report	
ISM (<mark>D7468</mark>)	D7468	Top Ring Mass Loss, mg, max		100	100	100	
. ,		Merit Rating, ^A	1000	1000	1000		
		Weighted demerits (WDN), max	286.2	311.7	323.0		
		Top groove fill (TGF), %, max	20	23	25		
	D6750	Top land heavy carbon (TLHC), %, max		3	4	5	
1N (D6750)		Oil consumption	g/kWh, (0 h to 252 h), max	0.54	0.54	0.54	
			(g/MJ) (0 h to 252 h), max	(0.15)	(0.15)	(0.15)	
		Piston, ring, and liner scuffing	none	none	none		
		Piston ring sticking		none	none	none	
RFWT (<mark>D5966</mark>)	D5966	Average pin wear,	mils, max	0.30	0.33	0.36	
IXI WI (D3900)	D3900	Average pin wear,	(µm) max	(7.6)	(8.4)	(9.1)	
		FA-4 Category Bench Test	s				
Tes	st Method	Measured	Parameter			Primary Performance Criteria	
		SAE J300 Vis	scosity Grade			SAE xW-30	
D4683				min		2.9	
or D4741 or D5481		High temperature/high shear viscosity at 150 °C,	max		3.2		
		Copper, mg/kg increase, max	Copper ma/kg increase max				
HTCBT, 135 °F (D6	594)	Lead, mg/kg increase, max				20 120	
, , , , , , , , , , , , , , , , , , ,	,	Copper strip rating, ^B max			3		
Noack (D5800)		Evaporative loss at 250 °C, %, max				13	
, ,		Foaming/settling, ^C Sequence I, mL, max				10/0	
Foam (<mark>D892</mark>)		Foaming/settling, ^c Sequence II, mL, max				20/0	
. ,		Foaming/settling, ^c Sequence III, mL, max					
D7109		Kinematic viscosity after 90 pass shearing, mm ² /					
	(see above methods)	HTHS Viscosity at 150 °C, mPa·s, min	,			2.8	
arter 90 pass snearing					,	25 000	
Sooted Oil MRV TP-1 (D6896) Viscosity, 180 h used oil sample from a T-11/T-11A test, tested at -20 °C, mPa·s, max (D7156 Engine test required) Yield stress of the 180 h used oil sample above, Pa max					`	≤35	
(¹ 3	1 /					_00	
Tes	st Method	Chemical Limits (non-critical) Measured Parameter					
D874		Mass fraction sulfated ach % may				Criteria	
D874		Mass fraction sulfated ash, %, max				1.0	
D4951 Mass fraction phosphorus, %, max					1	0.12	

D7216 (Elastomer Compatibility)								
Note—These are the <i>unadjusted specification limits</i> for elastomer compatibility. Candidate oils shall, however, conform to the <i>adjusted specification limits</i> , the calculation of which is described in Annex A5.								
Elastomer	Volume Change, %	Hardness Change, Points	Tensile Strength Change, %	Elongation at Break Change, %				
Nitrile (NBR)	(+5, -3)	(+7, –5)	(+10, -SL107-30)	(+10, –SL107-17)				
Silicone (VMQ)	(+SL107, -3)	(+5, –SL107)	(+10, -45)	(+20, -30)				
Polyacrylate (ACM)	(+5, -3)	(+8, -5)	(+18, –15)	(+10, -35)				
Fluoroelastomer (FKM)	(+5, -2)	(+7, –5)	(+10, -SL107+2)	(+10, –SL107)				
Vamac G	(+SL107+2, -3)	(+5, -SL107-2)	(+10, -SL107+2)	(+10, -SL107+10)				
Note—TMC SL107 is the de of TMC SL107.	esignation for the reference oil use	ed in this test method. This designa	tion represents the original blend o	or subsequent approved re-blends				

^A See Annex A7 for additional information.

^B The rating system in Test Method D130 is used to rate the copper coupon in Test Method D6594.

^c Ten minutes for Sequence I, II, and III.

NOTE 3—API has developed a symbol that can be licensed for use on containers of oils that conform to the requirements of one or more categories that are currently of commercial importance. API 1509 describes the symbol and licensing procedure.

NOTE 4-In practice, engine oils are often labeled with service category designations having some combination of both S and C prefixes.

NOTE 5—Intended service applications for the various categories described in 4.1.1 - 4.1.3 can be found in API 1509. Several applicable sections of that publication have been included in Appendix X2.

A5. PROCEDURE FOR DERIVING ADJUSTED SPECIFICATION LIMITS FOR ELASTOMER COMPATIBILITY

A5.1 Background

A5.1.1 This annex describes a statistical method to account for the inherent test variability in the elastomer compatibility test method. The need to take account of the inherent test variability arises in part because batch-to-batch, sheet-to-sheet and within-sheet variations in the properties of the reference elastomers (the four elastomers listed for the CI-4 category in Table 3; the five elastomers listed for the CJ-4 category in Table 4, the CK-4 category in Table 5 and the FA-4 category in Table 6) can be sufficiently large that they complicate making a decision as to whether or not a candidate oil has passed the elastomer compatibility requirements.

A5.1.2 Applying this statistical method to the unadjusted specification limits noted in Tables 3-6 produces the adjusted specification limits. *Passing* candidate-oil results shall lie within the range defined by the adjusted specification limits.

A5.1.3 The statistical method for determining the adjusted specification limits uses updated information about the industry test variability relevant to the time frame in which the candidate oil is tested. The TMC provides the updated information based on test results obtained by different test laboratories with different batches of reference elastomers on the same TMC SL107 reference oil.

A5.2 Unadjusted Specification Limits

A5.2.1 The unadjusted specification limits are shown for the CI-4 category in Table 3. (These are reproduced in Table A5.1 for comparison purposes.) The test method involves sixteen criteria. These criteria are the unadjusted specified limits for the four elastomer types (nitrile, silicone, polyacrylate and fluoroelastomer), with changes in four properties (volume, hardness, tensile strength and elongation at break). (The unadjusted specification limits are shown for the CJ-4 category in Table 4, the CK-4 category in Table 5 and the FA-4 category in Table 6.)

Elastomer Volume Change, %		Hardness Change, Points	Tensile Strength Change, MPa	Elongation at Break Change, %
Nitrile (NBR)	(+5, -3)	(+7, -5)	(+10, -SL107-30)	(+10, -SL107-17)
Silicone (VMQ)	(+SL107, -3)	(+5, -SL107)	(+10, -45)	(+20, -30)
Polyacrylate (ACM)	(+5, -3)	(+8, -5)	(+18, -15)	(+10, -35)
Fluoroelastomer (FKM)	(+5, -2)	(+7, -5)	(+10, -SL107+2)	(+10, -SL107)

TABLE A5.1 Unadjusted Specification Limits for the Elastomer Test Method as Part of the CI-4 Engine Oil Category

A5.3 Adjusted Specification Limits

A5.3.1 The adjusted specification limits are calculated by adjusting the numerical limits in Tables 3-6 (referred to as *fixed limits*), and the TMC SL107 limit in Tables 3-6 (referred to as a *variable limit*). The reference oil TMC SL107 is run in parallel with the candidate oil as a control for each experiment. The TMC SL107 limit ties back to the original TMC 1006 performance; it is this tie-back that accounts for the additional +/- adjustment to the performance of TMC SL107.

A5.3.2 The adjusted specification limits are determined as the unadjusted specification limits plus (in absolute terms) an amount to account for test variability.

A5.4 Inherent Test Variability

A5.4.1 Table A5.2 shows the initial TMC SL107 standard deviation estimates of the four reference elastomers and the four performance parameters, as reported by the TMC. The standard deviation estimates, applicable at the time a test oil is evaluated, are obtained from the TMC website (<u>https://www.astmtmc.org/ftp/docs/d4485/D7216_Adjusted_Specification_Limit_Data/</u>). With the introduction of SL107 Adjusted Specification Limits in 2023, the standard deviation took into account the data to date. Starting in 2025, the standard deviation will take into account a rolling 24 months of data and will be updated annually in February.

TABLE A5.2 Total and within-Laboratory Standard Deviation Estimates for the Four Reference Elastomers"								
Elastomer		Volume Change	Hardness Change	Tensile Strength Change	Elongation at Break Change			
Nitrile (NBR)	Total	0.57	1.16	5.53	6.57			
Nitrile (NBR)	Within-Lab	0.53	1.12	5.22	6.36			
Silicone (VMQ)	Total	3.08	2.13	5.14	6.82			
Silicone (VMQ)	Within-Lab	1.72	1.40	4.42	6.18			
Polyacrylate (ACM)	Total	0.57	1.70	7.14	10.50			
Polyacrylate (ACM))	Within-Lab	0.54	1.63	6.93	10.24			
Fluoroelastomer (FKM)	Total	0.21	2.14	4.02	6.20			
Fluoroelastomer (FKM)	Within-Lab	0.20	1.58	2.82	4.64			
Vamac G (MAC)	Total	1.88	1.46	5.82	7.84			
Vamac G (MAC)	Within-Lab	1.69	1.37	5.84	7.44			

TABLE A5.2 Total and Within-Laboratory Standard Deviation Estimates for the Four Reference Elastomers⁴

^A All data collected for EOEC Calibration runs using SL107 reference oil through December 31, 2023. Data is active through January 31, 2025. For future Standard Deviation Estimates, see "<u>https://www.astmtmc.org/ftp/docs/d4485/D7216_Adjusted_Specification_Limit_Data/</u>"

A5.5 Adjusted Specification Limits—Calculations

A5.5.1 Calculation of Fixed Limits:

A5.5.1.1 Calculate the standard error of the test-oil mean by dividing the appropriate *total standard deviation* estimate by the square root of the number of observations in the sample. The number of observations in the sample, in the absence of outliers, is six.

A5.5.1.2 Multiply the standard error of the test-oil mean by 2.0.

A5.5.1.3 Add or subtract the resulting number to or from the respective upper or lower unadjusted specification limits to obtain the *fixed* adjusted specification limit(s).

A5.5.2 Calculation of Variable Limits:

A5.5.2.1 Calculate the standard error of the test-oil mean by dividing the appropriate *total standard deviation* estimate by the square root of the number of observations in the sample. The number of observations in the sample, in the absence of outliers, is six. A5.5.2.2 Multiply the standard error of the test-oil mean by 2.8.

A5.5.2.3 Add or subtract the resulting number to or from the mean result obtained with TMC SL107 (run in parallel with the test oil) to obtain either the upper or lower *variable* adjusted specification limit.

A5.5.3 Table A5.3 shows an example of the calculated adjusted specification limits.

TABLE A5.3 An Example of Adjusted Specification Limits for the Four Reference Elastomers—Applicable for the Period February 1, 2024 to January 31, 2025⁴

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Elastomer	Volume Change, %	Hardness Change, Points	Tensile Strength Change, %	Elongation at Break Change, %				
Nitrile (NBR)	(+5.7, -3.7)	(+8.5, -6.5)	(+16.3, -SL107 -38.5)	(+16.3, -SL107 -25.8)				
Silicone (VMQ)	(+SL107 +2.6, -4.9)	(+7.1, -SL107 -1.8)	(+14.4, -49.4)	(-28.1, -38.1)				
Polyacrylate (ACM)	(+5.7, -3.7)	(+9.6, -6.6)	(+26.3, -23.3)	(+19.1, -44.1)				
Fluoroelastomer (FKM)	(+5.1, -2.1)	(+9.0, -7.0)	(+14.6, -SL107 -4.0)	(+18.6, -SL107 -9.6)				
Vamac G (MAC)	(+SL107 +2.3, -4.9)	(+6.0, -SL107 -1.0)	(+17.4, -SL107 -9.8)	(+19.5, -SL107 -12.4)				

^A Based on unadjusted specification limits, standard deviation estimates shown in Table A5.2, and six observations in all cases.

A5.6 Comparison of Unadjusted and Adjusted Specification Limits

A5.6.1 Table A5.1 reproduces the unadjusted specification limits for comparison with the above adjusted specification limits.